



AMERICAN METEOROLOGICAL SOCIETY



*The AFIT of Today is the Air Force of Tomorrow.*

# Using Satellite, NWP, and Atmospheric Refraction Assessments to Enhance Radiative Transfer Characterizations for Remote Sensing and Directed Energy Applications

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19<sup>th</sup> Conference on Integrated Observing and Assimilation Systems for the Atmosphere,  
Oceans, and Land Surface*

The views expressed in this document are those of the author(s) and do not reflect the official policy or position of the United States Air Force, the Department of Defense, or the United States government.

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# Overview



*The AFIT of Today is the Air Force of Tomorrow.*

- Introduction/Goal of Research
- Simulation Tool
- Methodology
- Results
- Conclusion/Future Work



# Introduction



*The AFIT of Today is the Air Force of Tomorrow.*

- Goal: couple numerical weather forecast, now-cast and satellite weather data with traditional climatologies for improved radiative transfer simulation
  - Higher fidelity path radiance for remote sensor applications
  - Higher resolution path refraction and optical turbulence effects for DE propagation
- Core Analytical / Synoptic Observation Tools:
  - Laser Environmental Effects Definition and Reference (LEEDR)
  - NOAA's numerical weather prediction tools (i.e. Global Forecast System)
  - NASA Aqua mission: AIRS and AMSU sensor suite



# Simulation Tool LEEDR

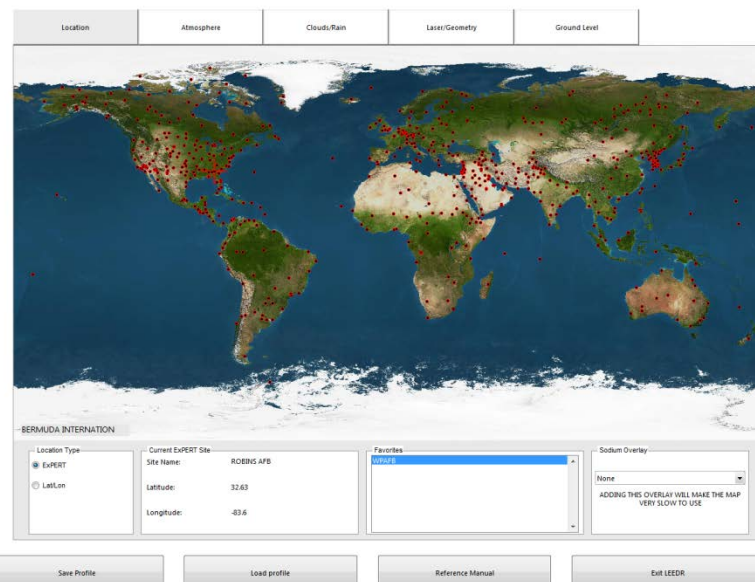
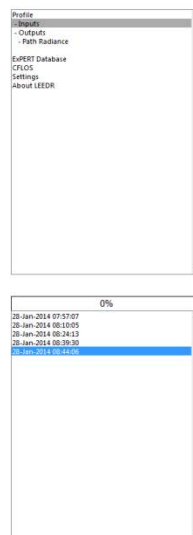


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- Calculates line-by-line and spectral band radiative transfer solutions by creating correlated, physically realizable vertical profiles of meteorological data and environmental effects (e.g. gaseous and particle extinction, optical turbulence, and cloud free line of sight)
- Accesses terrestrial and marine atmospheric and particulate climatologies
  - Allows graphical access to and export of probabilistic data from the Extreme and Percentile Environmental Reference Tables (ExPERT)



