

# Hurricane Sea-to-Air Heat Transfer

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## Hurricane Sea-to-Air heat fluxes:

- from  $C_E$  - 100 W/m<sup>2</sup> to 1000 W/m<sup>2</sup>
- from precipitation – 100,000 W/m<sup>2</sup>
- from sea cooling – 100,000 W/m<sup>2</sup>

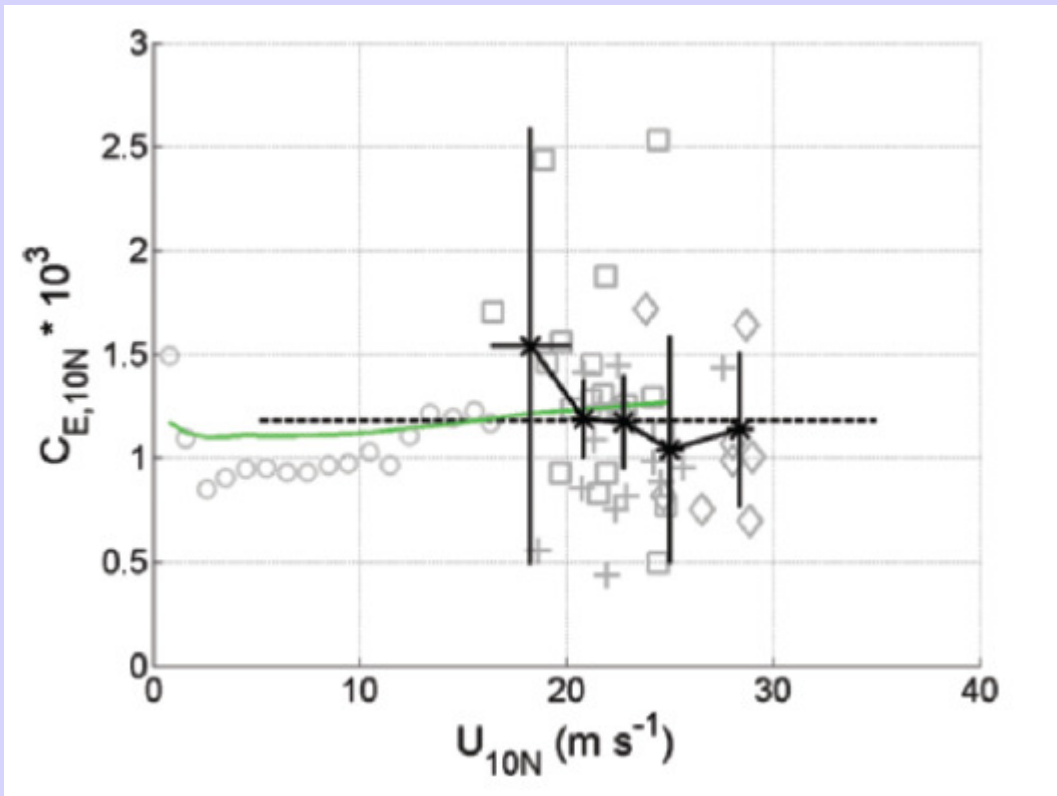
## Outline:

- Review of calculation methods
- Spray heat transfer
- Eddy correlation
- Evidence in favor of high heat flux

