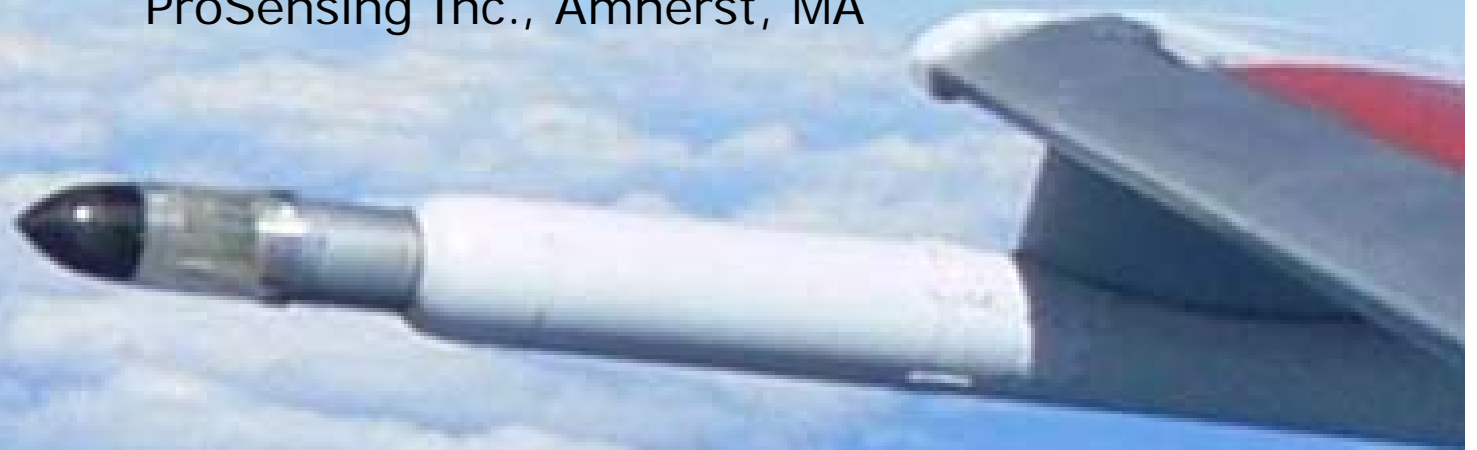


A COMPACT AIRBORNE KA-BAND PRECIPITATION PMS PROBE RADAR (KPR)

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ProSensing Inc., Amherst, MA



Background

- 2005: ProSensing developed a compact G-band (183 GHz) water Vapor radiometer (GVR) packaged in a standard PMS probe canister





GVR



Background (cont.)

- 2011-2013: ProSensing delivered six compact Ka-band (35 GHz) solid state range finding radars



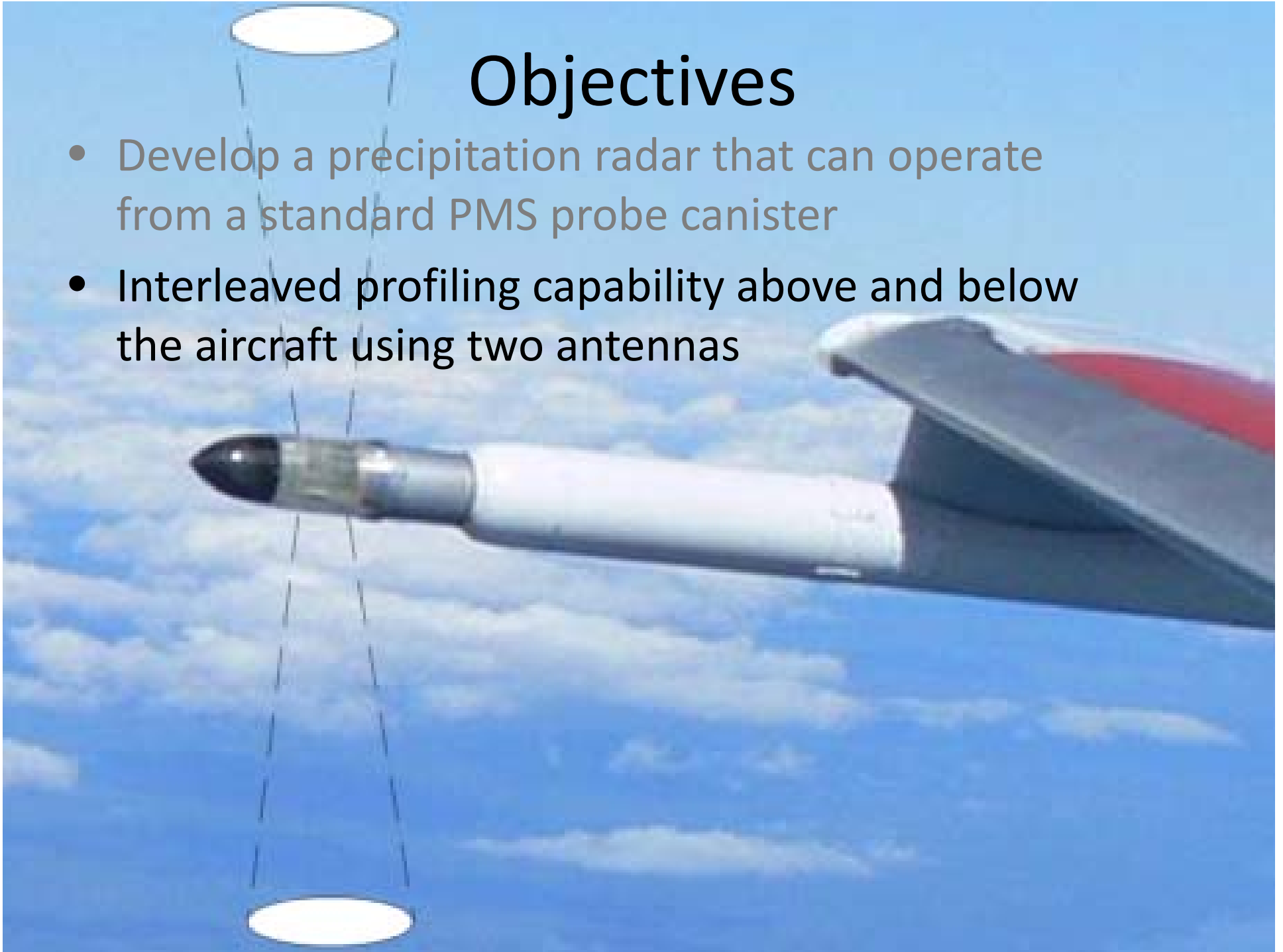
Objectives

- Develop a precipitation radar that can operate from a standard PMS probe canister