LEEDR  
Laser Environmental Effects Definition And Reference





# LEEDR

## Worldwide Climatology

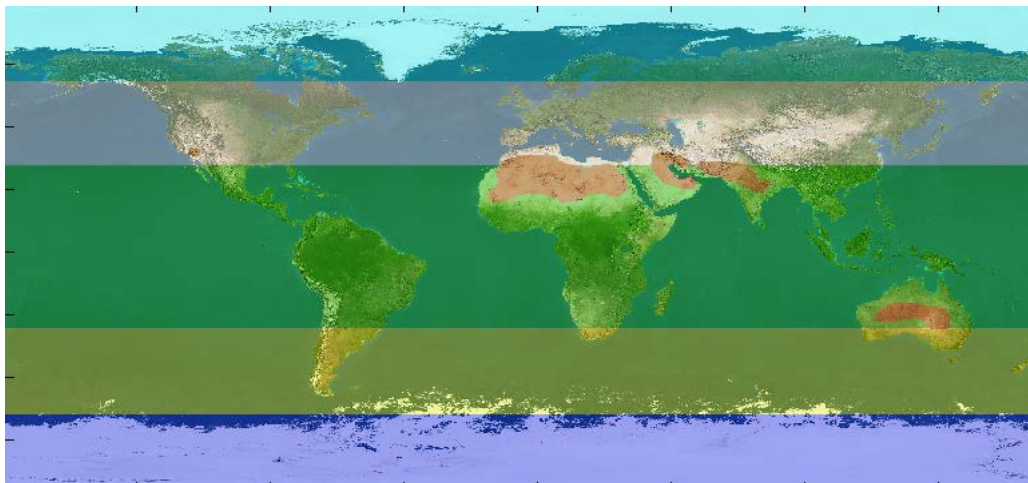
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Polar-North

Tropical

Polar-South

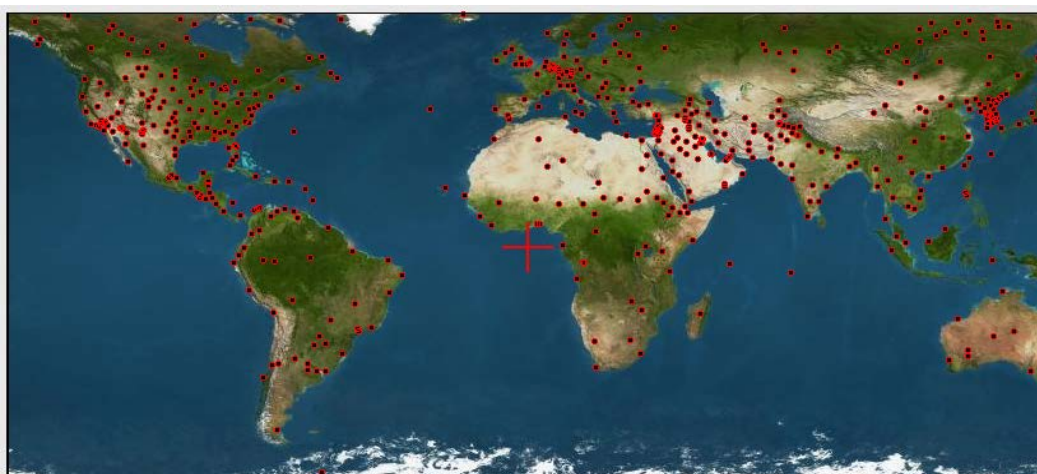


Midlat-North

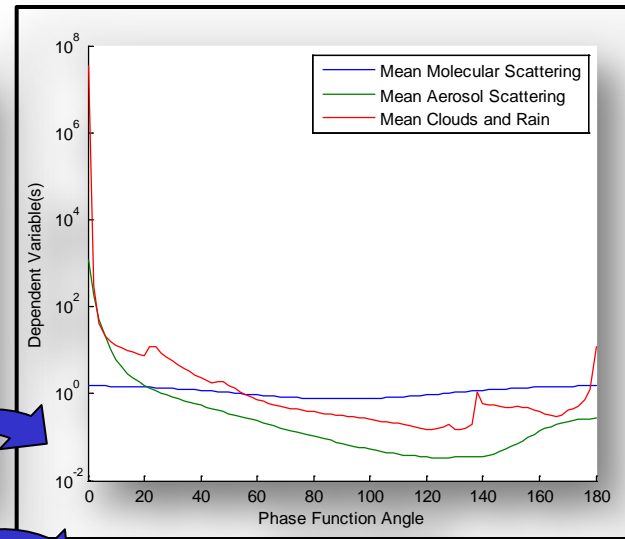
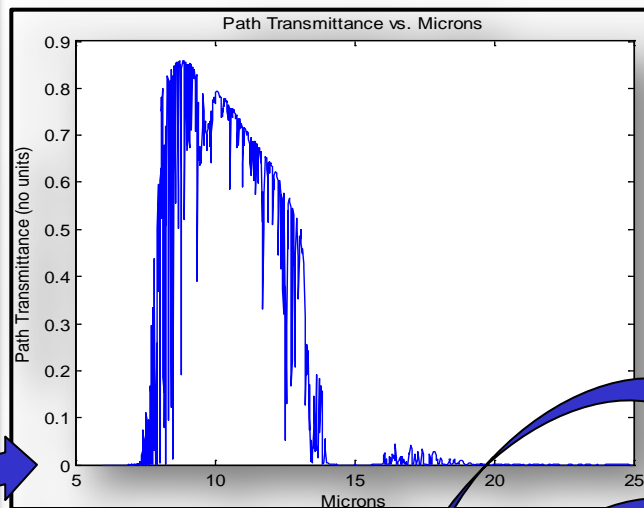
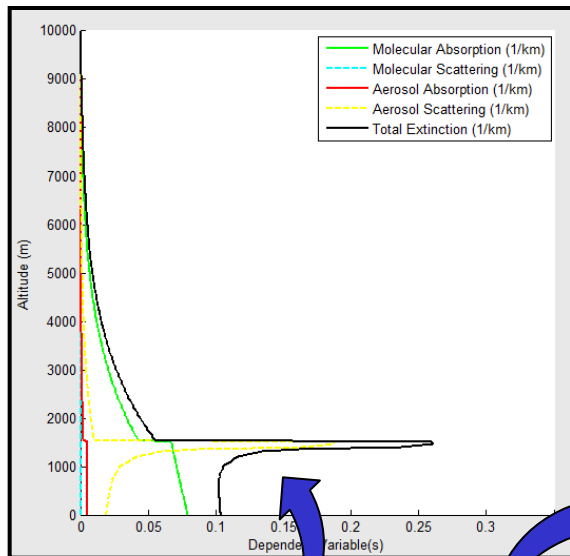
Desert (Red Shaded)

