

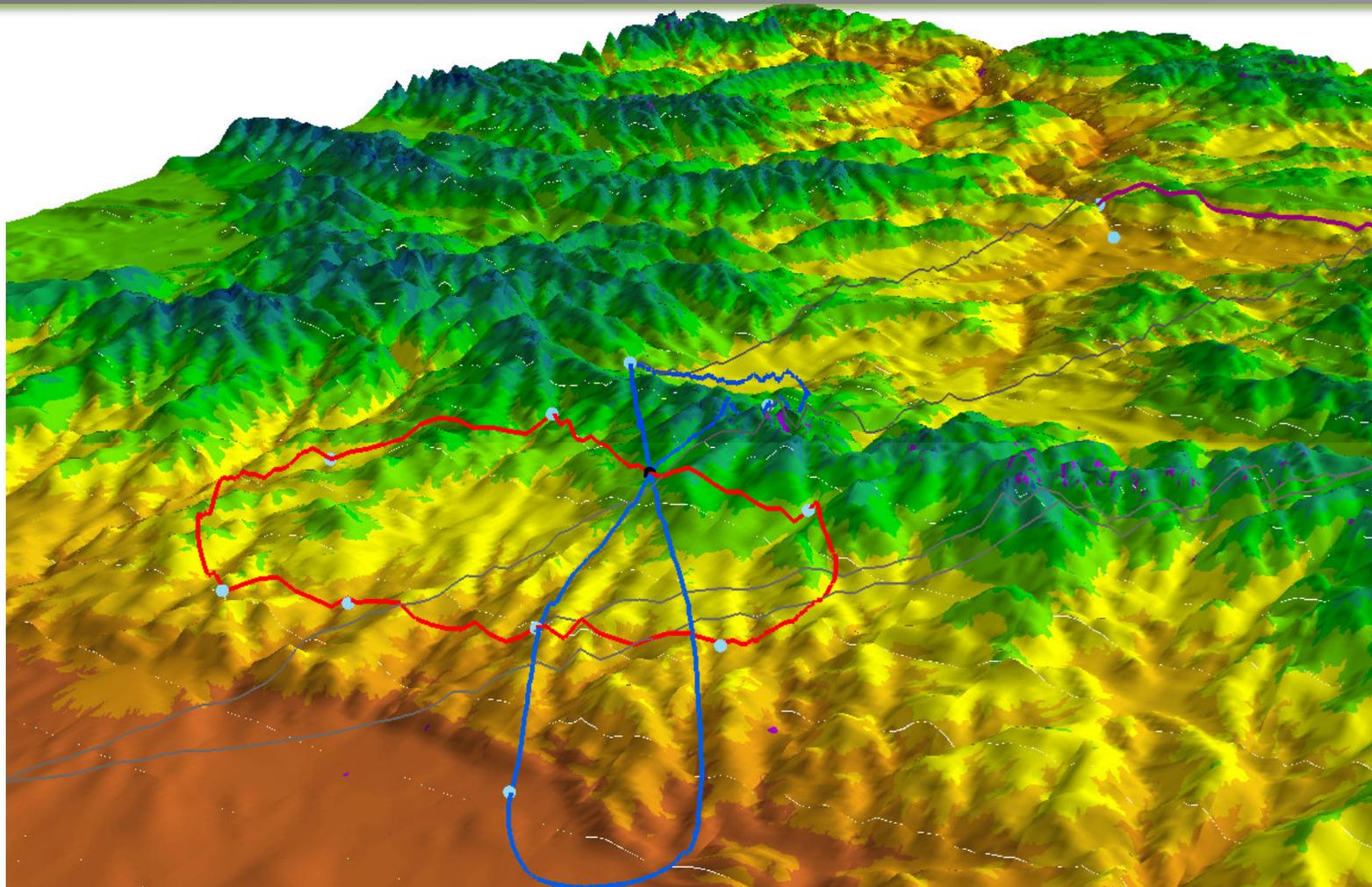
# **A nonlinear analytical analysis of terrain-induced canopy flows**

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# Outline

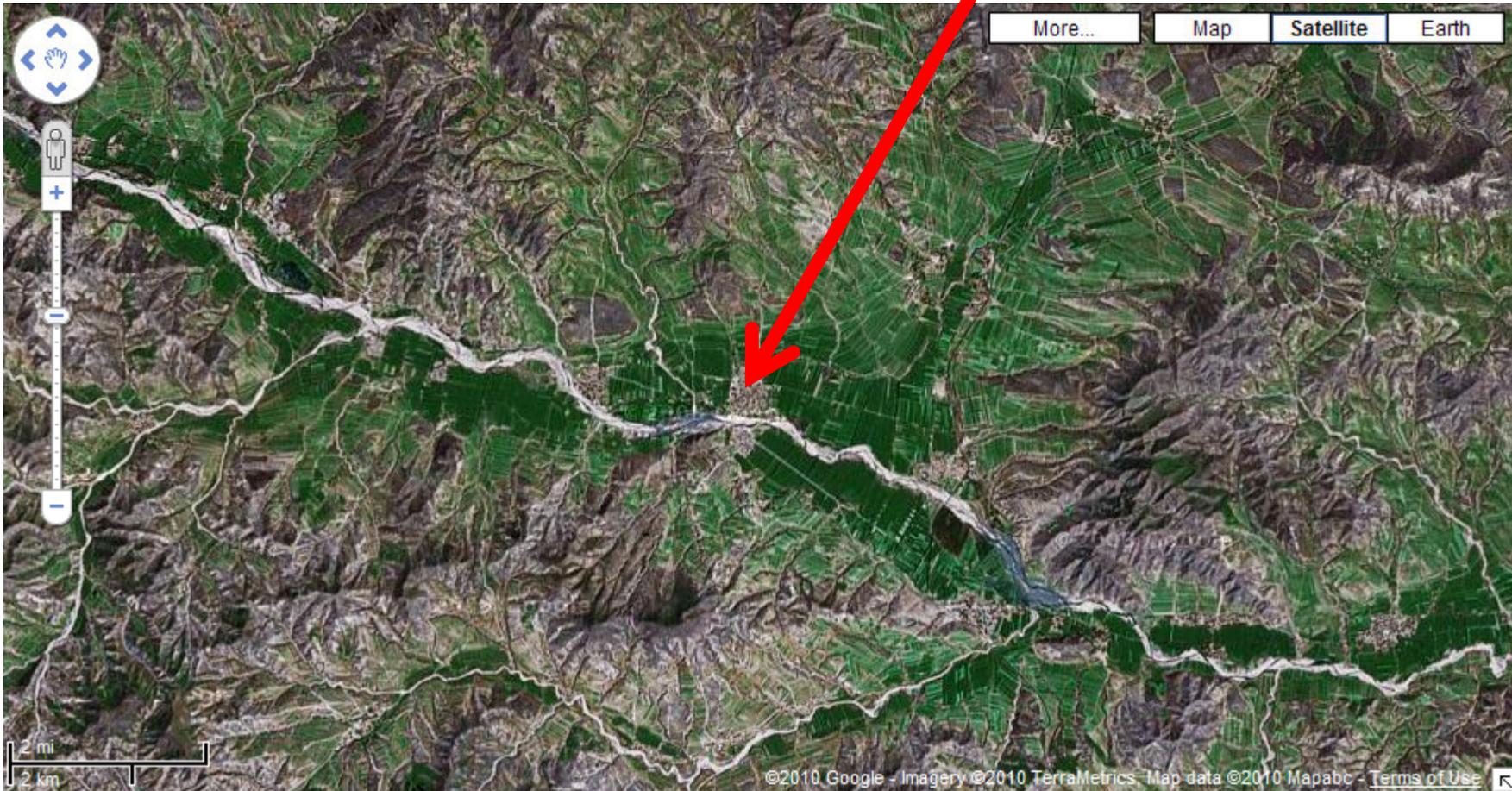
- **Complex terrain**
- **Analytical approach**

# ***Real world surface is not flat***



Courtesy of David Schimel

***Complex terrain is pretty much everywhere  
I was born from a complex terrain***



# Canopy flows over a forested hill Analytical theory milestone

A theoretical foundation (**no trees**) was established by Jackson and Hunt (1975)