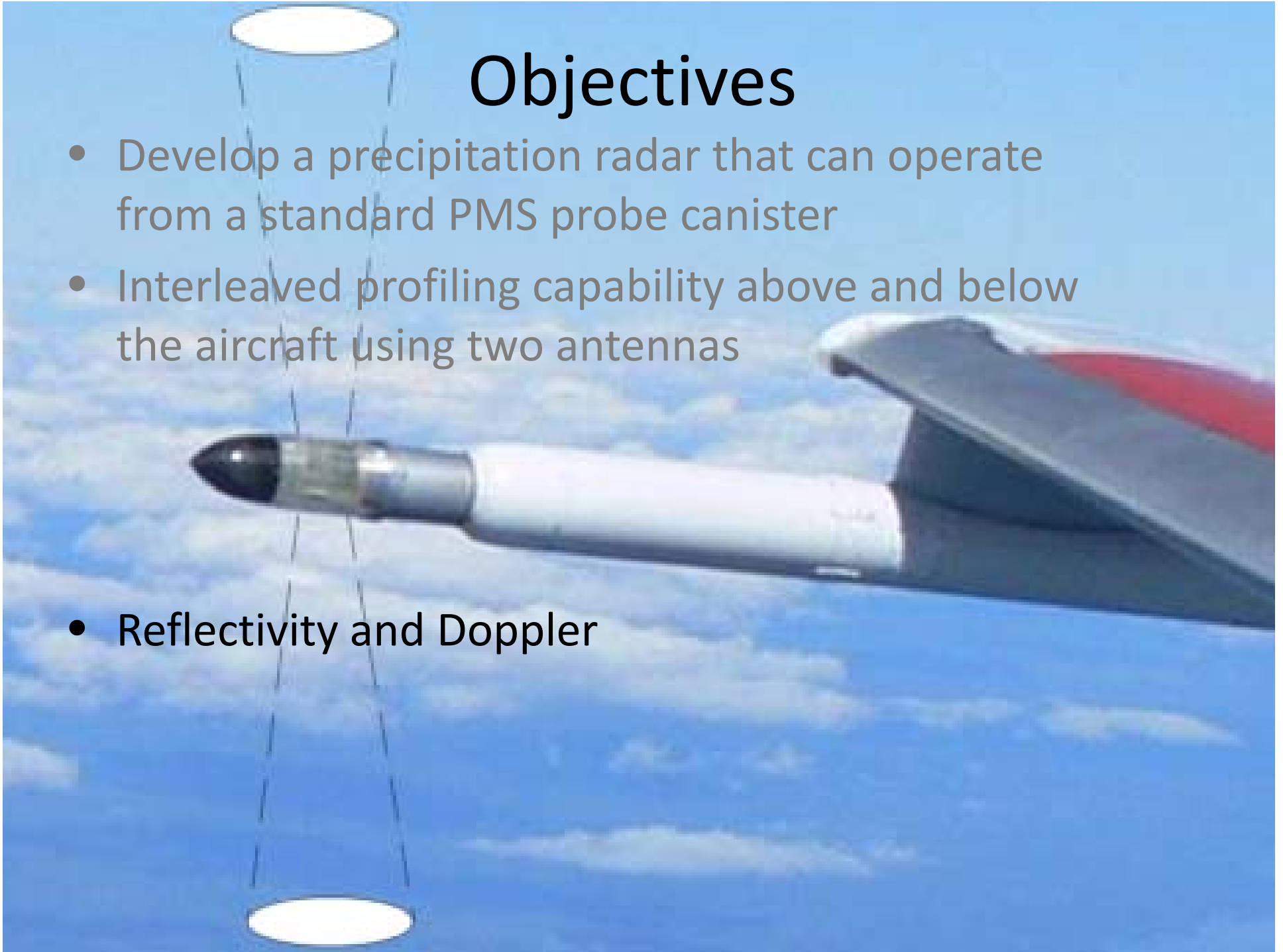
Objectives

- Develop a precipitation radar that can operate from a standard PMS probe canister
- Interleaved profiling capability above and below the aircraft using two antennas



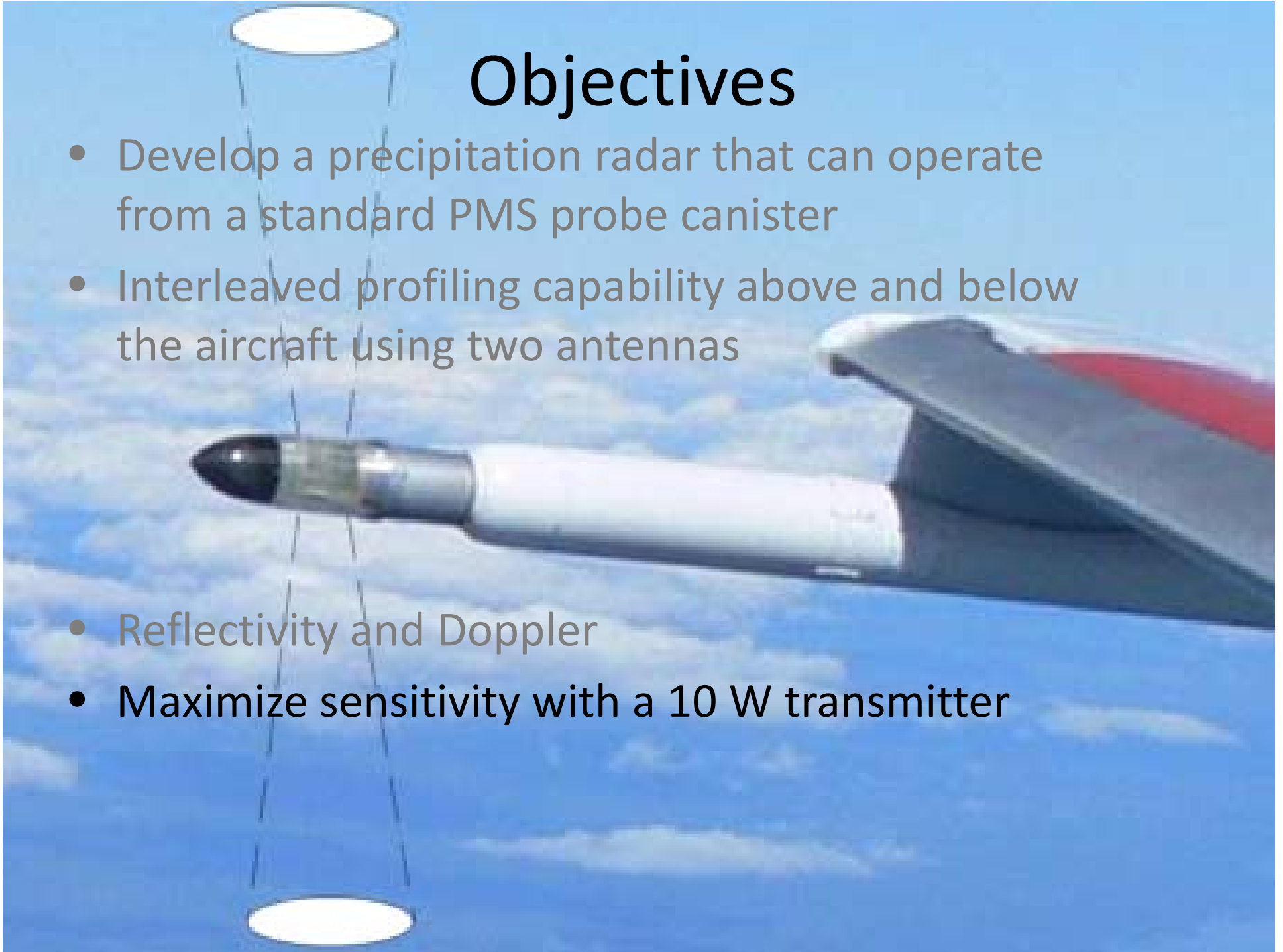
Objectives

- Develop a precipitation radar that can operate from a standard PMS probe canister
- Interleaved profiling capability above and below the aircraft using two antennas
- Reflectivity and Doppler



