

Introduction

A well-designed, closed-path eddy covariance (EC) system has good frequency response, needs little maintenance, and performs well in a variety of environmental conditions. The EC155 design was revised recently to include a Vortex Intake with a stainless steel sample cell. Each component influences overall system performance.

Objective

This work presents some of the system performance testing for the new EC155 design.



Dirty air enters the vortex chamber through a tangent port inducing vortex flow. Momentum ter where clean sample air is drawn.







Elora, Ontario, Canada

2016 the system was upgraded to the new vortex design.



Logan, Utah, USA

cell windows for the entire **307 day test** (Burgon, et al., 2015).

Extreme Dirty Air Performance

References

Eddy Covariance Systems with Vortex Intakes. A GU Fall Meeting 2015 Poster B33C-0669

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Performance Evaluation of an Innovative Sampling System for Closed Path Eddy Covariance Measurements

Rex Burgon^a, Steve Sargent^a, Benjamin Conrad^a ^aCampbell Scientific, Inc., USA

Thermal Damping

Background

Rannik, et al. (1997) used a simple, steady-state model to assess tubing length required to damp temperature fluctuations sufficiently to neglect the WPL (Webb, 1980) temperature term. They found the Reynolds number inside the tube to be an important factor, noted that fluctuations would damp more quickly than the steady state, and suggested the importance of experimental verification of physical intake tubes. Their Figure 3(a) showed L/D of 300 to be sufficient for the conditions that most closely describe the EC155. Their often referenced statement that L/D should be on the order of 1000 is a conservative upper bound on the tube length required, not a minimum requirement.

Temperature damping in the original EC155 intake/sample cell was measured by Sargent (2015), and was shown to reduce the sensible heat flux of the air within the sample cell compared to ambient by more than a factor of 100, even for cospectra with very low frequencies.

The new design includes two changes to further improve temperature damping: • An intake tube with a smaller ID (0.085" compared to 0.105"), giving a higher Reynolds number for better heat transfer from the air to the tube wall, increased L/D ratio (220 to 290), and more thermal mass (thicker wall) for increased damp-

- ing of fluctuations
- temperature before entering the sample cell

Method

The new design was tested using the method of Sargent (2015). A heat gun was directed at the inlet and cycled on and off for several cycles at a controlled period. Several test runs provided results over a series of frequencies. Fast response thermocouples measured temperatures of the inlet air, air in the cell, and the cell block. The cell used for thermal testing was modified to position a thermocouple (air) in the optical path.



Conclusions

- No delicate thermocouples exposed to sample air stream
- No complications related to weighting multiple dynamic thermocouple readings

System Frequency Response

System frequency response depends on details of the gas sampling components such as rain cap, filter and intake tube as well as flow rate (Aubinet, 2016). The new EC155 design replaces the filter with a vortex cleaner that splits the total flow (2 LPM bypass and 6 LPM sample). The original sample flow was 7 LPM. Frequency response performance was verified for both designs including the complete gas sampling systems.

Method

The technique of Sargent (2012) was used to measure frequency response. The otherwise steady CO₂ and H₂O concentrations were pulsed by injecting a short (< 5ms) burst of "tank" air into the sample flow just upstream of the rain cap. The system response was recorded at a sample rate of 50 Hz with a 25 Hz digital filter.

Conclusions

- Excellent system response, difference consistent with slight
- change in sample flow.
- New design cutoff frequency = 4.3 Hz• Original design cutoff frequency = 5.1 Hz

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• A heat-exchange passage milled into the sample cell block (large thermal mass) to bring the air even closer to the block



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