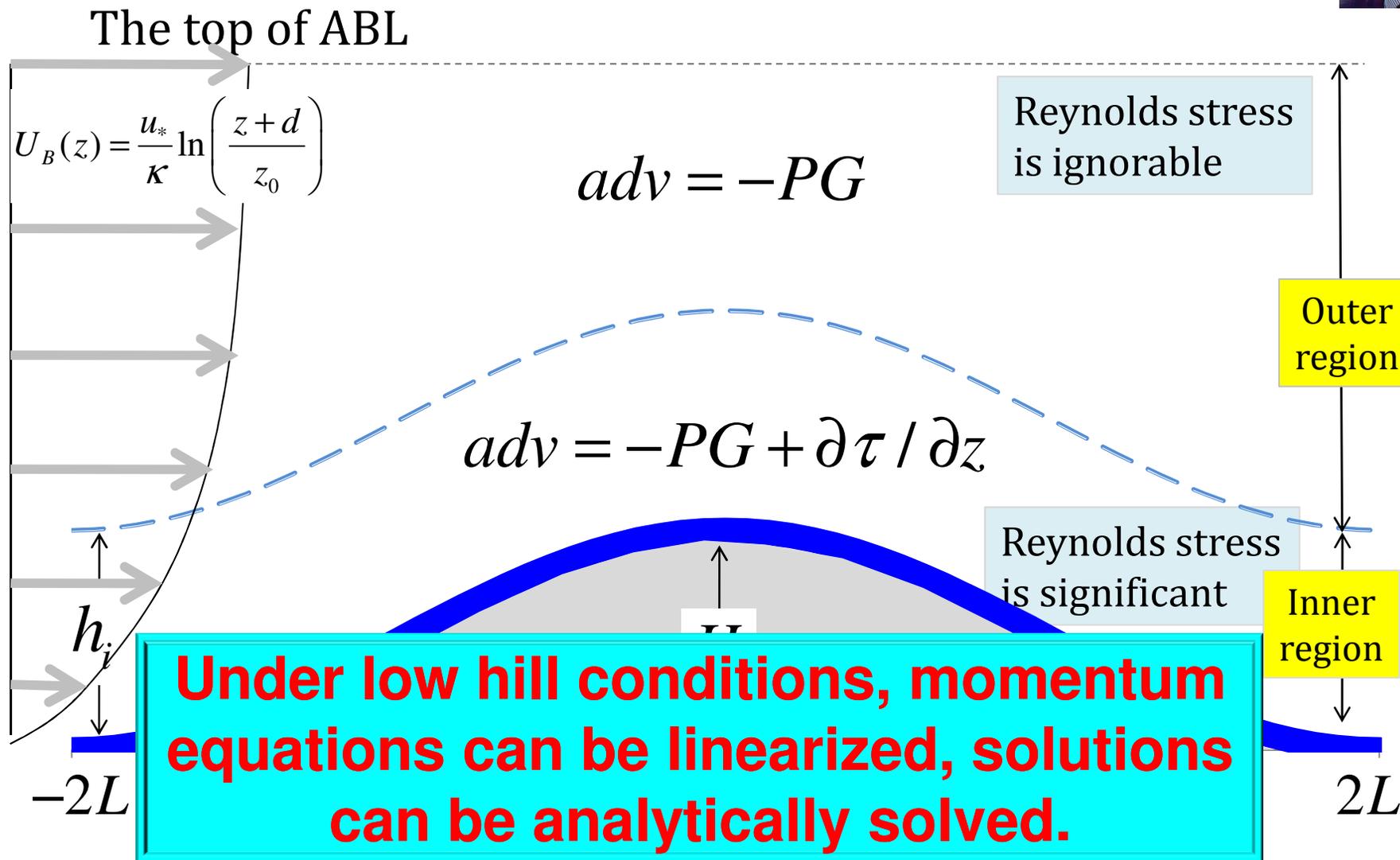
Analytical solutions of canopy flows over a forested hill was first obtained by Finnigan and Belcher (2004)



Intensive laboratory studies of canopy flows over a forested hill has been Conducted by Katul and Poggi (2008a,b,c,d,e)



# JH75 → A linear theory



$$adv = u\partial u / \partial x + w\partial u / \partial z$$

$$PG = \partial P / \partial x$$

$$\tau = -\overline{u'w'}$$



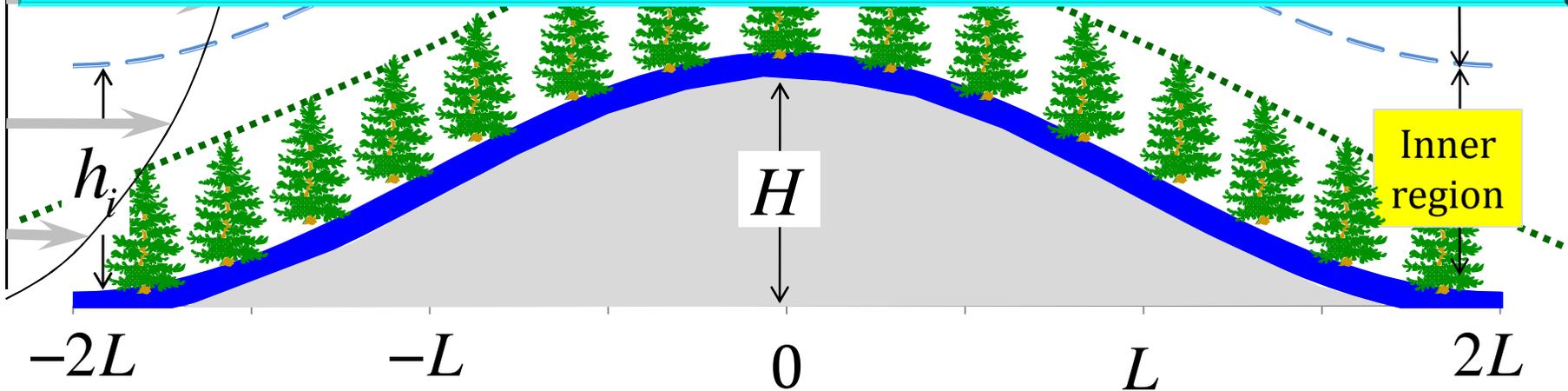
# FB04 → analytical solution within canopy



FB04 kept all assumptions of JF75's linear theory same except adding a canopy layer near ground and obtained analytical solutions of wind profile within canopy.