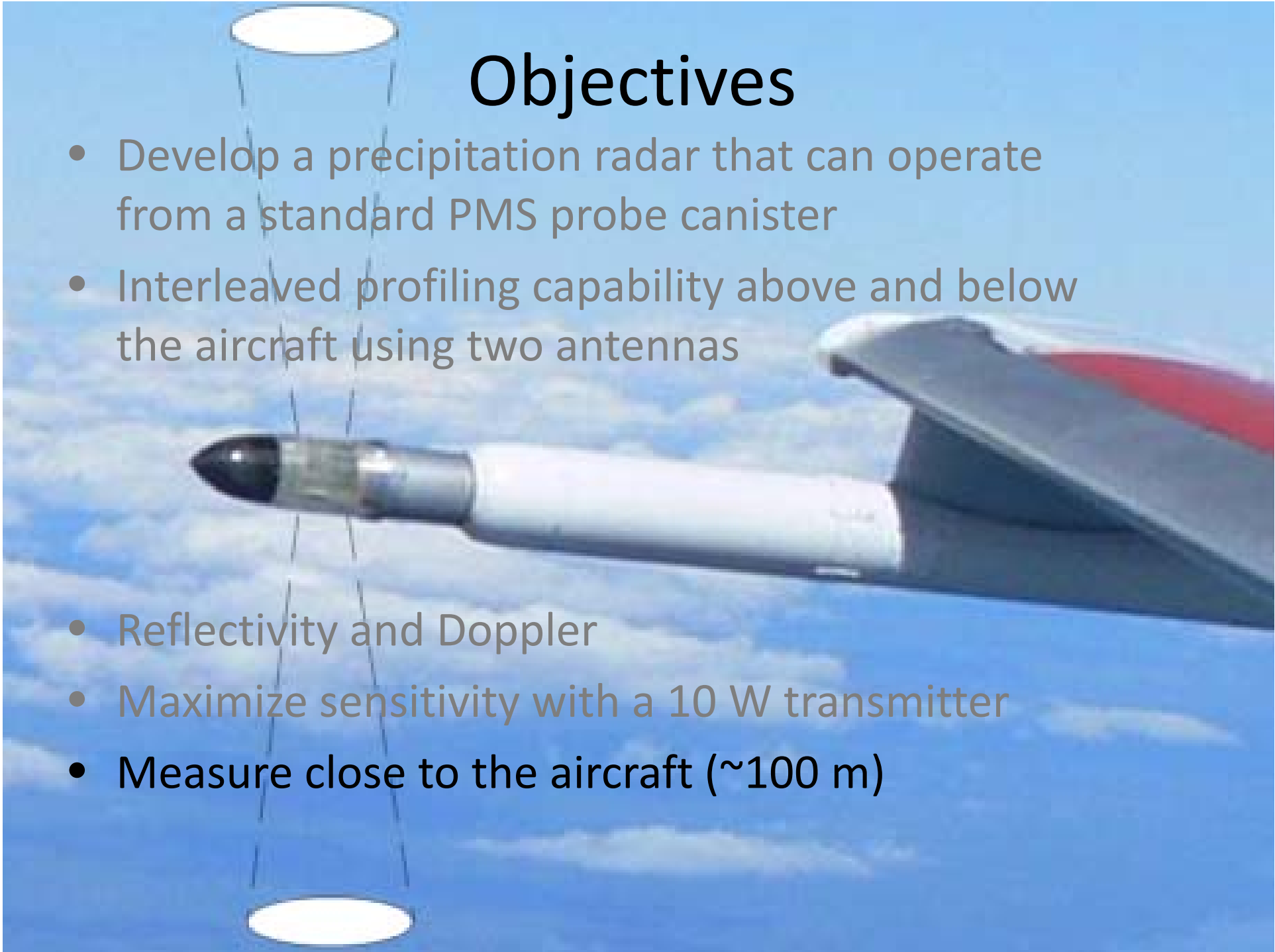
Objectives

- Develop a precipitation radar that can operate from a standard PMS probe canister
- Interleaved profiling capability above and below the aircraft using two antennas
- Reflectivity and Doppler
- Maximize sensitivity with a 10 W transmitter



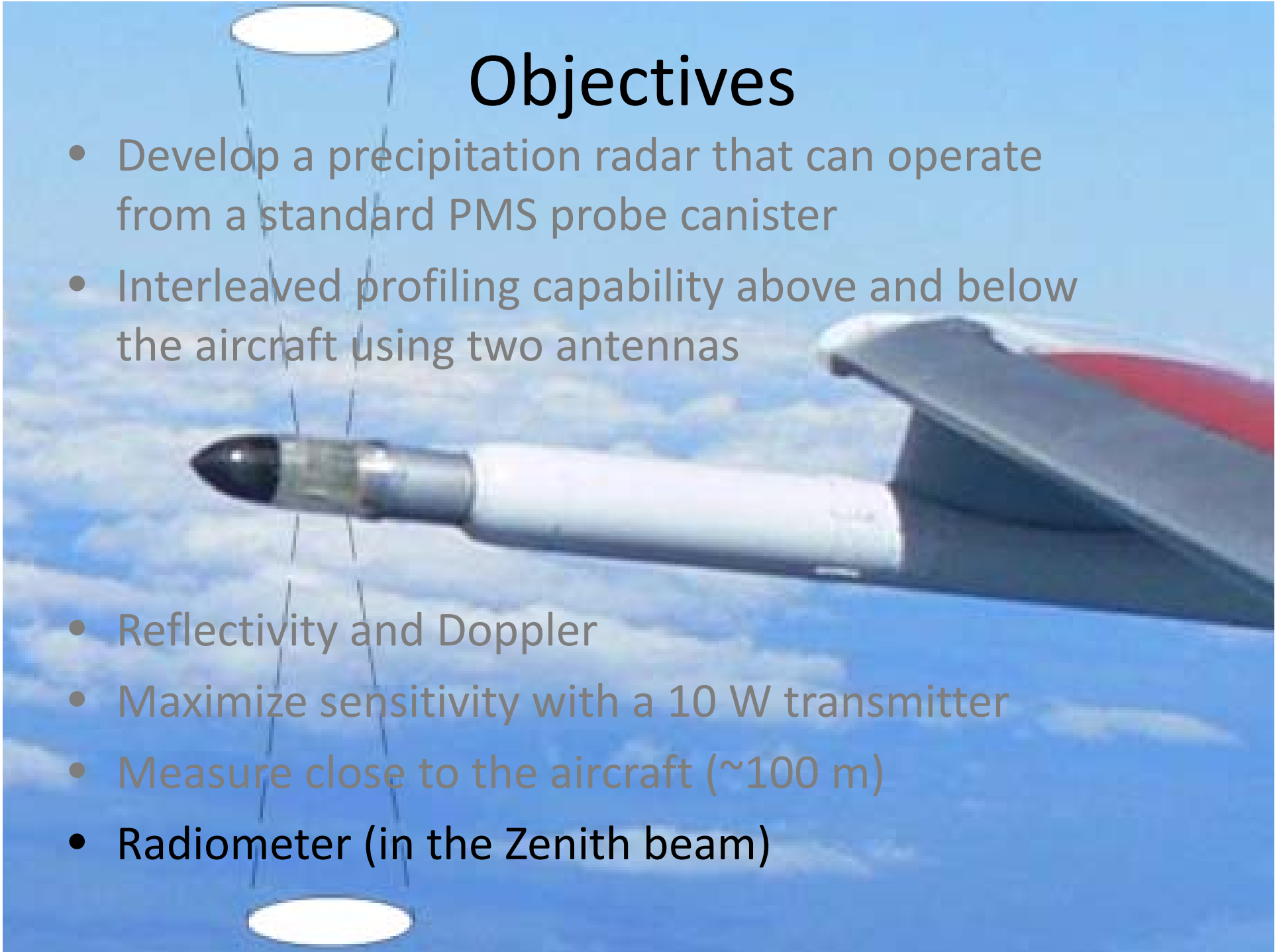
Objectives

- Develop a precipitation radar that can operate from a standard PMS probe canister
- Interleaved profiling capability above and below the aircraft using two antennas
- Reflectivity and Doppler
- Maximize sensitivity with a 10 W transmitter
- Measure close to the aircraft (~100 m)



