Determining Geometry for Common Comparison Radar Space

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Background:

A condition for the successful inter-radar comparison between two radars is the time-space synchronization in the middle region where the comparison is most effective. In first approximation, a collection of radar beams that overlap in the middle of two radars is represented as a vertical 'wall' with fixed size. How accurate is this analogy?

Objective:

To establish the theoretical basis for the geometrical evaluation of a set of target points at equal distance from two neighbouring radars.



1. Reference systems:



The radars locate the target volume in reference

3. Vectorial equations:



4. CIS solution:

Since the two sets of three vectors describe the position of same target with respect to the Earth centre, equating them results in three scalar equations:

2. Common inter-radar space (CIS):



 α – azimuth

 β – elevation

 λ – longitude

 ϕ – *latitude*

h–altitude

H-tower hight

r – radial distance

mean sea level, and at third

of a common target point

measured from the radar.

 $f(\alpha_{B},\beta_{B},r_{B})$

vector is a local position vector

 $f_x(\alpha_B,\beta_B,r_B) = F_x(\alpha_A,\beta_A,r_A,\lambda_A,\phi_A,h_A,H_A,\lambda_B,\phi_B,h_B,H_B)$ (1) $f_{y}(\alpha_{B},\beta_{B},r_{B}) = F_{y}(\alpha_{A},\beta_{A},r_{A},\lambda_{A},\phi_{A},h_{A},H_{A},\lambda_{B},\phi_{B},h_{B},H_{B})$ (2) $f_{z}(\alpha_{B},\beta_{B},r_{B}) = F_{z}(\alpha_{A},\beta_{A},r_{A},\lambda_{A},\phi_{A},h_{A},H_{A},\lambda_{B},\phi_{B},h_{B},H_{B})$ (3)

For a target point at equal distance from both radars: $r_A = r_B$

(4)

Using the four scalar equations it is possible to obtain the local azimuth and elevation from the second radar, as well as the equal distance, assuming the geographical coordinates and antenna heights are known:



Parameters and constants:



For independent angles (α_A, β_A) we need to obtain theoretical values of dependant variables (r, α_R, β_R) that determine coordinates of CIS.

5. Graphical CIS presentation:



CIS from WKR and WSO radars in the local WKR reference system

 $f(\alpha_A, \beta_A, r_A)$

 $\overrightarrow{OC} = \overrightarrow{OA} + \overrightarrow{AA_h} + \overrightarrow{A_hC} = \overrightarrow{OB} + \overrightarrow{BB_h} + \overrightarrow{B_hC}$ $f(\lambda_A, \phi_A, h_A, H_A) \qquad f(\lambda_B, \phi_B, h_B, H_B)$