## Heat flux calculated from heat transfer equation

### Dalton Coefficient

$$C_E = 0.00118$$



Note figure from: Black et al. BAMS March 2007

### Heat Transfer Equation

$$Q_a = \rho C_E (h_s - h_a) u$$

#### Tropical sea light wind

for SST=25.5°C, P=100 kPa

$T_a = 24.5$ ,  $RH_a = 80\%$ ,

$h_s = 79000$ ,  $h_a = 64800$  J/kg

$u = 5$  m/s

$$Q_a = 100 \text{ W/m}^2$$

#### Hurricane eyewall

for: SST = 26°C, P = 95 kPa

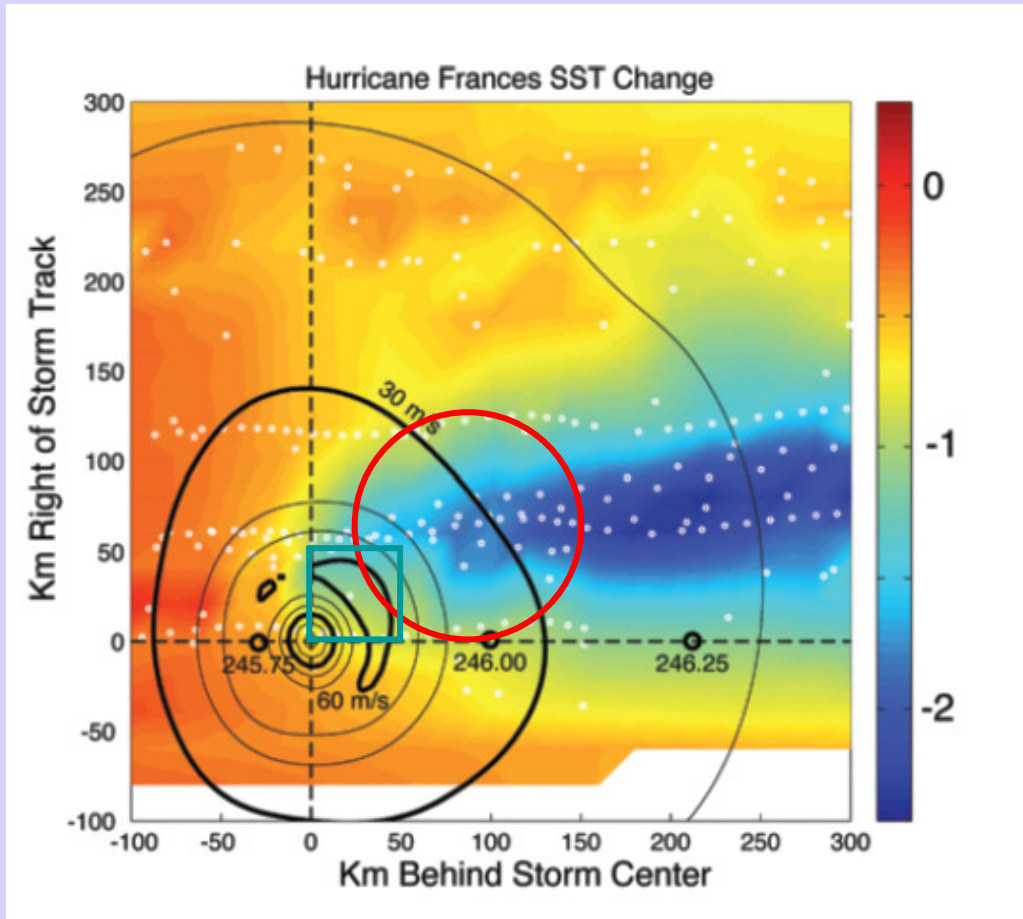
$T_a = 24.5$ ,  $RH_a = 95\%$ ,

$h_s = 84200$ ,  $h_a = 74800$  J/kg

$u = 50$  m/s

$$Q_a = 600 \text{ W/m}^2$$

## Heat flux from rain and sea cooling



### From rain

$$Q_v = L_v m d^2 (\pi/4)$$

for:  $m = 10 \text{ mm/hr}$  ( $0.0028 \text{ kg/s m}^2$ )