$U_B(z)$

**This layer is important but difficult to know!!!  
What assumptions were made in FB04 theory?**



$$adv = u\partial u / \partial x + w\partial u / \partial z$$

$$PG = \partial P / \partial x$$

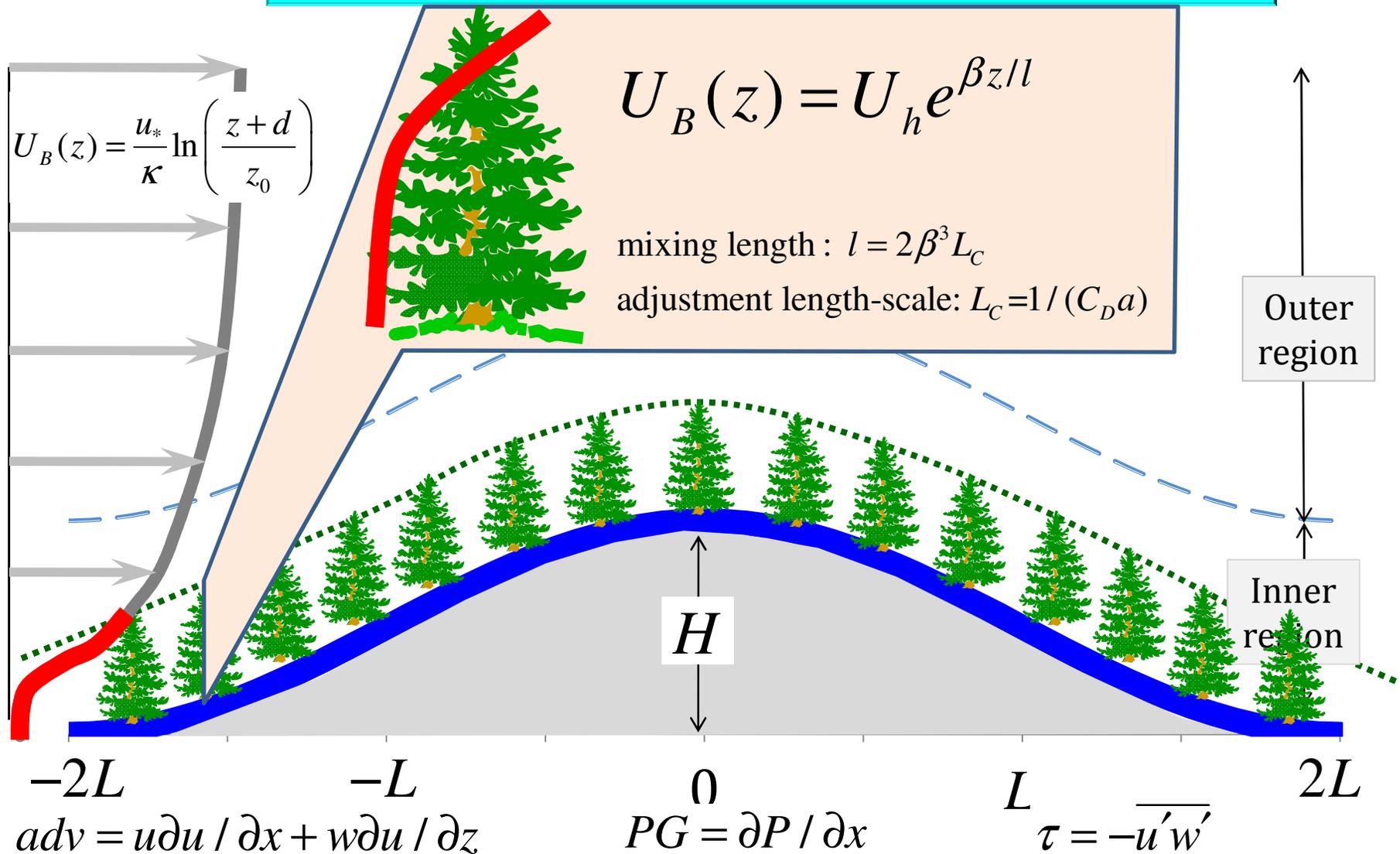
$$\tau = -\overline{u'w'}$$



# FB04 → analytical solution within canopy



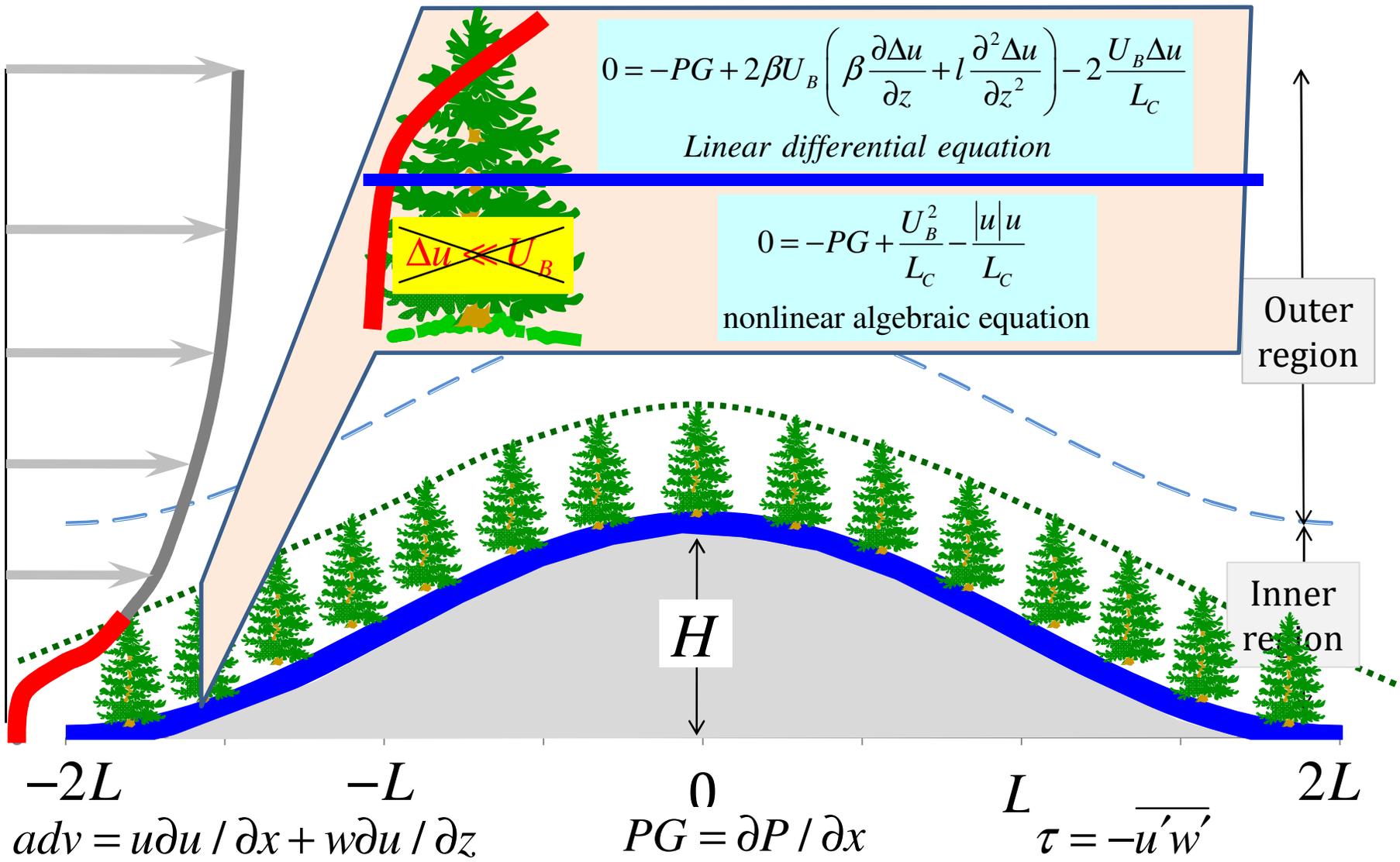
## Basic state within canopy: Inoue's model





**To obtain analytical solution**  $u(z) = U_B(z) + \Delta u(z)$

**Assumed:** ~~adv~~  $\Rightarrow$  3-force balance;  $\Delta u \ll U_B \Rightarrow$  linearization





# FB04 → analytical solution within canopy



$$u = U_B + \Delta u = \left| U_B^2 - L_C PG \right|^{1/2} \text{sgn} \left( U_B^2 - L_C PG \right) + A_C U_C e^{\beta z/l}$$

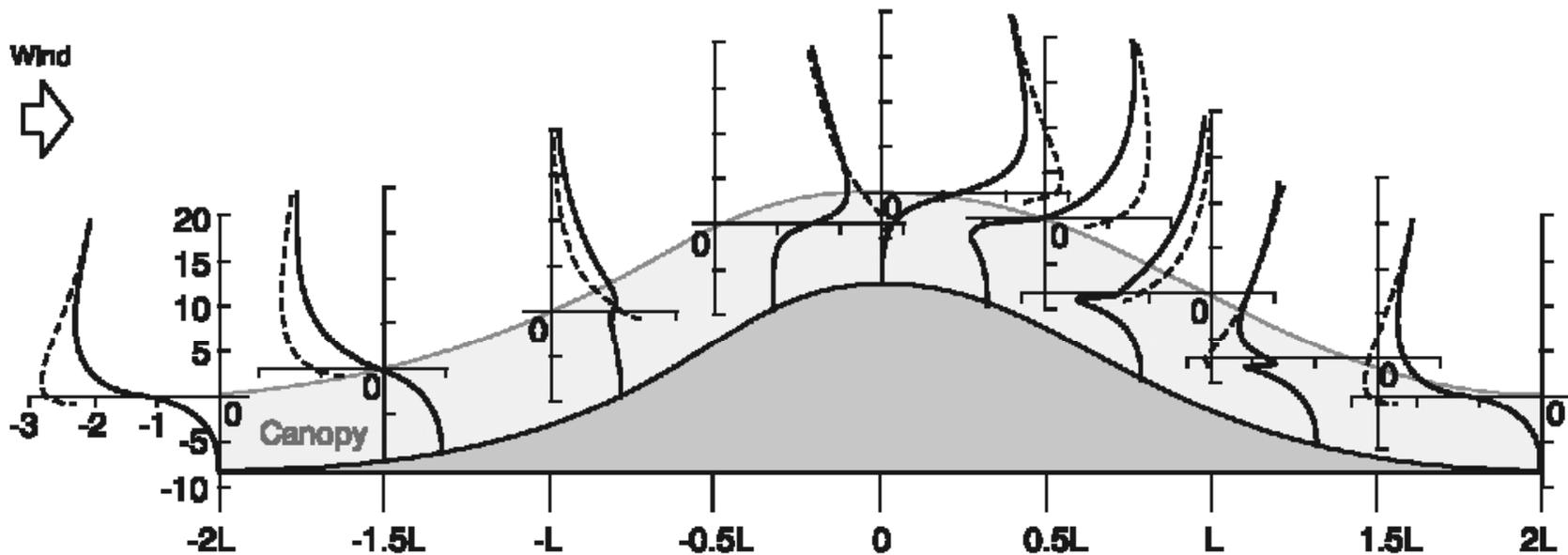


Figure 2. Comparison of canopy velocity perturbation,  $\Delta u/U_{SC}$  with the no-canopy solution of Hunt *et al.* (1988; dotted line). Note the Hunt *et al.* solution is only valid to  $z = -d + z_0$ . Profiles are plotted at a series of  $X/L$  values between  $X/L = -2$  (upwind trough) and  $X/L = 2$  (downwind trough). The units of  $Z$  are m, and the vertical range is from  $2h_i > Z > L_c$ . See text for details.