Midlat-South

**LEEDR ocean site selection map and upper air regions**

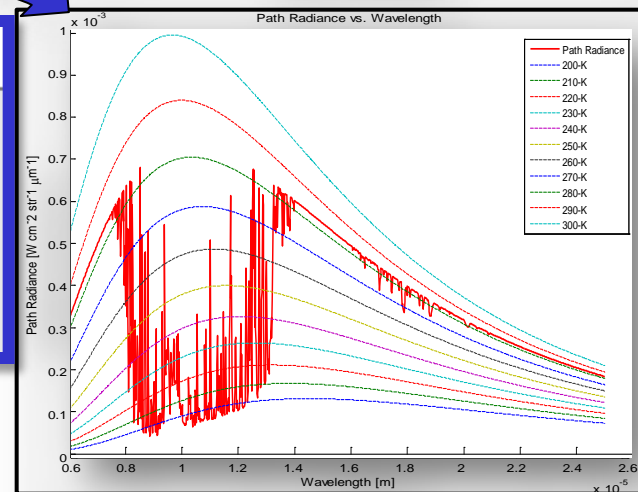


**573 ExPERT (land) locations represented in LEEDR**



Values	2D Outputs	Comparisons	Export	Backscatter	Phase Functions	Path Radiance
Path Results						
Path Transmittance:	0.758151					
Path Extinction (1/km):	0.00276872					
Path Specific Attenuation (dB/km):	0.0120244					
Surface Visibility (km):	28.0687					
Slant Path Visibility (km):	483.369					

- LEEDR provides user multiple interactive views of atmospheric radiative effects



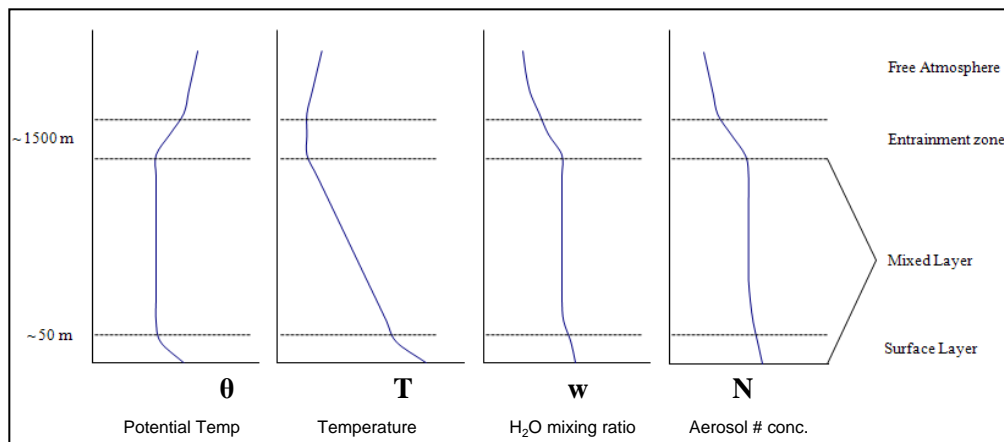




## Atmospheric Boundary Layer: Realistic Lapse Rate

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- Description
  - Well mixed layer up to 1.5-2.0 km thick
  - Capped by temperature inversion
- Effects
  - Trap pollutants & aerosols
  - Location of wind shear
  - Atmospheric turbulence (surface layer)
  - Increasing RH & extinction with height