$d = 300 \text{ km}$

$$Q_v = 491 \text{ TW}$$

### From sea cooling

$$Q_t = C_w \Delta T w d v$$

for:  $\Delta T = 2.5^\circ\text{C}$ ,  $d = 100 \text{ m}$

$w = 100 \text{ km}$ ,  $v = 5 \text{ m/s}$

$$Q_t = 524 \text{ TW}$$

### Per unit spray production area

$$Q_e = Q / A$$

for:  $Q = 500 \text{ TW}$ ,  $A = 2500 \text{ km}^2$ ,

$L = 50 \text{ km}$ ,  $w = 50 \text{ km}$

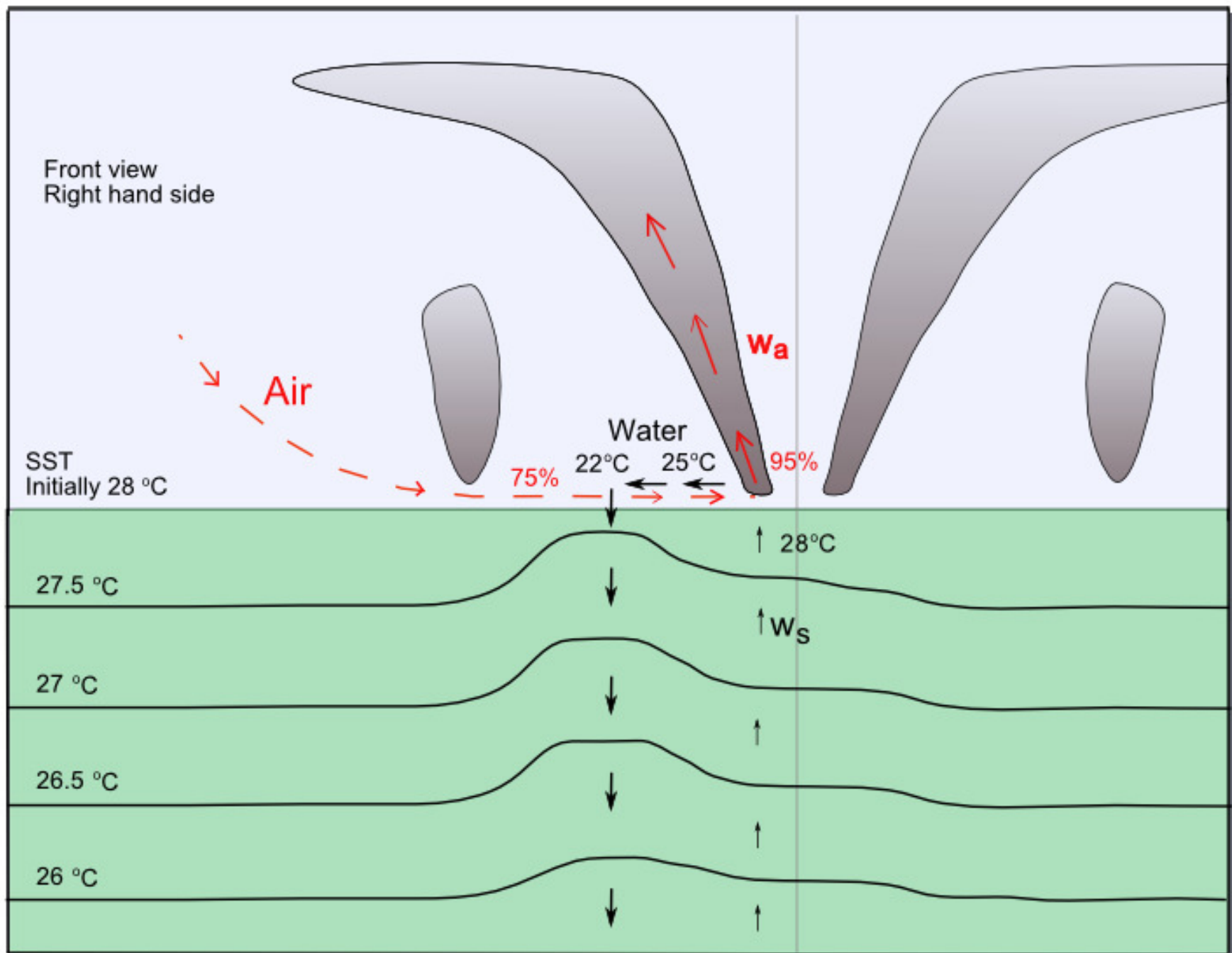
$$Q_e = 200,000 \text{ W/m}^2$$

### Per unit spray distribution area

$$Q_a = 40,000 \text{ W/m}^2$$

- $2500 \text{ km}^2$  green rectangle – Spray production area.
- $12,500 \text{ km}^2$  red circle – Spray deposition area.