**FB04 made great progresses but some weaknesses need to be improved**

## **What are weaknesses of FB04?**

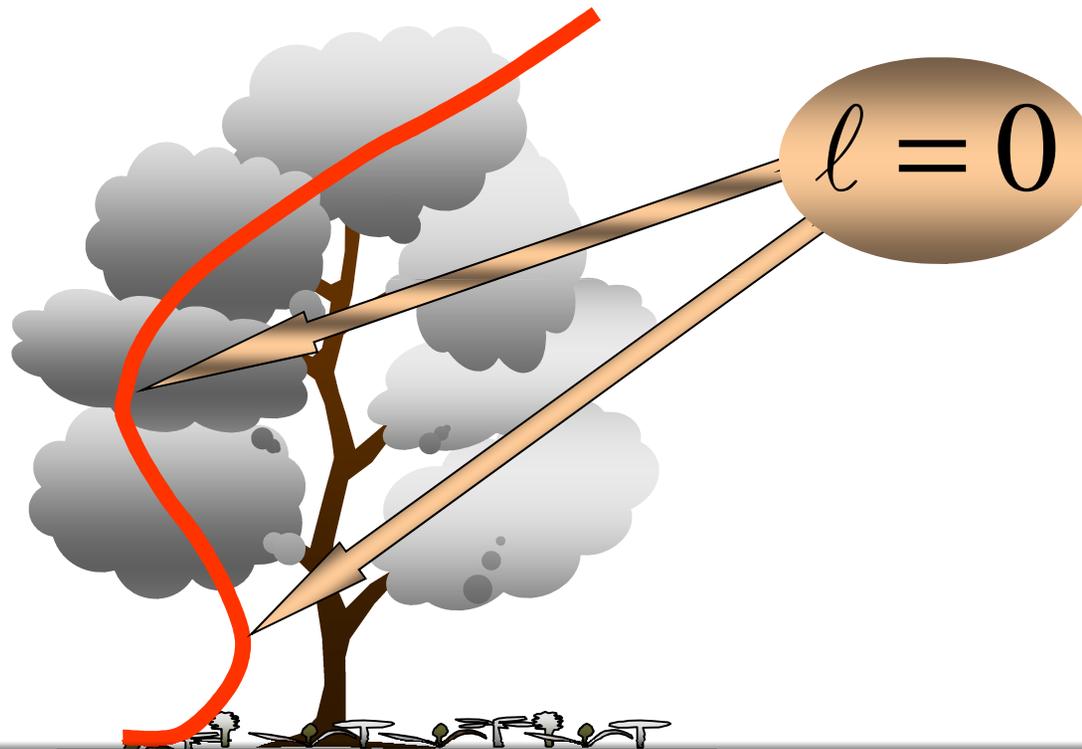
- **Physical inconsistency** -- Constant mixing-length assumption leading to a varying mixing-length.
- **A non-slip boundary condition** is not able to apply to the nonlinear algebraic equation.
- It is unnecessary to divide a canopy layer into **two layers**: a linear layer and a nonlinear layer.
- No need to assume  $\Delta u \ll U_B$

**Theoretically, Mixing-length is not constant within canopy!**



Von Karman  
similarity rule

$$\ell = \kappa \left| \frac{d\bar{u} / dz}{d^2\bar{u} / dz^2} \right|$$



- Mixing-length is not constant
- Mixing-length theory is not valid within canopy

**Large Eddy Simulation demonstrated “that a constant mixing-length assumption is not strictly valid within the canopy.” – Andrew Ross (2008 in BLM)**

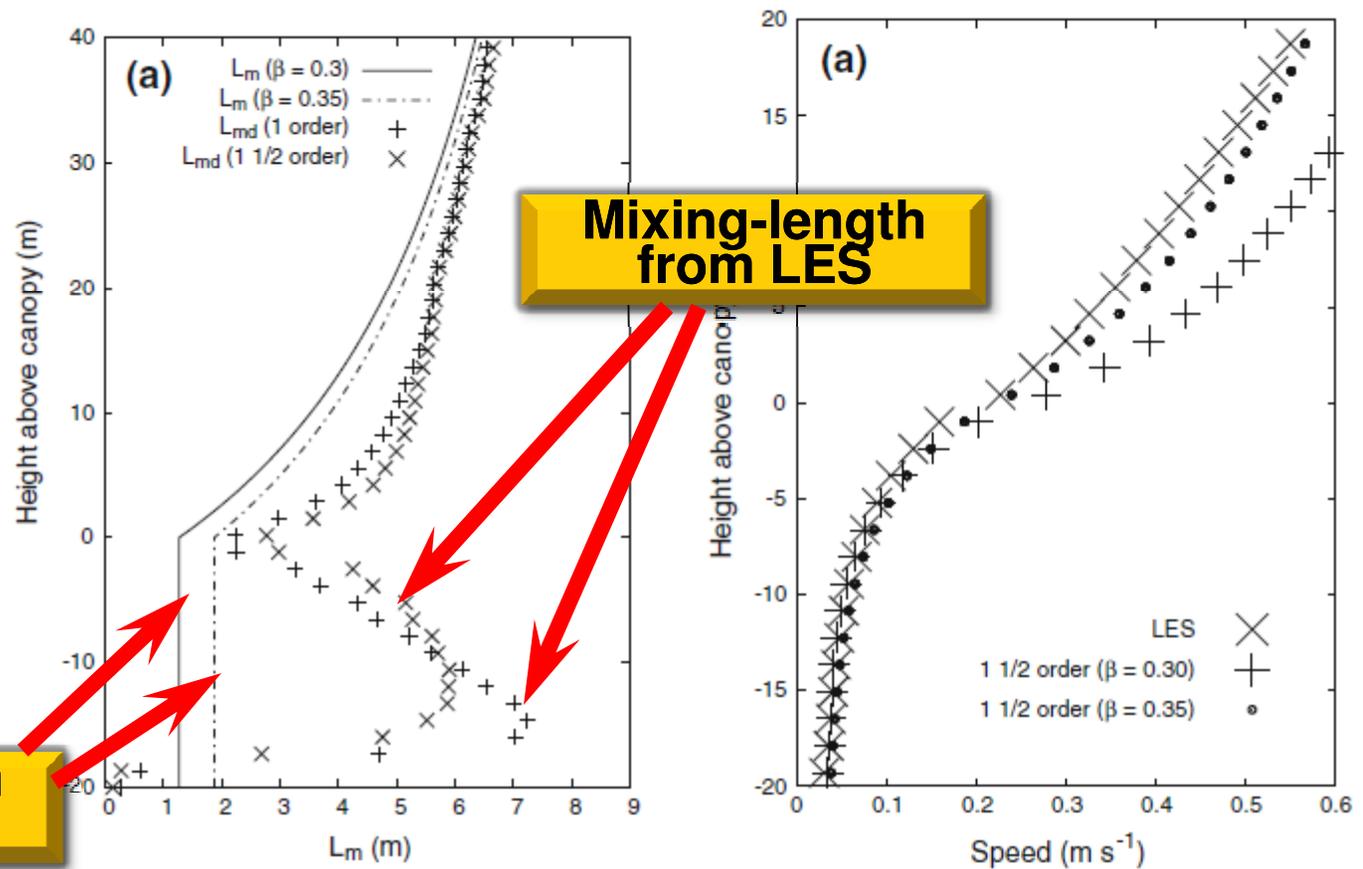
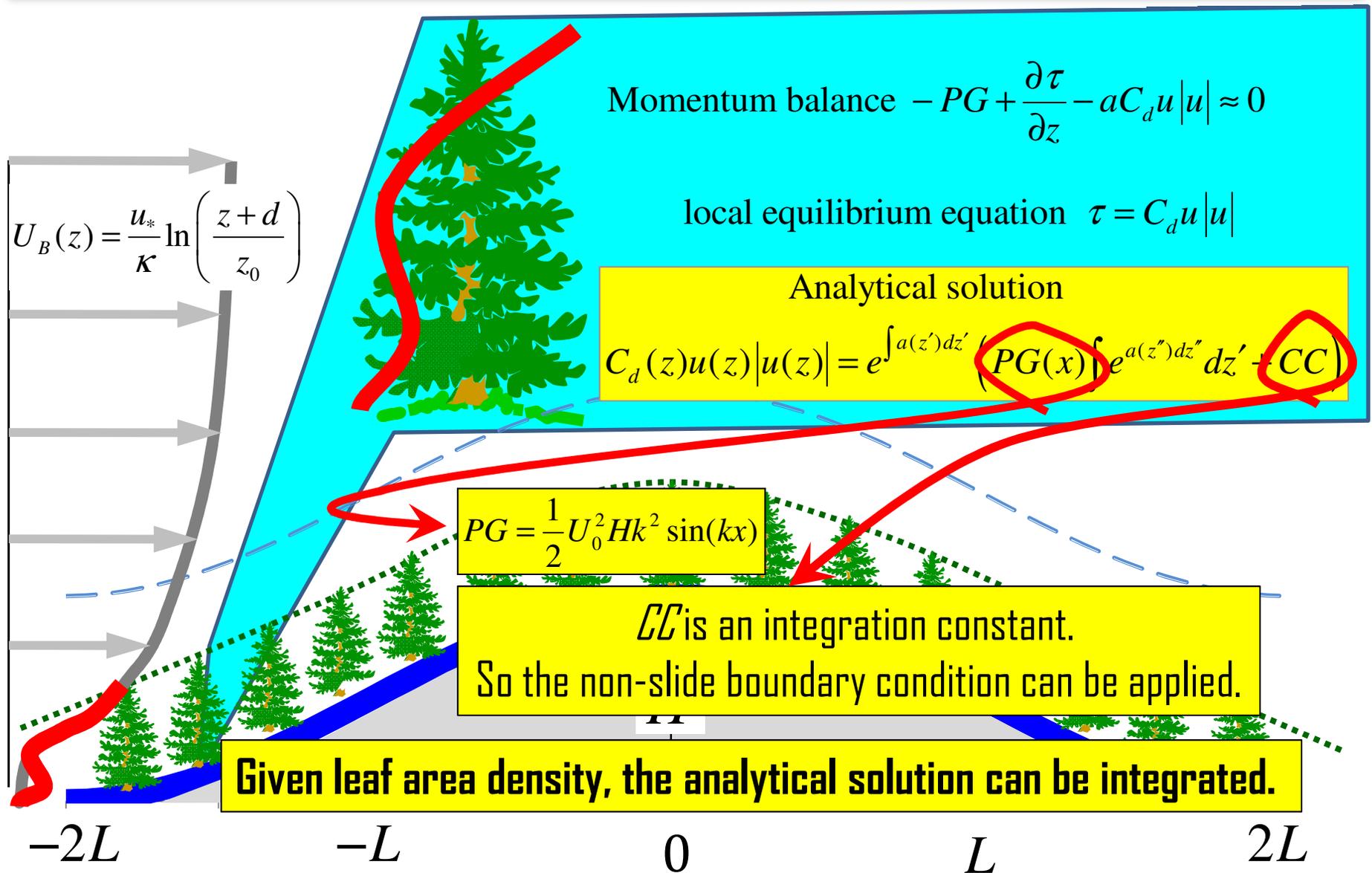