Objectives

- Develop a precipitation radar that can operate from a standard PMS probe canister
- Interleaved profiling capability above and below the aircraft using two antennas
- Reflectivity and Doppler
- Maximize sensitivity with a 10 W transmitter
- Measure close to the aircraft (~100 m)
- Radiometer (in the Zenith beam)



Key Enabling Component

- Compact 10 W, pulsed, solid state Ka-band power amplifier



Size: 5"x3"x1"

Design Features

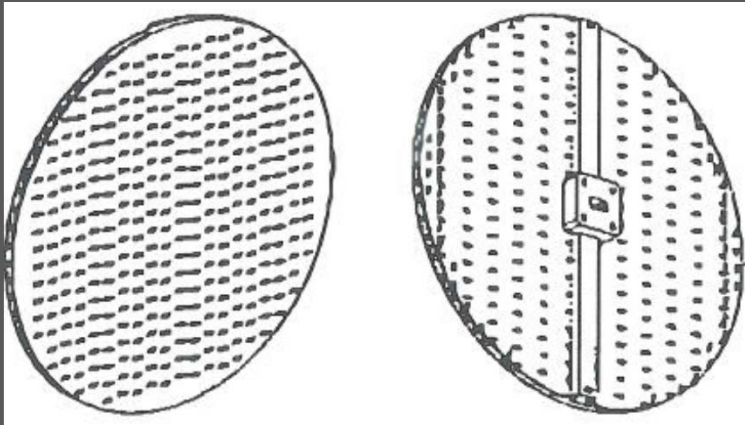
- Interleaved profiling capability above and below the aircraft using two antennas -> T/R switch network and dual-antennas



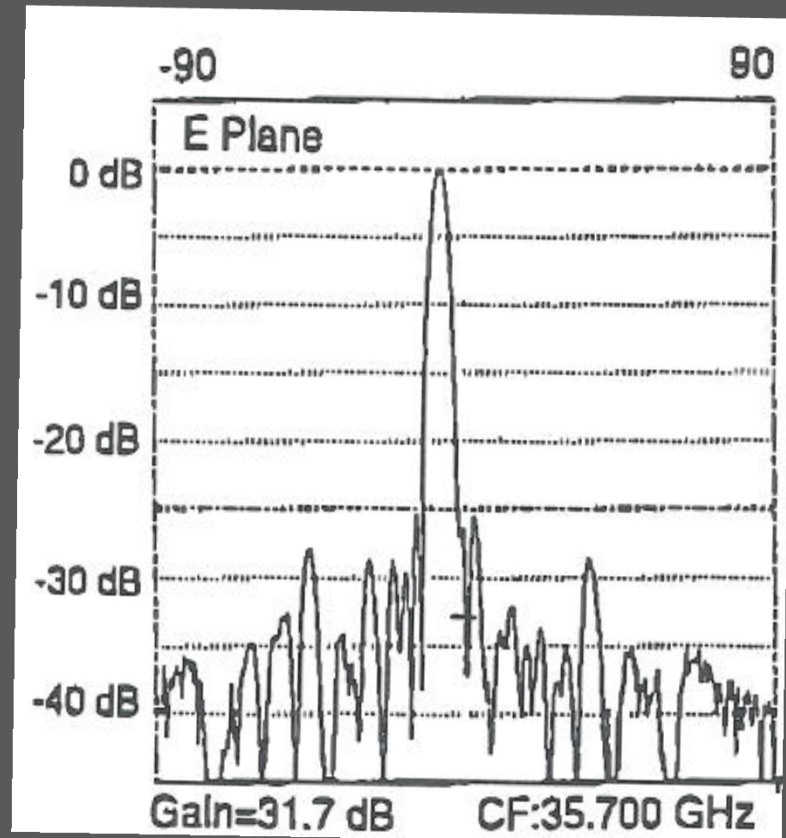
- ~ 0.2 dB loss per junction
- ~ 30 dB isolation per junction
- ~ 200 ns transition time
- 20 kHz max. PRF rate (40 kHz events)

Design Features

- Interleaved profiling capability above and below the aircraft using two antennas -> T/R switch network and dual-antennas



- Slotted Waveguide Array
- 35.5 – 35.9 GHz Freq. Range
- 4.2 Beamwidth
- 31.7 dB Gain



Design Features

- Interleaved profiling capability above and below the aircraft using two antennas -> T/R switch network and dual-antennas
- **Reflectivity and Doppler measurements -> Integrated Analog Devices ADIS16375 IMU**



- 3-axis gyroscope: $\pm 300^\circ/\text{sec}$
- 3-axis accelerometer: $\pm 5g$
- Temperature range: -40°C to $+105^\circ\text{C}$
- Bandwidth: 330 Hz; 2.4 kHz sampling