# HURRICANE SEA COOLING PROCESS



## Hurricane Eyewall Isenthalpic air-water mixing

### Inlets

#### Water

$$T = 27.5 \text{ }^\circ\text{C}$$

$$m_l = 1606.2 \text{ g}$$

$$H = 185,080 \text{ J}$$

#### Air

$$P = 97 \text{ kPa}$$

$$T = 25 \text{ }^\circ\text{C}$$

$$U = 75 \%$$

$$m_a = 1 \text{ kg}$$

$$m_v = 15.7 \text{ g}$$

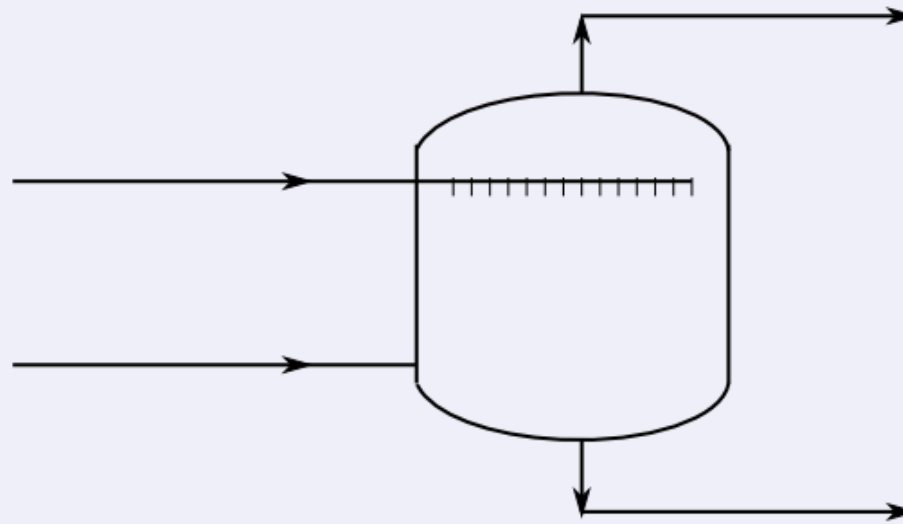
$$T_w = 21.7 \text{ }^\circ\text{C}$$

$$H = 65,160 \text{ J}$$

#### Total Inlets

$$m_w = 1621.92 \text{ g}$$

$$H = 250,240 \text{ J}$$



### Outlets

#### Air

$$P = 97 \text{ kPa}$$

$$T = 26 \text{ }^\circ\text{C}$$

$$U = 95 \%$$

$$m_a = 1 \text{ kg}$$

$$m_v = 21.2 \text{ g}$$

$$T_w = 25.4 \text{ }^\circ\text{C}$$

$$\rho = 1.12 \text{ kg/m}^3$$

$$H = 80,090 \text{ J}$$

#### Water

$$T = 25.4 \text{ }^\circ\text{C}$$

$$m_l = 1600.75 \text{ g}$$

$$H = 170,150 \text{ J}$$

#### Total Outlets

$$m_w = 1621.92 \text{ g}$$

$$H = 250,240 \text{ J}$$

$$\text{Heat transfer per unit mass air } (Q_m) = \underline{14,930 \text{ J}}$$

$$\text{Heat transfer per unit area: } w_a \approx \underline{2 \text{ m/s}}$$

From added vapor:

$$Q_a = \rho w_a Q_m = 1.12 * 2 * 14,930 \approx \underline{34,000 \text{ W/m}^2}$$