$$\left(\frac{dT}{dz}\right)_{dry} = -\frac{g}{c_p} = -9.8K \cdot km^{-1}$$

**Dry adiabatic temperature lapse rate**

$$\left(\frac{dT_d}{dz}\right) = -\frac{g}{\epsilon l_v} \frac{T_d^2}{T} \approx -1.8K \cdot km^{-1}$$

**Lapse rate of dewpoint temperature**

$$\left(\frac{dT}{dz}\right)_{moist} = -\frac{g}{c_p} \frac{1 + l_v w_s / RT}{1 + l_v^2 w_s / c_p R_v T^2}$$

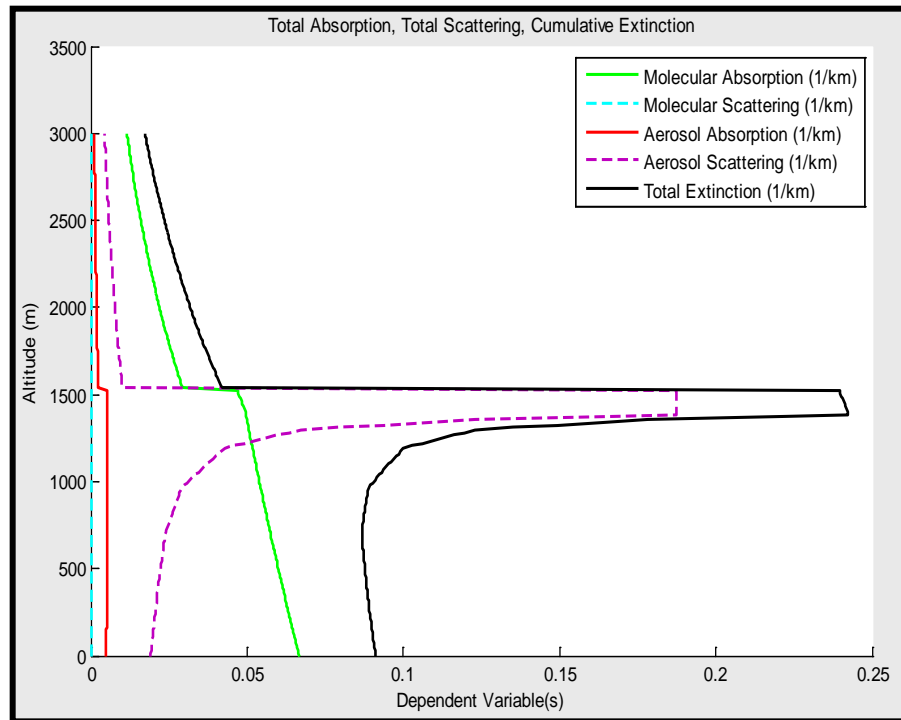
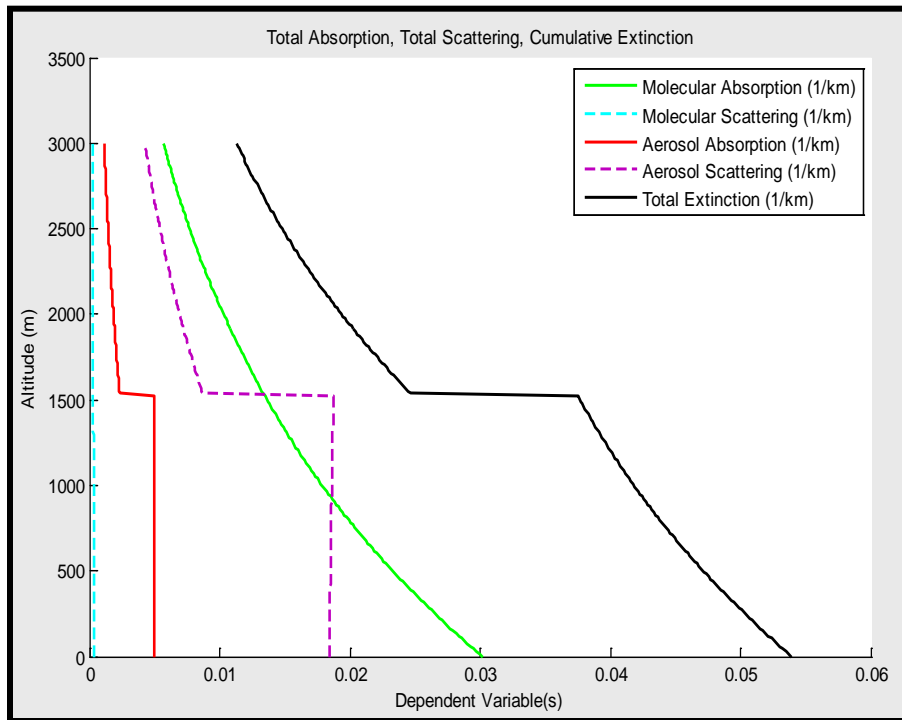
**Moist (saturated) lapse rate**