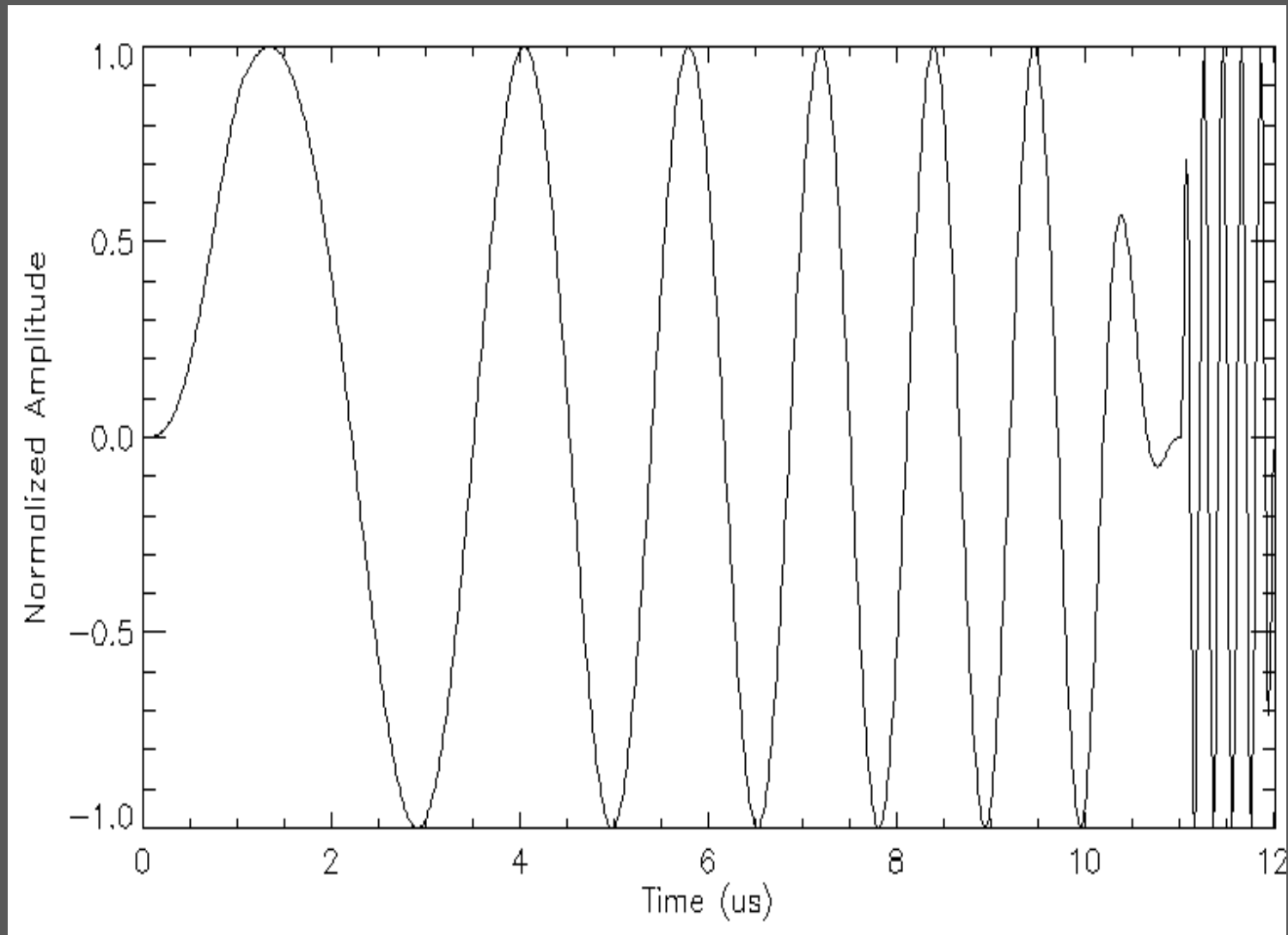
Design Features

- Interleaved profiling capability above and below the aircraft using two antennas -> T/R switch network and dual-antennas.
- Reflectivity and Doppler measurements -> Integrated Analog Devices ADIS16375 IMU
- Maximize sensitivity with a 10 W transmitter -> Pulse compression

Design Features

- Interleaved profiling capability above and below the aircraft using two antennas -> T/R switch network and dual-antennas
- Reflectivity and Doppler measurements -> Integrated Analog Devices ADIS16375 IMU
- Maximize sensitivity with a 10 W transmitter -> Pulse compression
- Measure close to the aircraft (~100 m) -> Combined offset frequency short/chirped TX pulse
Wide-band RF; dual-channel IF receiver and data system