$a = (L1^2 - I2^2)(L3M2 - I)$	(L2M3) + 2L1L2(L1M3 -	$-L3M1)-(L3^2-L2^2)$	L1M3 - L3	$(M1)^2$	$L1 = I1 + \frac{1}{2}$	$\frac{OA_{hx} - OB_{hx}}{OA} K2$
$b = 2 \begin{cases} -I2L1(L3M2 - L2M3) - L2[L1(J2L3 + I2M3) + I2(L1M3 - L3M1)] \\ + (L3^2 - L2^2)(L1M3 - L3M1)(J2L3 + I2M3) \end{cases}$					L2 = I3 -	$\frac{OA_{hz} - OB_{hz}}{OA_{hx} - OB_{hx}} K1$
c = 2I2L2(J2L3 + I)	$2M3) - (L3^2 - L2^2)$	$(J2L3+I2M3)^2$		J		$OA_{hz} - OB_{hz}$
$d = (L3^2 - I2^2)(L3M2 - L2M3)$					$L3 = I4 - \frac{hx}{OA_{hz} - OB_{hz}} K3$	
$I1 = \sin \phi_B \cos \lambda_B$ $I2 = \sin \lambda$	$J1 = \sin \phi_B \sin \lambda_B$	$K1 = \sin \phi_B$			M1 = J1 +	$\frac{OA_{hy} - OB_{hy}}{OA_{hz} - OB_{hz}} K2$
$I2 = \sin \lambda_B$ $I3 = \cos \phi_B \cos \lambda_B$	$J 2 = \cos \lambda_B$ $J 3 = \cos \phi_B \sin \lambda_B$	$K 2 = \cos \phi_B$ $K 3 = \sin \beta_A \sin \phi_A - \frac{1}{2} \sin \phi$	$-\cos \alpha_A \cos \alpha_A$	$s\beta_A\cos\phi_A$	M2 = J3 -	$-\frac{OA_{hy}-OB_{hy}}{OA_{hy}-OB_{hy}}K1$
$I4 = \cos \alpha_A \cos \beta_A \sin \beta_A$	$\phi_A \cos \lambda_A - \sin \alpha_A \cos \alpha_A \cos \alpha_A \sin \alpha_$	$\cos \beta_A \sin \lambda_A + \sin \beta_A$ $\cos \beta_A \cos \lambda_A + \sin \beta_A$	$A_A \cos \phi_A \cos \phi_A \cos \phi_A$	$s \lambda_A$ $sin \lambda_A$	M3 = J4 -	$-\frac{OA_{hy} - OB_{hy}}{OA_{hz} - OB_{hz}}K3$
$\overrightarrow{OA} = \frac{a}{\sqrt{1 - e^2 \sin^2 \phi}}$	$= \left[\cos\phi_A\cos\lambda_A\hat{e}_x\right]_A$	$\lambda_A + \cos \phi_A \sin \lambda_A \hat{e}$	$y_y + (1 - e)$	$\left \sin\phi_{A}\hat{e}_{z}\right $	$e^2 = 0.00$	6 694 379 990 14
$\overrightarrow{OB} = \frac{a}{\sqrt{1 - e^2 \sin^2 \phi}}$	$= \left[\cos\phi_B \cos\lambda_B \hat{e}_B\right]$	$\lambda_{x} + \cos \phi_{B} \sin \lambda_{B} \delta$	$\hat{e}_{y} + (1 - \epsilon)$	e^2)sin $\phi_B \hat{e}_z$]	<i>a</i> =	= 6 378 137.0 <i>m</i>
6. Anal 1) The first (<i>L</i> , <i>W</i> , <i>H</i>)	yse: approxim = <i>const</i>	nation:	TI		CIS	
very robus	st and ina	ccurate.	Π	W		L
			-			

2) The second approximation: $(L,W,H) = f(\lambda_A,\phi_A,h_A,H_A,\lambda_B,\phi_B,h_B,H_B)$ much more accurate but not operationally suitable.



The spatial distribution of CIS points generated width 1 Deg azimuth and elevation resolution presented in local (WKR) radius-azimuth-elevation space (left) and Descartes reference system (right).

Summary:

- Converting coordinates to the geocentric coordinate system is essential for obtaining accurate common inter-radar space (CIS) coordinates
- The CIS coordinates depends on the geographical locations of a radar pair
- The CIS coordinates in the local coordinate system are not necessary in the vertical 'wall' but more often they are in the 'tilted wall'
- Obtained formulas for CIS are very accurate but not operationally suitable since they determine the geometric equidistant points not the common radar pulse volumes; next steps will be the inclusion of the technical characteristics of radars and a conversion of geometric elevation to antenna axis elevation

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36th Conference on Radar in Meteorology, September 16-20 2013, Breckenridge, CO.

3) The third approximation should include the radar characteristics:

 $(L,W,H) = f \begin{pmatrix} \lambda_A, \phi_A, h_A, beamWidth_A, beamPulse_A, \\ \lambda_B, \phi_B, h_B, beamWidth_B, beamPulse_B \end{pmatrix}$ and will be operationally applicable.