# LEEDR

## Standard vs Realistic Extinction Profiles

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**Left panel:** Absorption and scattering effects on 1.31525  $\mu\text{m}$  radiation over a 6000 m slant path from 3000 m altitude to the surface in a US Standard Atmosphere where the boundary layer is only defined with a constant aerosol concentration through the lowest 1524 m. **Right Panel:** Same slant range geometry as the left panel, but for a Wright-Patterson AFB summer atmosphere at 1500-1800 local time where the boundary layer is defined by constant aerosol concentrations.

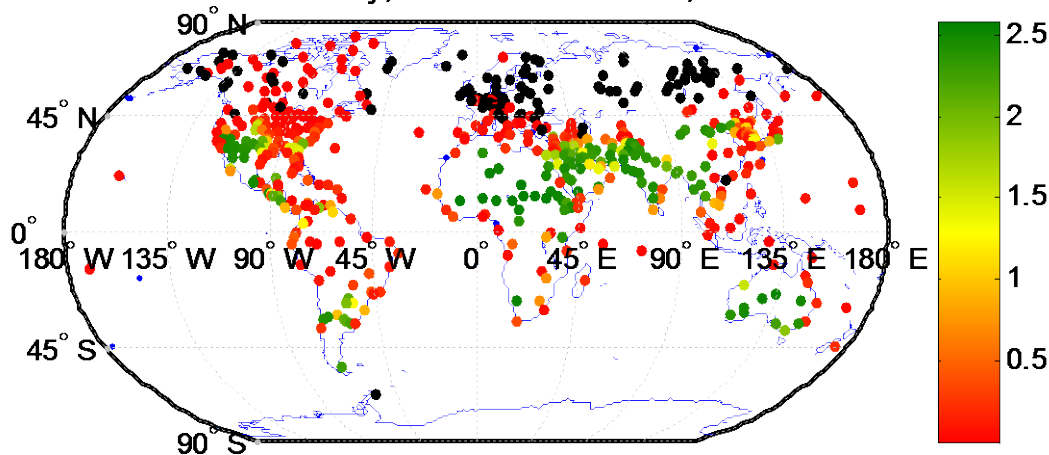


# LEEDR Realistic Atmospheres

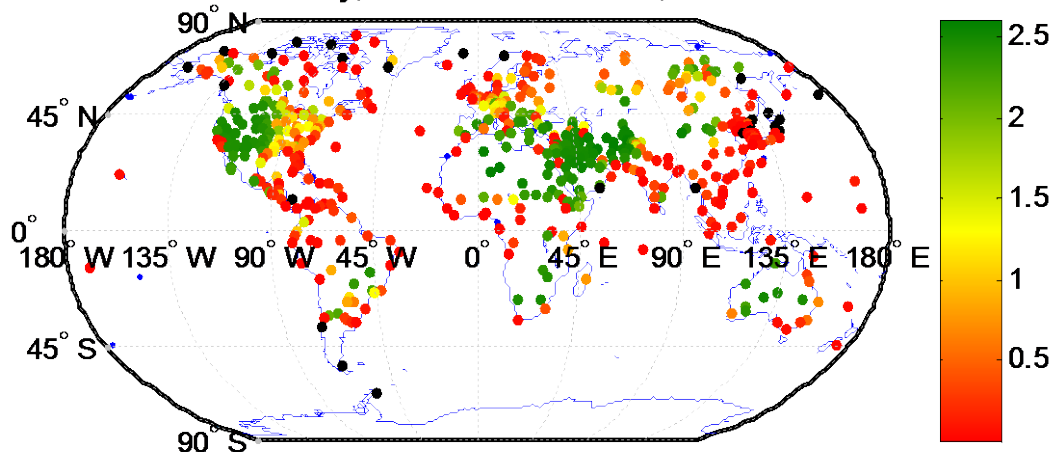
## The Impact: Elevated Aerosol Extinction