Combined Chirp/Short pulse

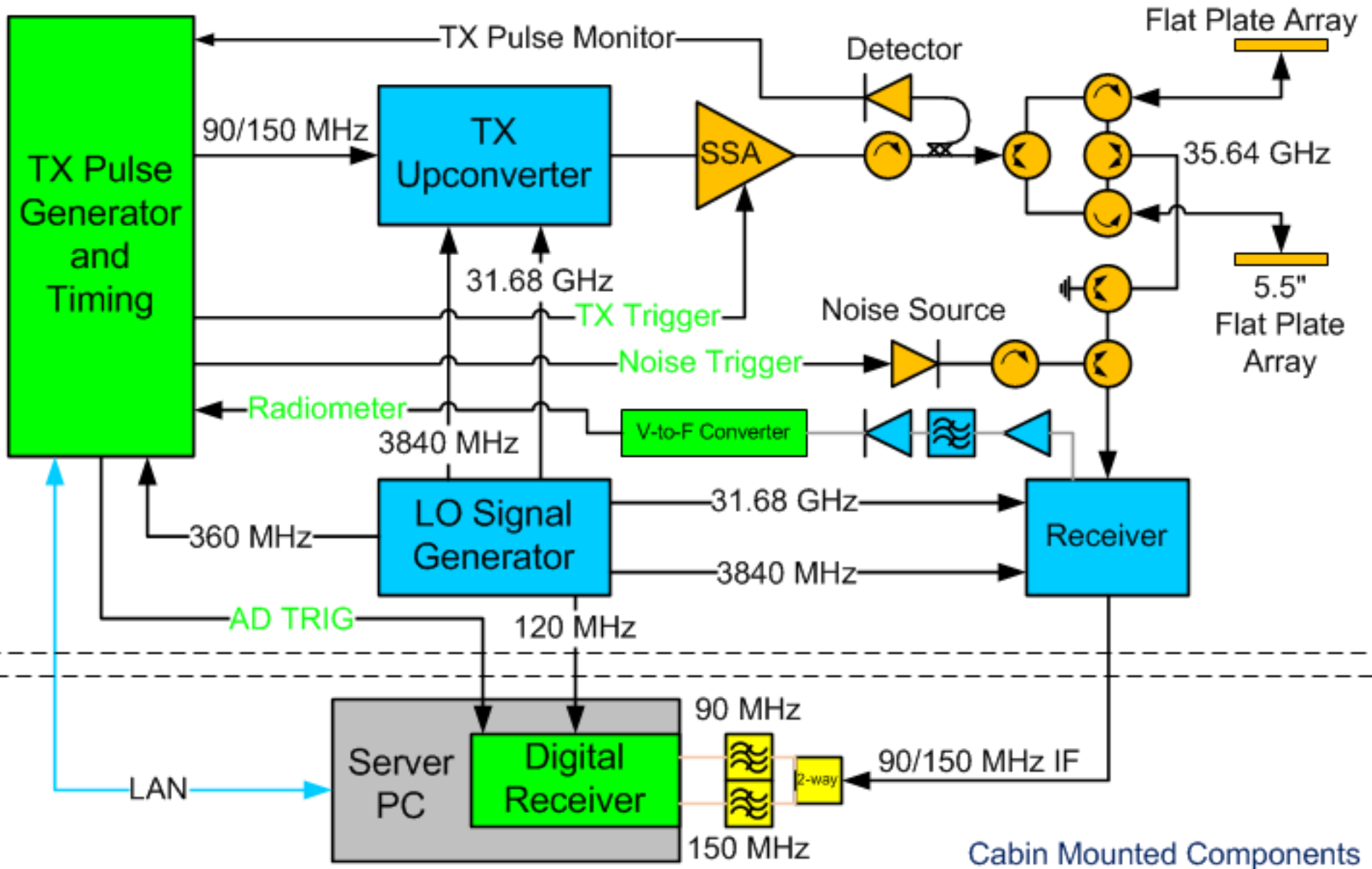


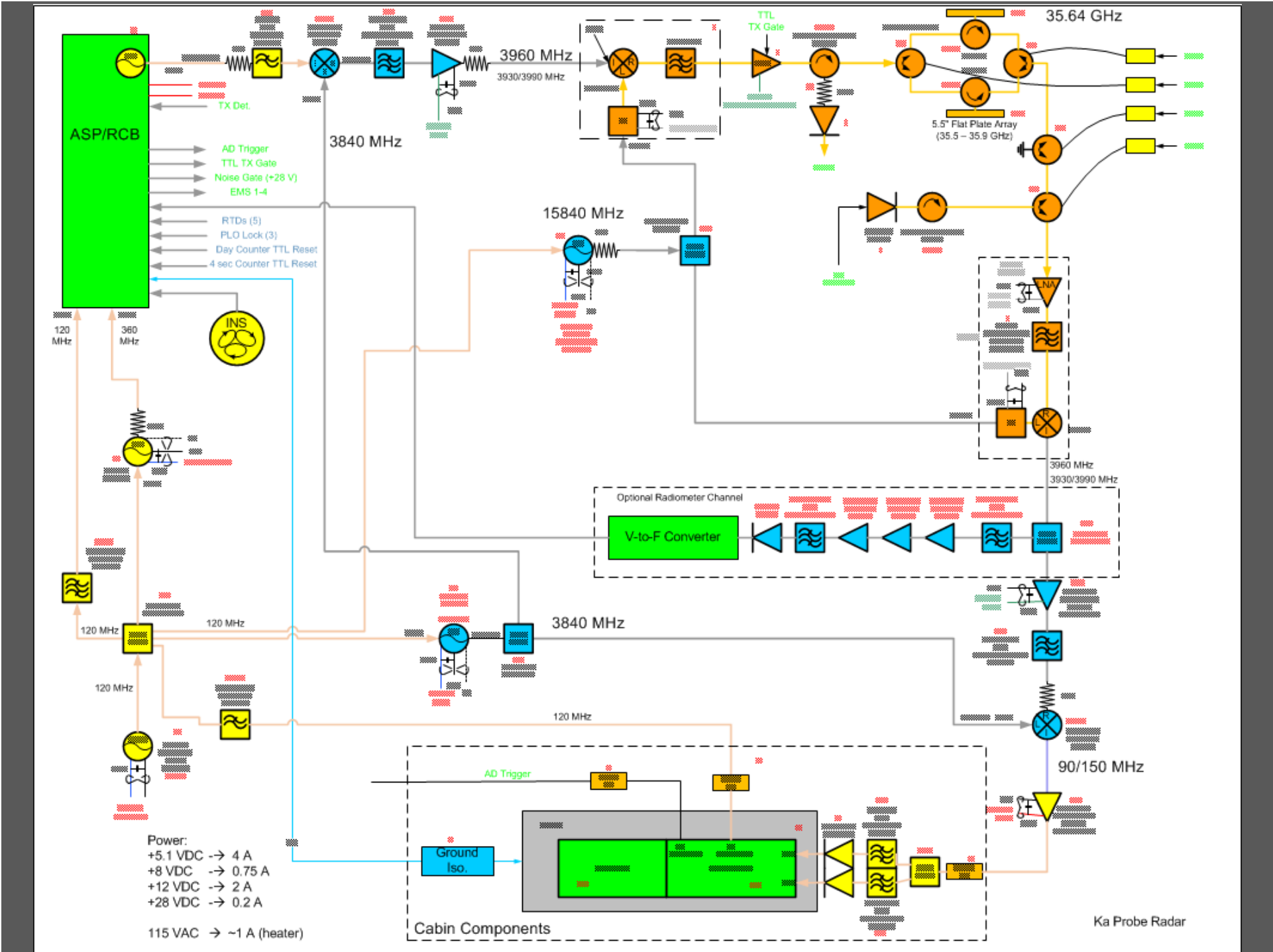
Design Features

- Interleaved profiling capability above and below the aircraft using two antennas -> T/R switch network and dual-antennas.
- Reflectivity and Doppler measurements -> Integrated Analog Devices ADIS16375 IMU
- Maximize sensitivity with a 10 W transmitter -> Pulse compression.
- Measure close to the aircraft (~100 m) -> Combined offset frequency short/chirped TX pulse.
- Radiometric measurement capability (in Zenith beam) -> Integrated noise source and wide band radiometer receiver