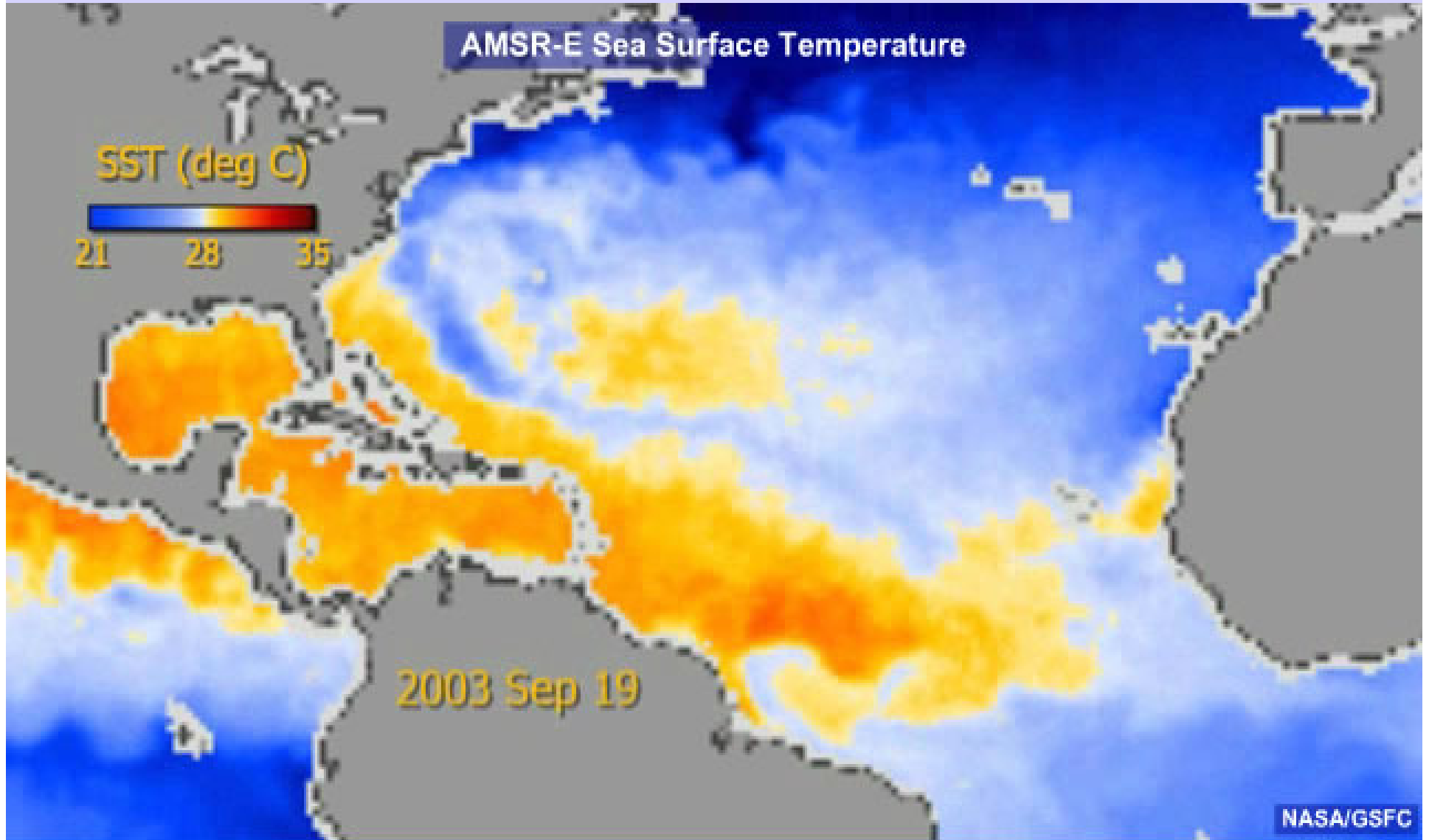
From total vapor

$$Q_t = \rho w m_v L_v = 1.12 * 2 * 21.2 * 2500 \approx \underline{120,000 \text{ W/m}^2}$$

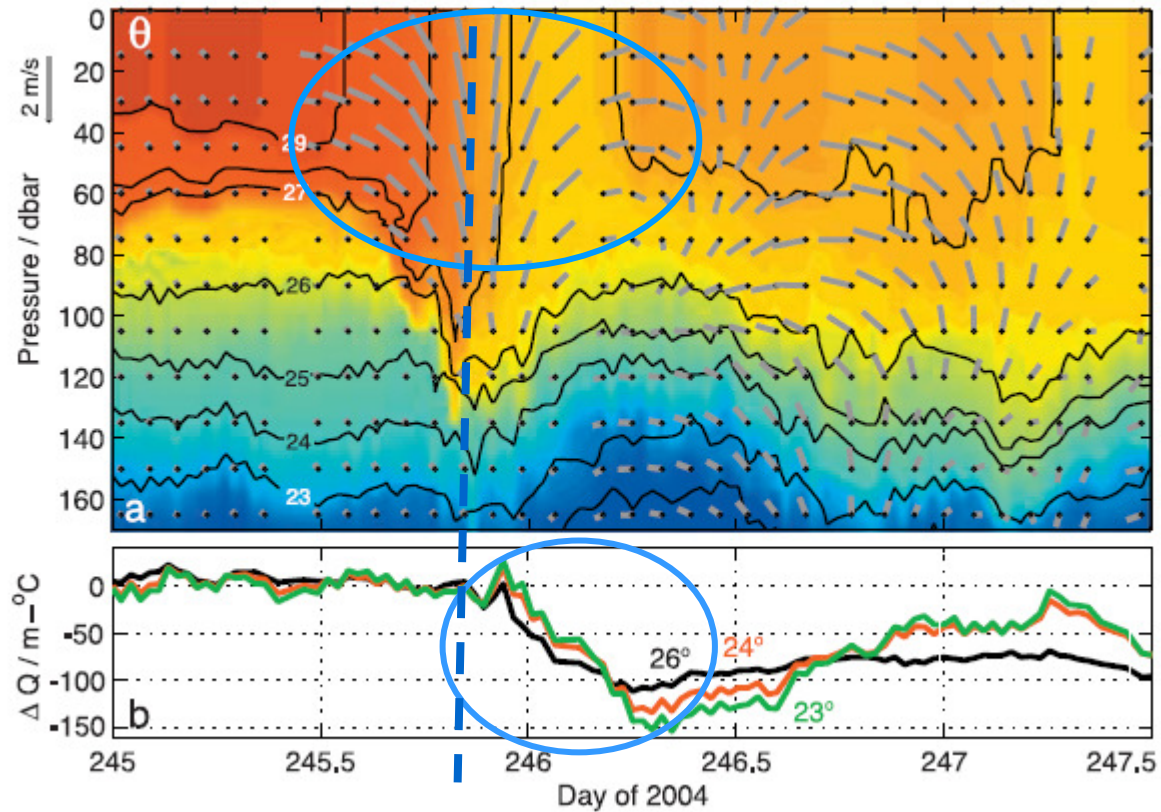
Eyewall Water Upflow ( $w_s$ )