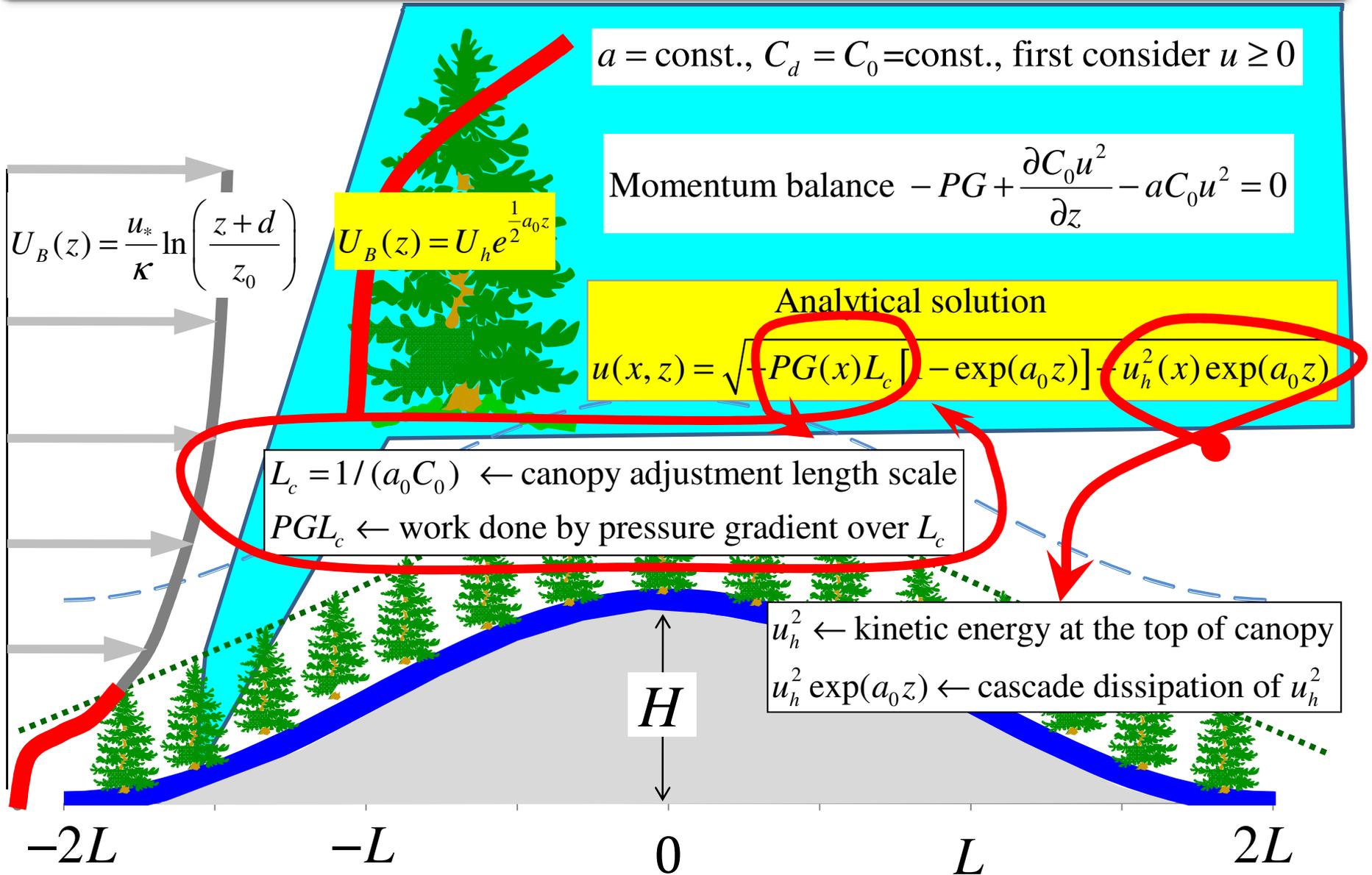
Fig. 7 Profiles of (a) mixing length ( $L_m$ ) and (b) :

# A new nonlinear model – forested hill



Our model can do  
what FB04 can do,  
but even better!