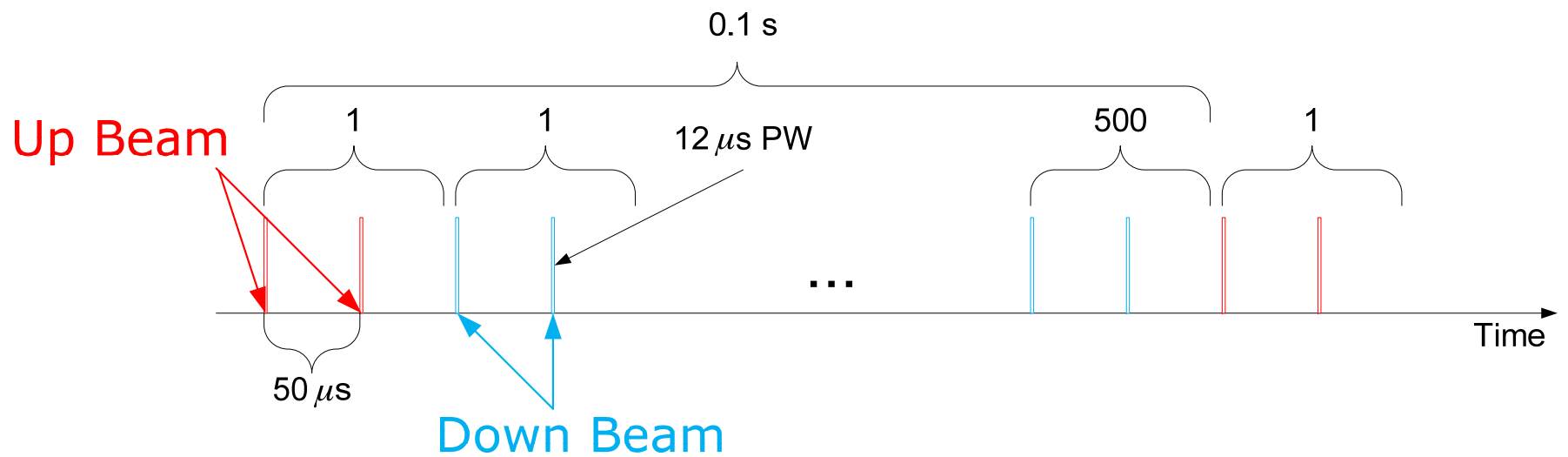
Simplified Component Level Diagram

Pod Mounted Components





Radar Pulsing



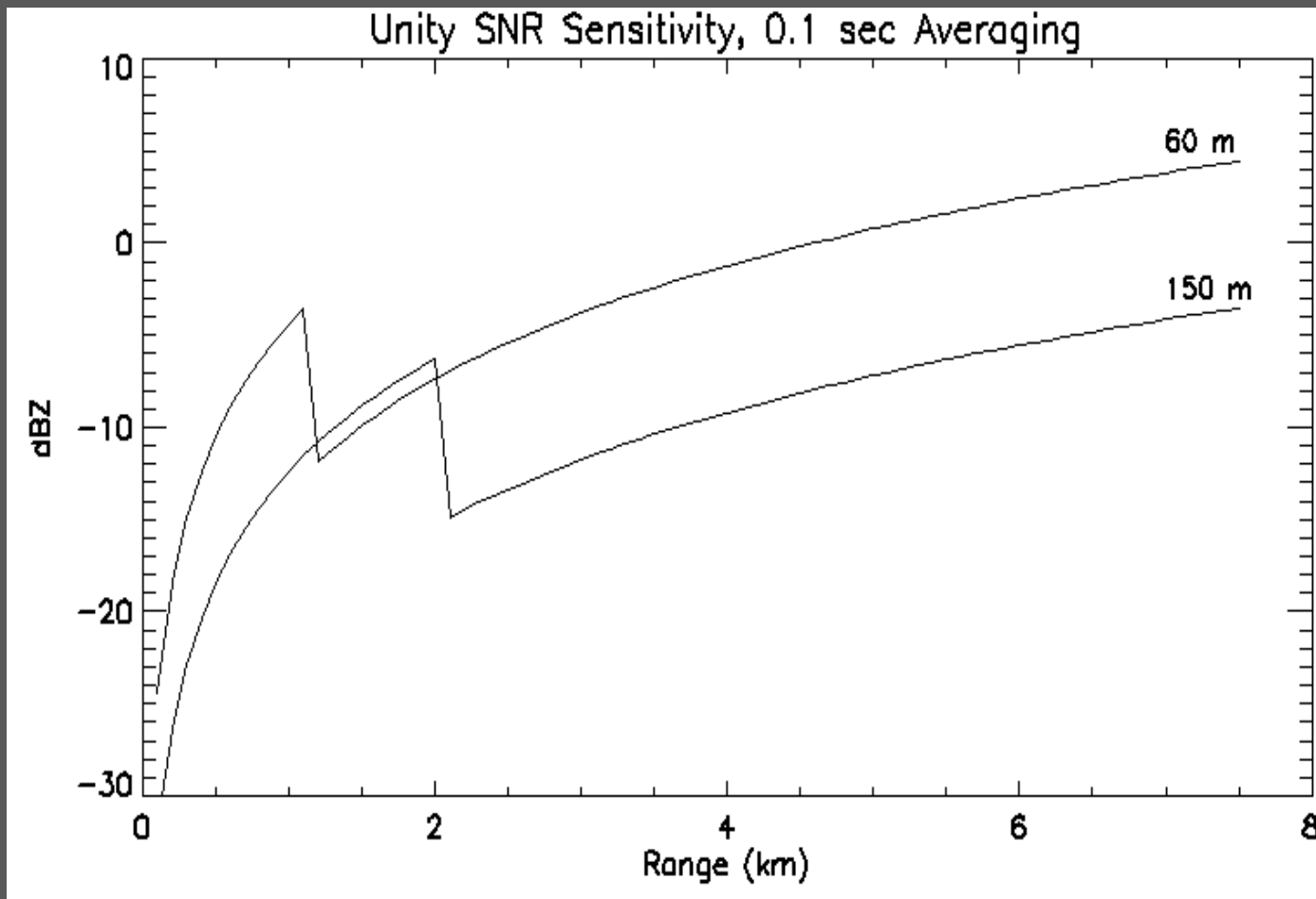
$PRI = 50 \mu\text{s} \leftrightarrow PRF = 20 \text{ kHz}$