$$w_s = \rho w_a m_l * 3.6 = 1.12 * 2 * 1.6 * 3.6 \approx \underline{12 \text{ m/hr}}$$

## Hurricane Isabel effect on sea surface temperature as observed from satellite



## Hurricane Frances sea temperature profile



From: D'Asaro et al. GRL 2007.

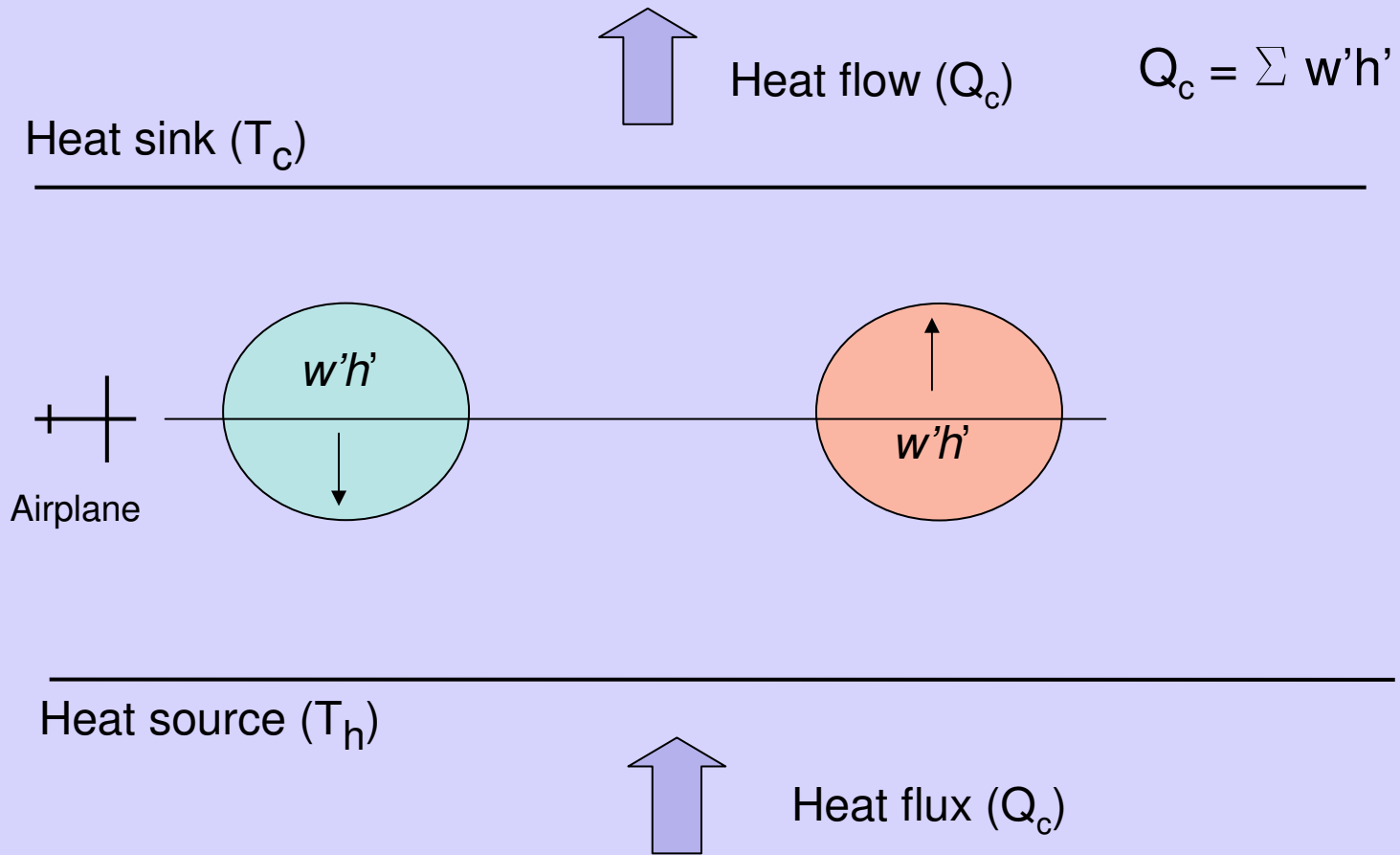
### Sea cooling:

- takes place during hurricane passage.
- is concentrated near the hurricane.
- extends to depths of 50 to 100 m.

### Notes:

- Blue ovals zone of high cooling.
- Blue dashes hurricane position

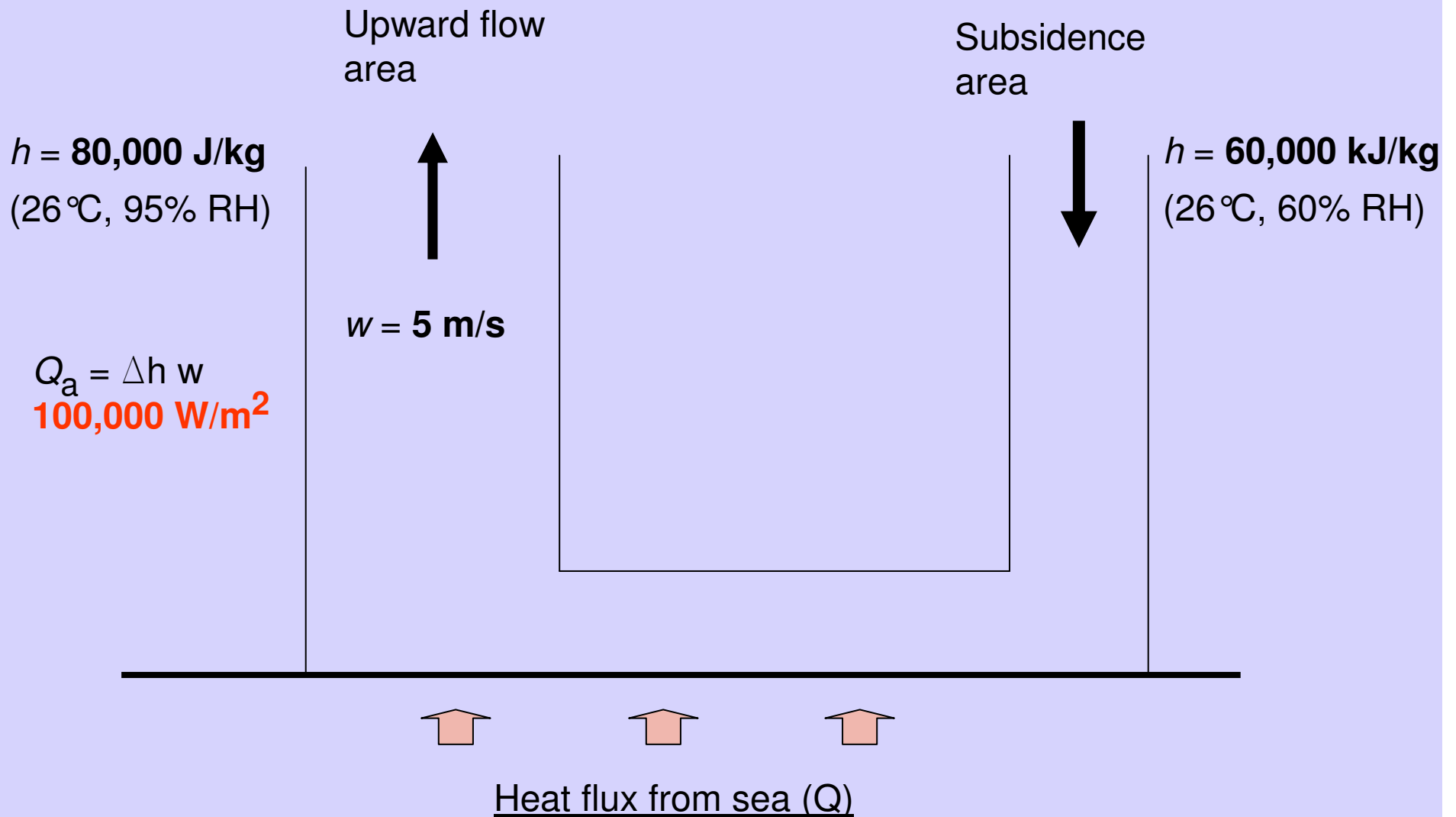
## Eddy correlation heat flux measurement principle