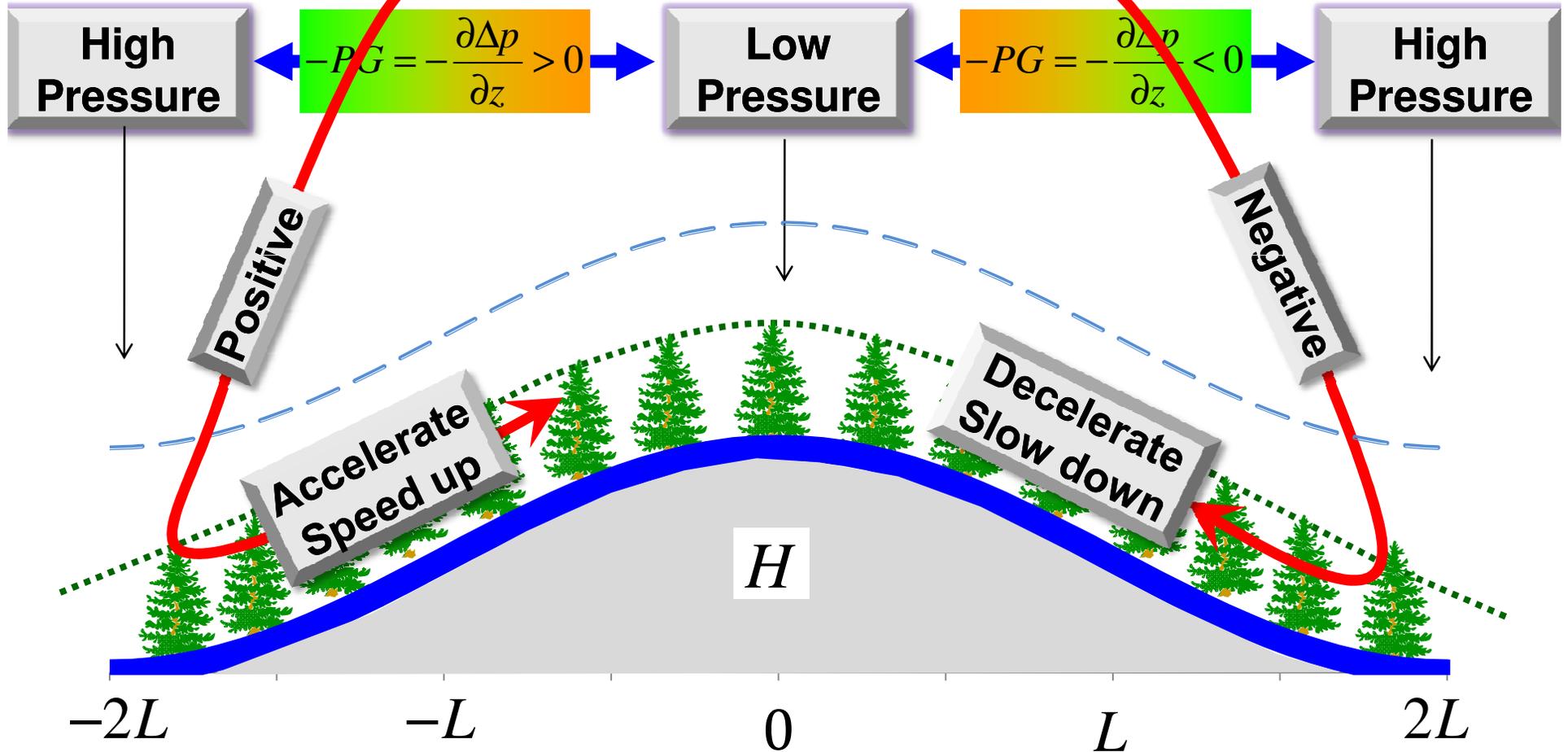
# A new nonlinear model – uniform vegetation



# A new nonlinear model – uniform vegetation

Analytical solution

$$u(x, z) = \sqrt{-PG(x)L_c} [1 - \exp(a_0 z)] + u_h^2(x) \exp(a_0 z)$$



# A new nonlinear model – uniform vegetation

Analytical solution

$$u(x, z) = \sqrt{-PG(x)L_c} [1 - \exp(a_0 z)] + u_h^2(x) \exp(a_0 z)$$

$$u(x, z_d) = \sqrt{-PG(x)L_c} [1 - \exp(a_0 z_d)] + u_h^2(x) \exp(a_0 z_d) = 0$$

$$Z_d(x) = \frac{1}{a_0} \ln \left( \frac{PG(x)L_c}{u_h^2(x) + PG(x)L_c} \right)$$