Pulse Pair Group Frequency = 5 kHz

$T_{INT} = 0.1 \text{ sec}$

$N = 5000 * 0.1 = 500$

Sensitivity



$$P_t = 40 \text{ dBm}$$

$$F_s = 5 \text{ kHz}$$

$$T_{INT} = 0.1 \text{ sec}$$

$$N = 500$$

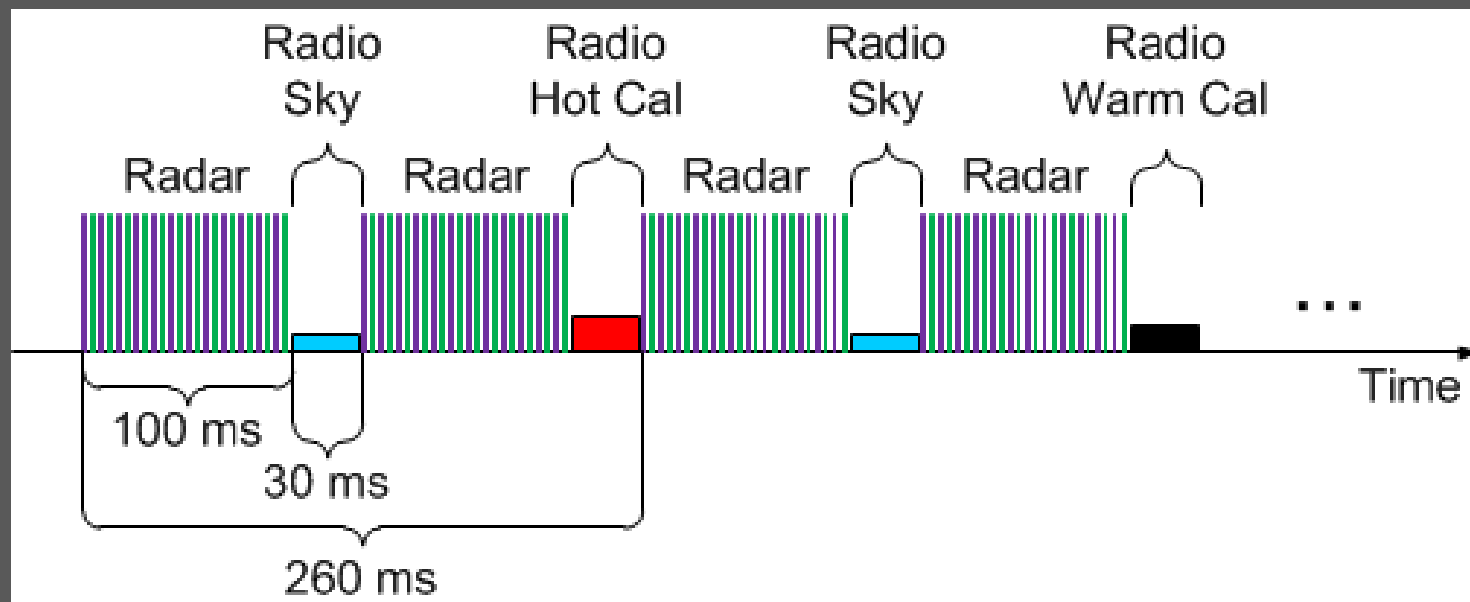
$$\text{Comp.} = 10x$$

Interleaved Radiometer Measurements

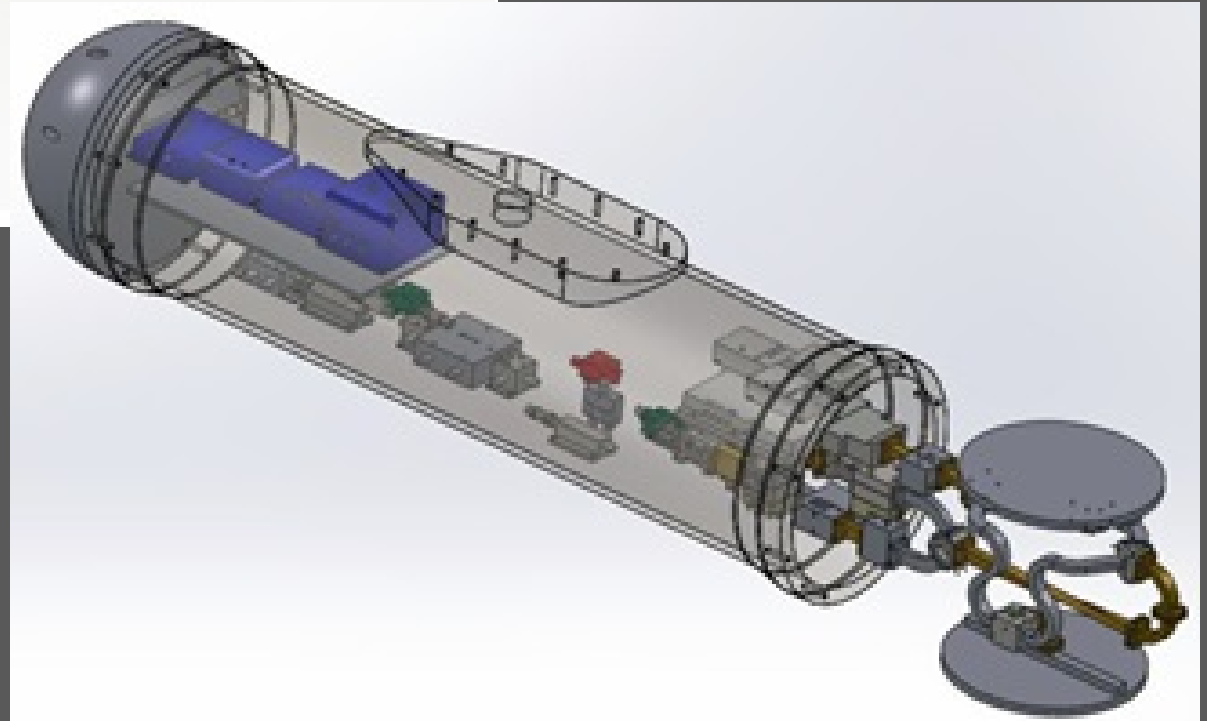
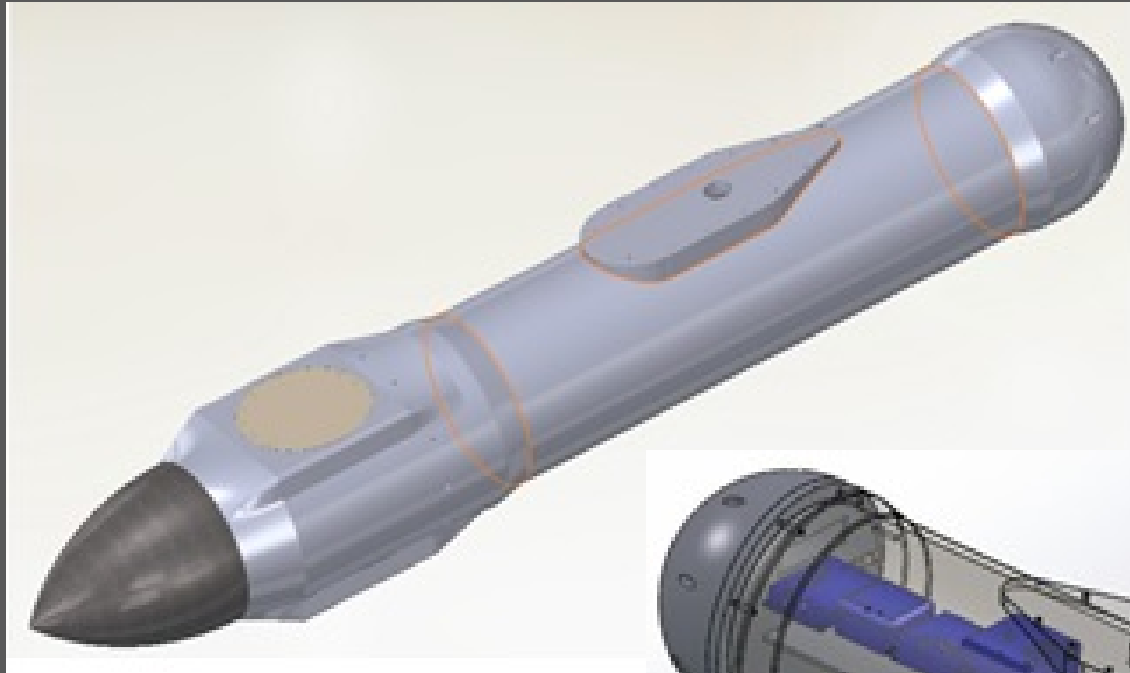
- LWP precision $< \sim 0.02$ mm ($< \sim 20$ g/m²)
- Requires a $\Delta T_B < 0.5$ K
- $$\Delta T_B = \frac{T_{ANT} + T_{SYS}}{\sqrt{B\tau}} \approx \frac{1000}{\sqrt{B\tau}}$$
- $B\tau > 4e6$
- with Radar Data System:
 - $B = 40$ MHz, then $\tau > 100$ ms
- with dedicated Radiometer Receiver:
 - $B = 200$ MHz, then $\tau > 20$ ms

Interleaved Radiometer Measurements

- 100 ms Integration -> 10-15 m Flight Distance
- 4.2° BW Antenna -> ~75 m footprint @ 1 km
- 150 ms radar period: 15-20 m flight distance
- 300 ms radiometer period: 30-45 m distance

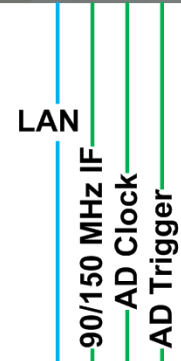
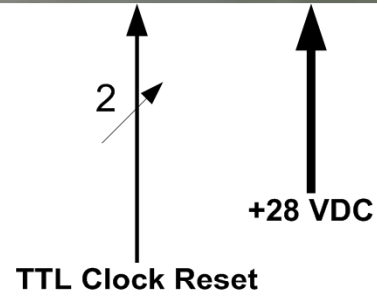


CAD Design



System Diagram

Transceiver



Data Acquisition Server



Client Display



The development of the first unit is being funded by NASA EPSCoR grant NNX13AN09A to the University of Wyoming.



Interleaved Radiometer Measurements

- The observed brightness temperature can be estimated as

$$T_B = T_{BG} + (1 - L)T_{AT}$$

where

$$T_{BG} = \sim 2.7 \text{ K}; T_{AT} = \sim 280 \text{ K}$$

$$L = \exp(-0.23\alpha\Delta x) = \exp(-0.23\kappa LWP)$$

Δx = attenuating distance in km

α = attenuation rate in dB/km

κ = attenuation coefficient; $\sim 0.6 \text{ dB km}^{-1} \text{ g}^{-1} \text{ m}^3$ liquid cloud at Ka-band

m_V = liquid water content (g m^{-3})

LWP (Liquid Water Path in units of g m^{-2}) = $1000 m_V (\text{g m}^{-3}) * \Delta x (\text{km})$

$LWP (\text{mm}) = m_V (\text{g m}^{-3}) * \Delta x (\text{km})$

- $\Delta T_B \cong 0.13\Delta LWP \times T_{AT} \exp(-0.13 \times LWP)$
- $\Delta T_B \cong 0.3 \text{ K}$, if $\Delta LWP = 0.01 \text{ mm}$ or 10 g/m^2