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Irradiance Ratio: January, 20-1500m Altitudes, 5km Slant Path



Irradiance Ratio: July, 20-1500m Altitudes, 5km Slant Path



- Ratios of HEL irradiance; realistic aerosol environment over standard environment
  - Std: US Std Atm with 23km Modtran Rural aerosols
- Realistic conditions at land sites are in general worse than standard in terms of DE propagation

Inputs

Wavelength

6e-06

-

2.5e-05

Molecular Points:

10

Aerosol Points:

10

☒ Correlated K

Geometry

Observer at Target

Observer Altitude:

100000

Observer Zenith:

180

Observer Azimuth:

0

Layers:

50

Calculate

Path Radiance

Surface

☒ Surface Type:

Snow\_Cover

Albedo Defined From: 1.4e-06 m to 5e-05 m

User Emissivity:

1

User Albedo:

0.1

Temperature:

296

Date and Time (UTC)

<

August

>

2013

S	M	T	W	R	F	S
				1	2	3
4	5	6	7	8	9	10
11	12	13	14	15	16	17
18	19	20	21	22	23	24
25	26	27	28	29	30	31

Hour

Minute

Seconds

13

5

28.595

Snow\_Cover

Forest

Farm

Desert

Ocean

Cloud\_Deck

Old\_Grass

Dead\_Grass

Maple\_Leaf

Burnt\_Grass

CCM3\_Sea\_Ice

Conifer

Olive\_Gloss\_Paint

Deciduous\_Tree

Sandy\_Loam

Granite

Galvanized\_Steel

Grass

Black\_Plastic

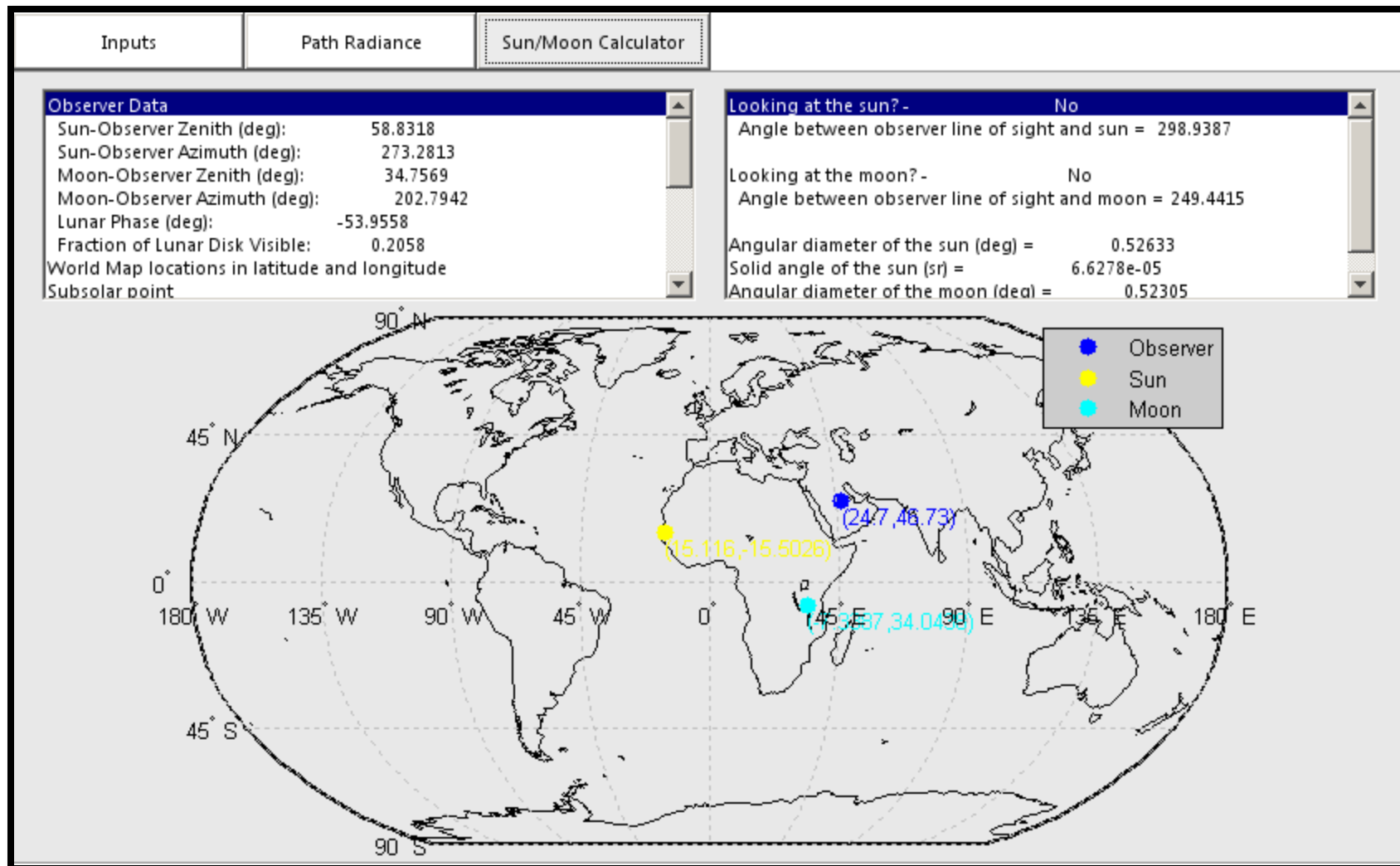
Aluminum

**Important for Solar/Lunar Calculations!**

# LEEDR Path Radiance GUI

## Key Aspect: Earth-Sun-Moon Geometry

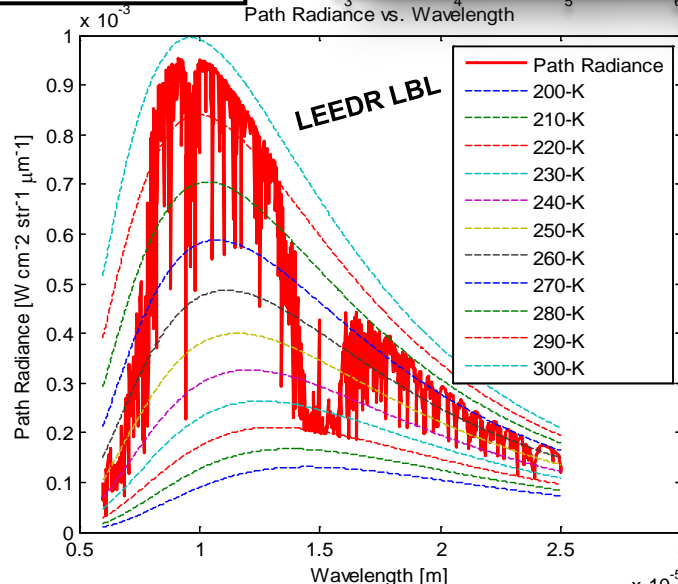
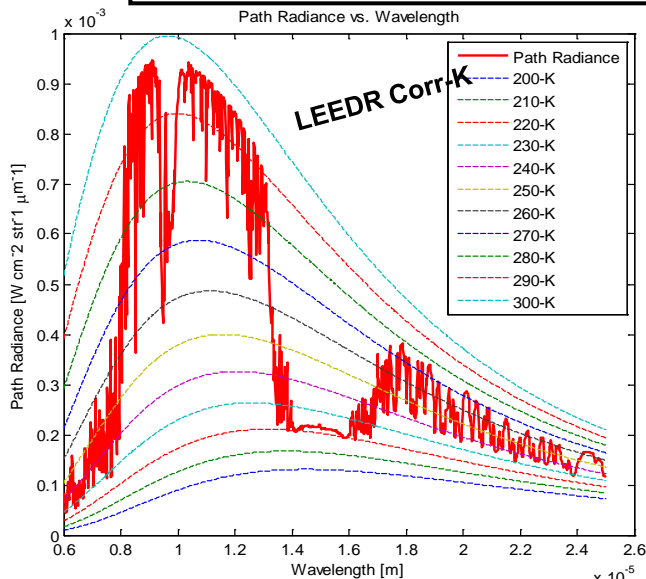
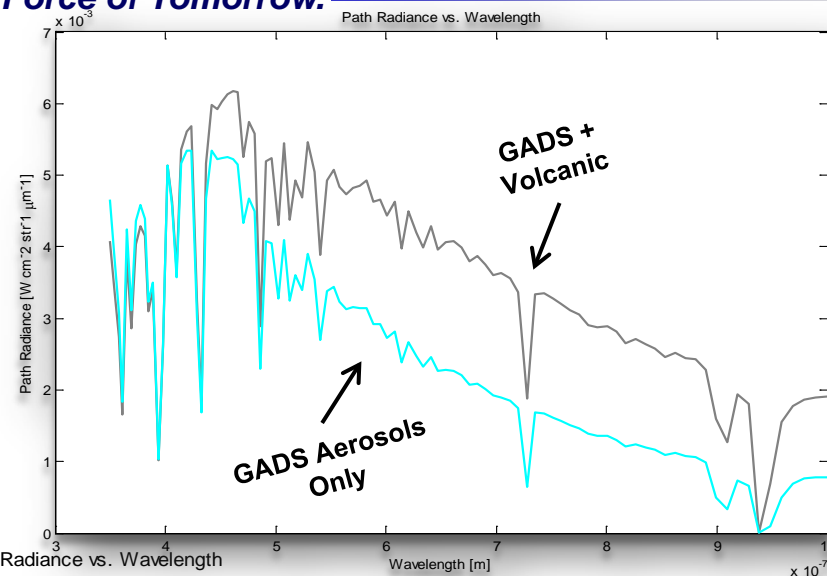
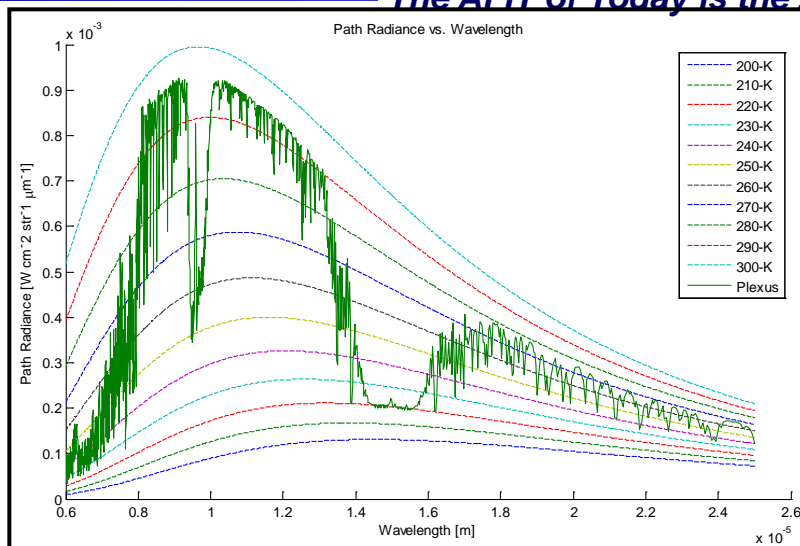
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# LEEDR Path Radiance