Recirculation region

$Z_d =$  separation level

$u > 0$

$u < 0$

$-PGL_c$  is Negative on leeward side

$H$

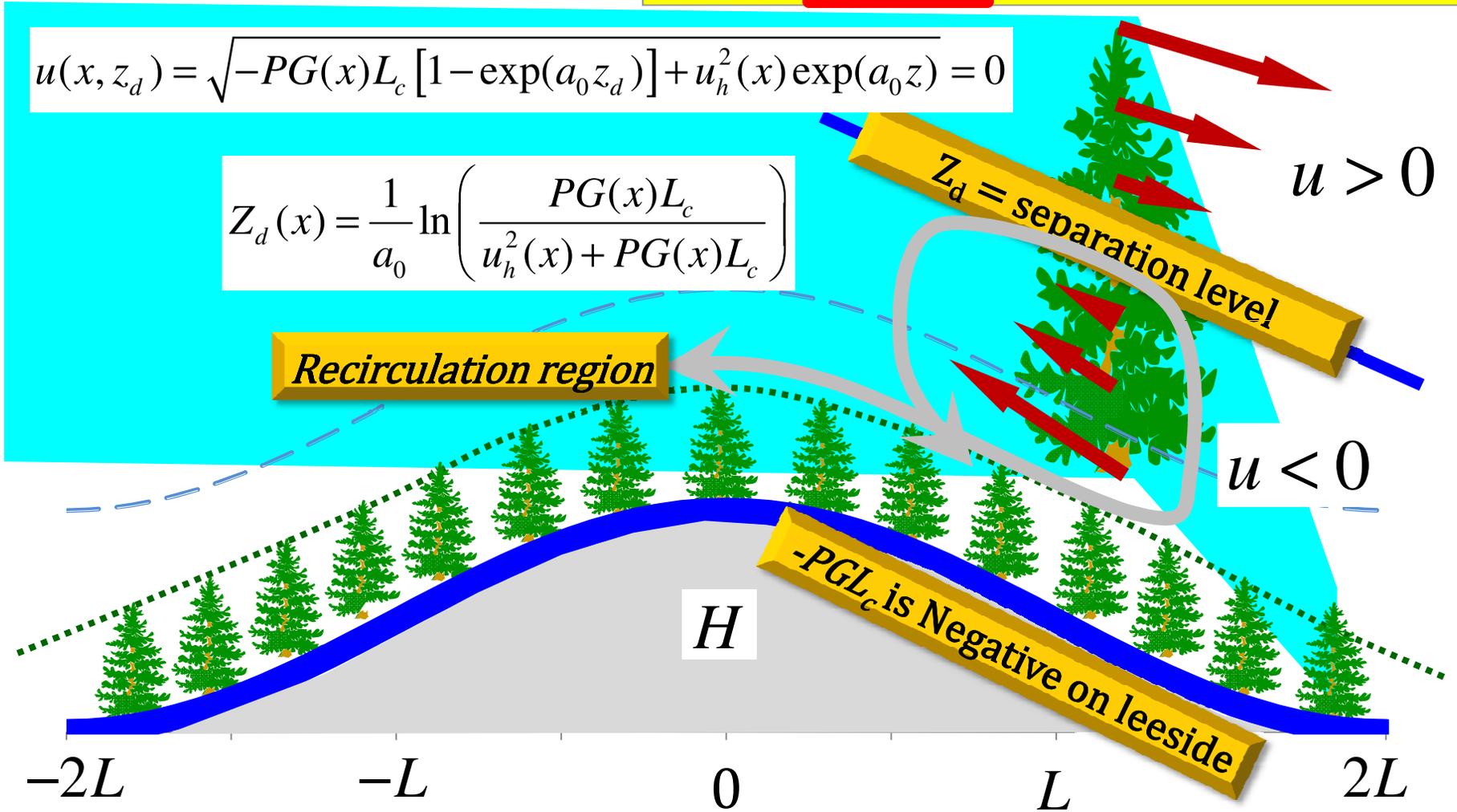
$-2L$

$-L$

$0$

$L$

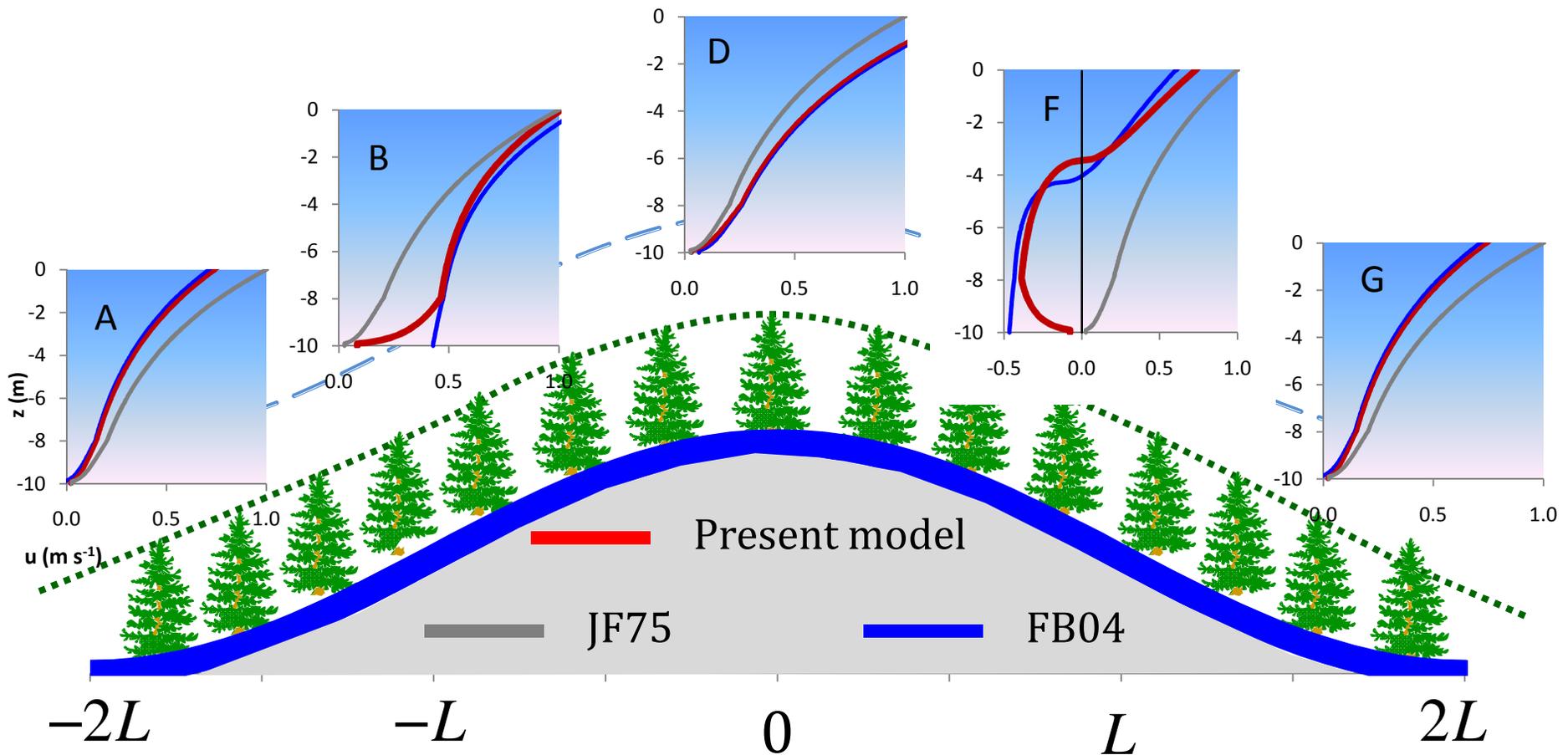
$2L$



# A new nonlinear model – uniform vegetation

Excellent agreement between FBO4 and present model at the crest and troughs.

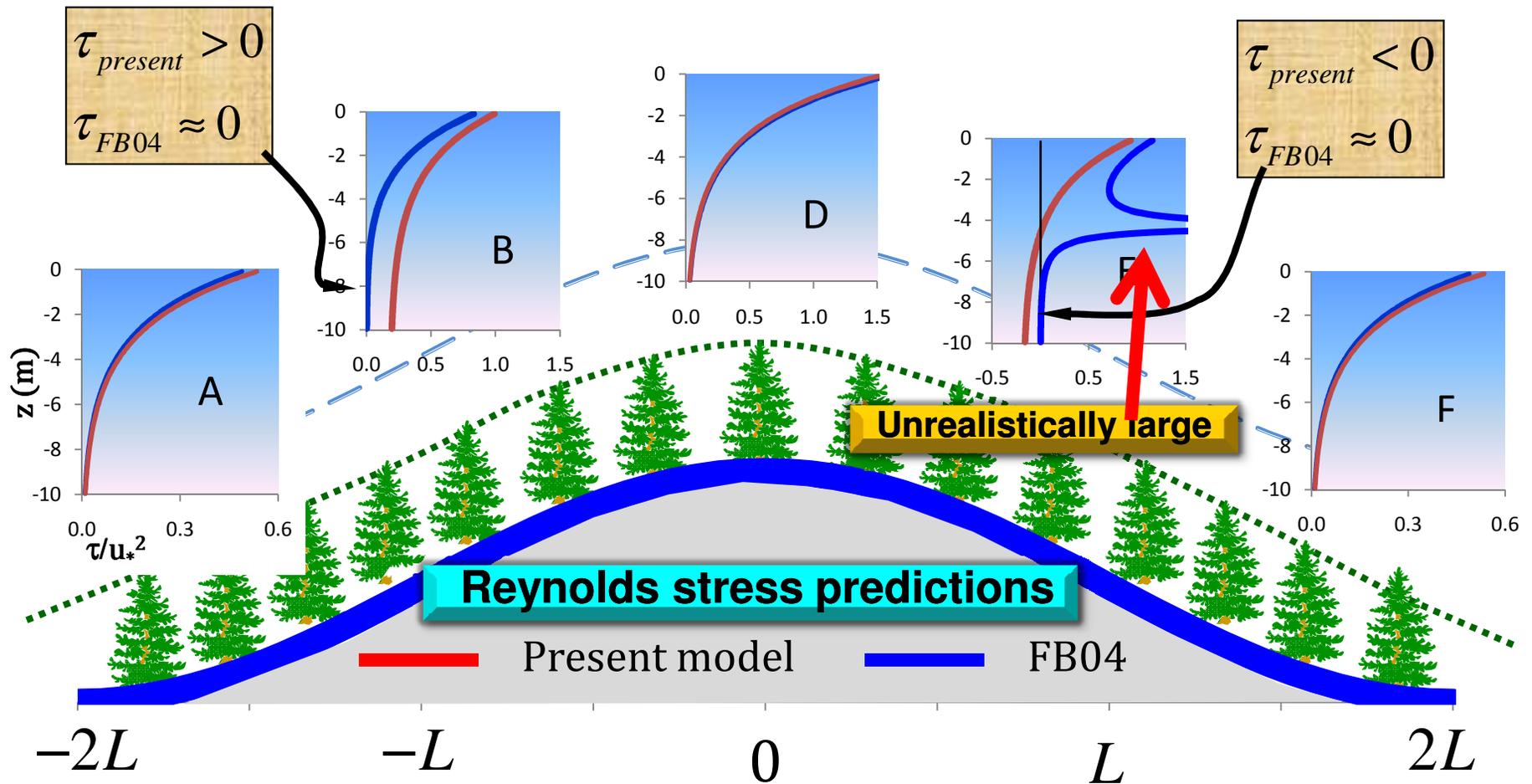
The **S-shaped** wind profile on windward side and **C-shaped** wind profile on leeward side are predicted by the new model rather than by FBO4.



# A new nonlinear model – uniform vegetation

Excellent agreement at the crest and trough

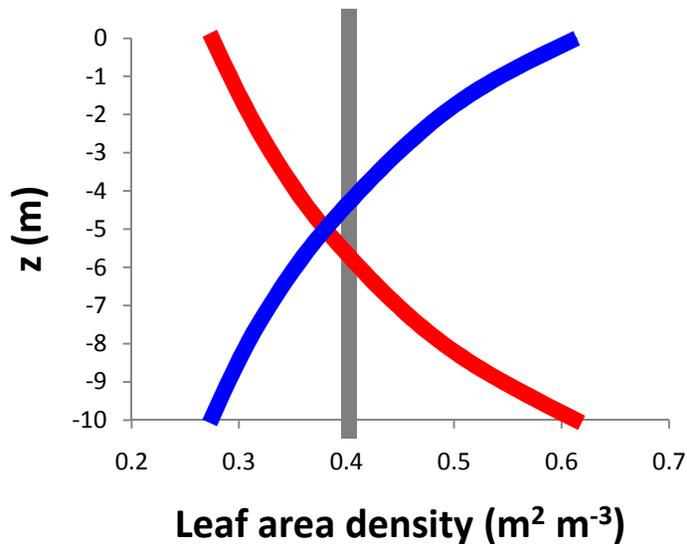
Different on windward and leeward sides



Our model can do  
what FB04 cannot do!