- Conditions must be uniform in horizontal direction.
- There must be no net convergence (LICOR).



## Steady-State Flow - Heat Flow Example



## What does Eddy Correlation see in the previous steady-state case?

$h = 80,000 \text{ J/kg}$   
 $w = 5 \text{ m/s}$

Hurricane  
area

Subsidence  
area

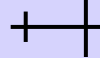
$h = 60,000 \text{ J/kg}$

### Heat Flux

$$Q_a = \Delta h w$$

$$100,000 \text{ W/m}^2$$

Sampled  
Drafts



$w$	3	7	m/s
$w'$	-2	+2	m/s
$h'$	-2	+2	kJ/kg
$h$	78	82	kJ/kg

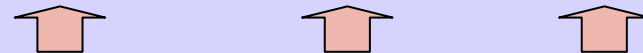
### Upflow Fluctuations

$$Q_c = \sigma \sum w'h'$$

$$Q_c = 0.2 * (2 * 2)$$

$$= 800 \text{ W/m}^2$$

Missed  
Drafts



Heat flux from sea (Q)

## Effect of mean upward velocity on heat flux

Mean upward velocity  
contribution

Eddy correlation  
contribution

$$Q = \bar{m} m_v L_v + \Sigma w'h'$$

$$Q = \rho \bar{w} m_v L_v + \Sigma w'h'$$

$$Q = 1.0 \times 2 \times 20 \times 2500 + 0.2 (2 \times 2 \times 1000)$$

$$Q = 100,000 + 800 = 100,800 \text{ W/m}^2$$

## Possible Sea-to-air heat transfer equation new form

$Q_i$  - Previous  
**Interfacial**  
term

$Q_s$  - New  
**Spray**  
term

$$Q = \rho C_E (h_s - h_a) (u + C_s u^5)$$

where:

$$C_e = 1.18 * 10^{-3}$$

$$C_s = 2.6 * 10^{-5}$$

### Sample heat Fluxes

<u>Velocity</u> w (m/s)	<u>Interfacial</u> $Q_i$ (W/m <sup>2</sup> )	<u>Spray</u> $Q_s$ (W/m <sup>2</sup> )
50	<b>600</b>	<b>100000</b>
40	484	32800
25	302	3125
10	121	32
5	<b>60</b>	<b>1</b>

## Rough Estimate of Convective Sea-to-Air Heat Fluxes

	<u>Average (W/m<sup>2</sup>)</u>	<u>Total (PW)</u>
Entire Earth	102	52
Land	102	16
Sea	<b>102</b>	<b>36</b>
Sea interfacial (Dalton Equation)	<b>72</b>	<b>25</b>
Sea Spray - Tropical Cyclones	<b>&gt;10,000</b>	<b>2</b>
Sea Spray - non tropical cyclone spray	<b>&lt;10,000</b>	<b>9</b>

## Further of evidence in favor of high sea to air heat flux hypothesis

- The heat content of sea water is much greater than that of air.
- Hurricanes significantly reduce the heat content of the sea.
- The heat content of the tropical air is not significantly reduced.
- The heat must come from the sea.
- Huge quantities of heat can be transferred from sea to air through isenthalpic mixing of spray and air.

### Thank you

More information available in forthcoming paper:  
On Hurricane Energy  
by: Louis M. Michaud  
in Meteorology and Atmospheric Physics

and at:  
[www.vortexengine.ca](http://www.vortexengine.ca)