- Varying leaf area density
- Varying drag coefficient

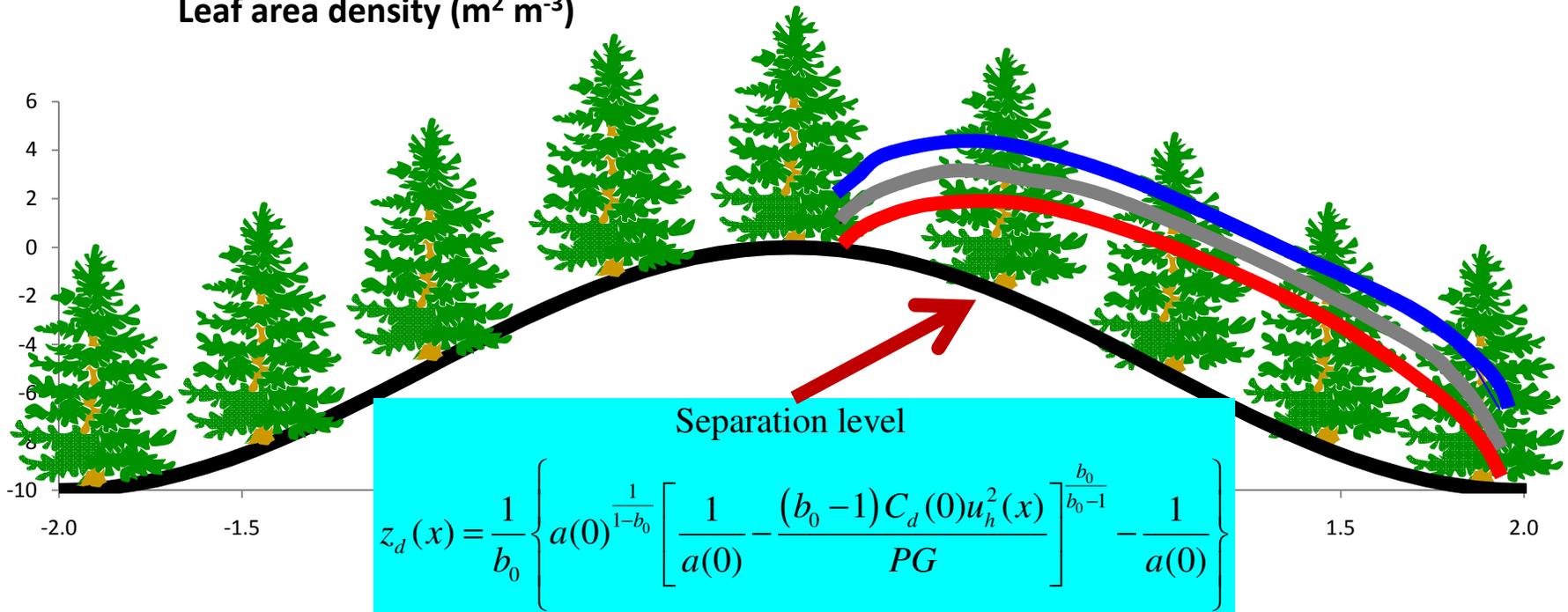
# A new nonlinear model – varying LAD



$LAI = 4.0$  for all examples  
 $a_0 = \text{const.} = 0.4 \rightarrow E_1$  black

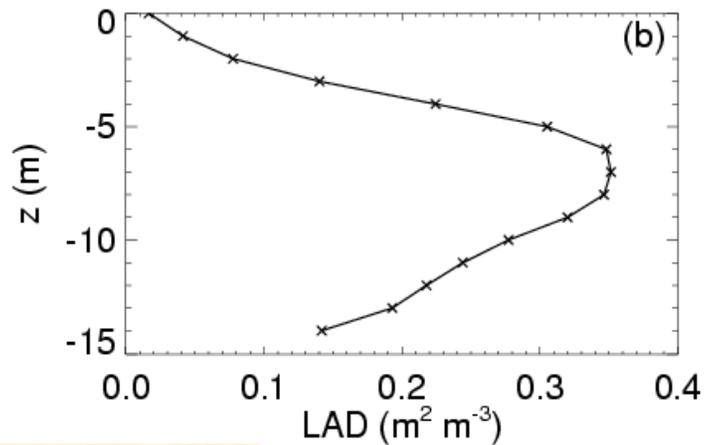
leaf area density  $\rightarrow a = \frac{1}{b_0(z+h) + b_1}$

$\left\{ \begin{array}{l} b_0 = -0.2, b_1 = 3.63 \rightarrow E_2 \text{ increasing function (blue)} \\ b_0 = 0.2, b_1 = 1.63 \rightarrow E_3 \text{ decreasing function (red)} \end{array} \right.$

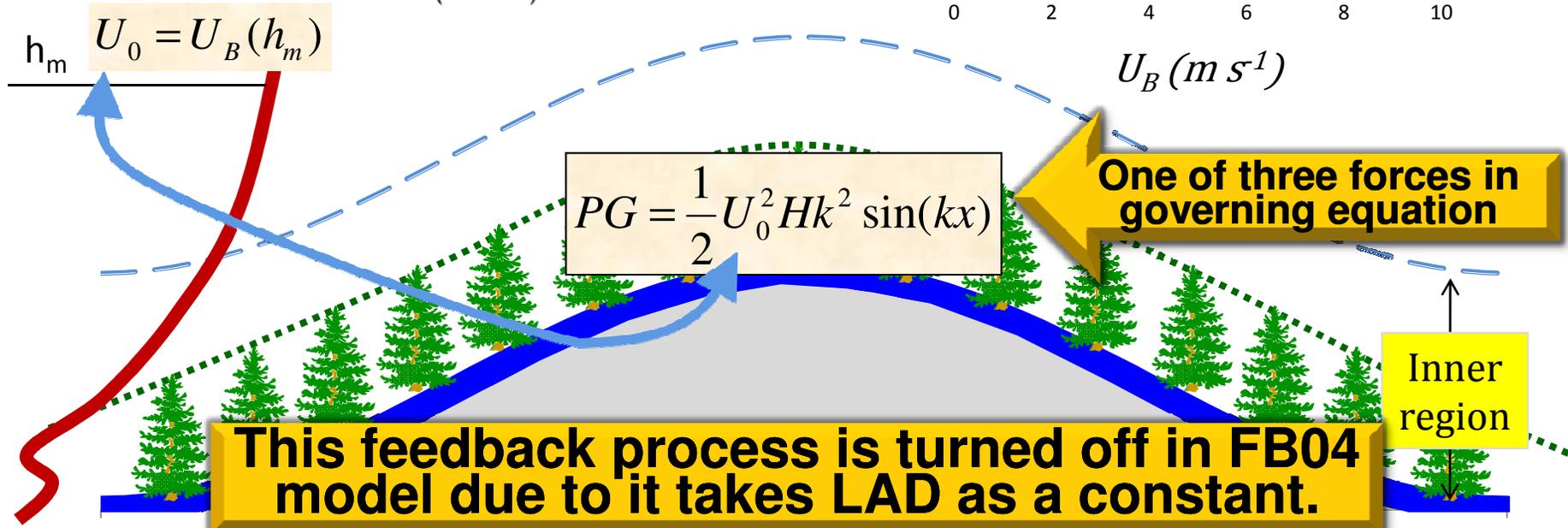
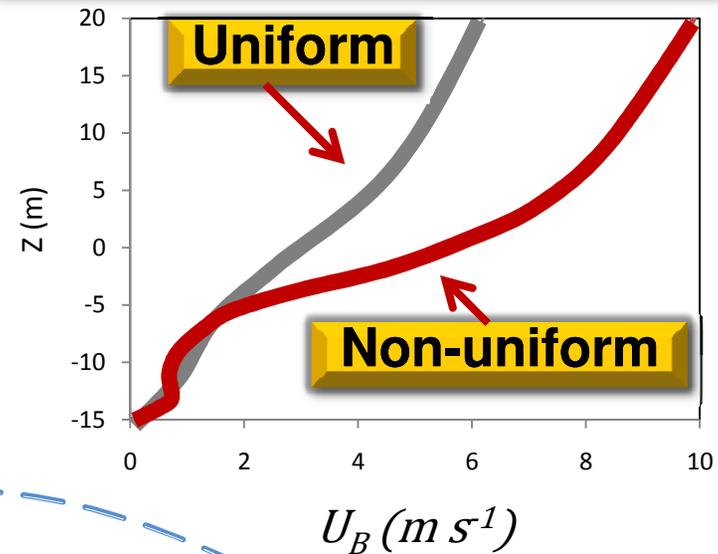


# What will be lost if we treat non-uniform LAD as uniform LAD?

Observed LAD at Niwot Ridge AmeriFlux site



Difference in basic state  $U_B$



## Summary and Conclusion

**Following weaknesses of FB04 have been improved!**

- **Physical inconsistency** -- Constant mixing-length assumption leading to a varying mixing-length.
- **A non-slip boundary condition** is not able to apply to the nonlinear algebraic equation.
- It is unnecessary to divide a canopy layer into **two layers**: a linear layer and a nonlinear layer.
- No need to assume  $\Delta u \ll U_B$

**The new model is simpler but more useful!**

- Separation level prediction
- Perform feedback - varying LAD  $\rightarrow$  changing  $U_B$  in outer region  $\rightarrow$  affecting PG in the inner region  $\rightarrow$  modifying momentum balance in canopy layer

**Thank You!**