## Tailored Derivation / Flexible Solutions

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- Upward or downward looking spectral path radiance calculation fully incorporated into LEEDR
  - Line-by-line
  - Correlated-k
  - Single scattering
  - With / without aerosol effects



# LEEDR Path Bending GUI

## Realistic Atmospheric Refractivity Profiles



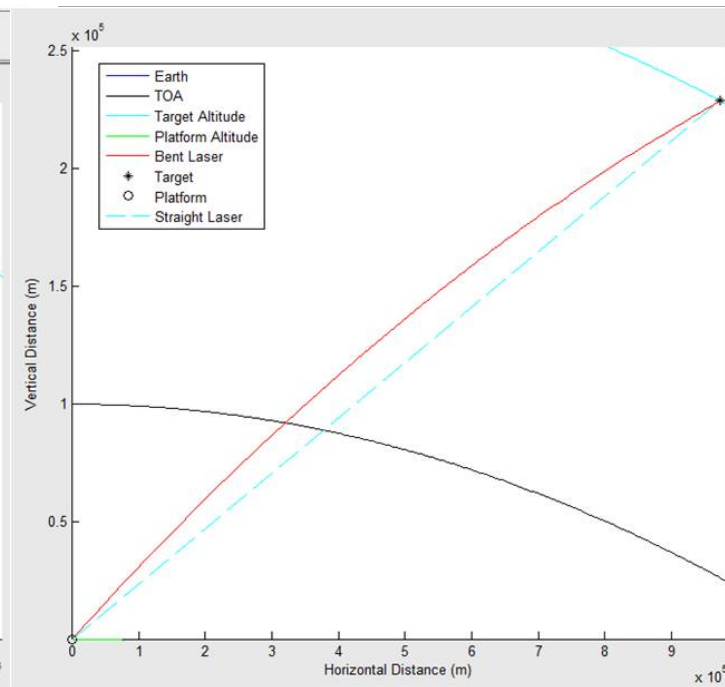
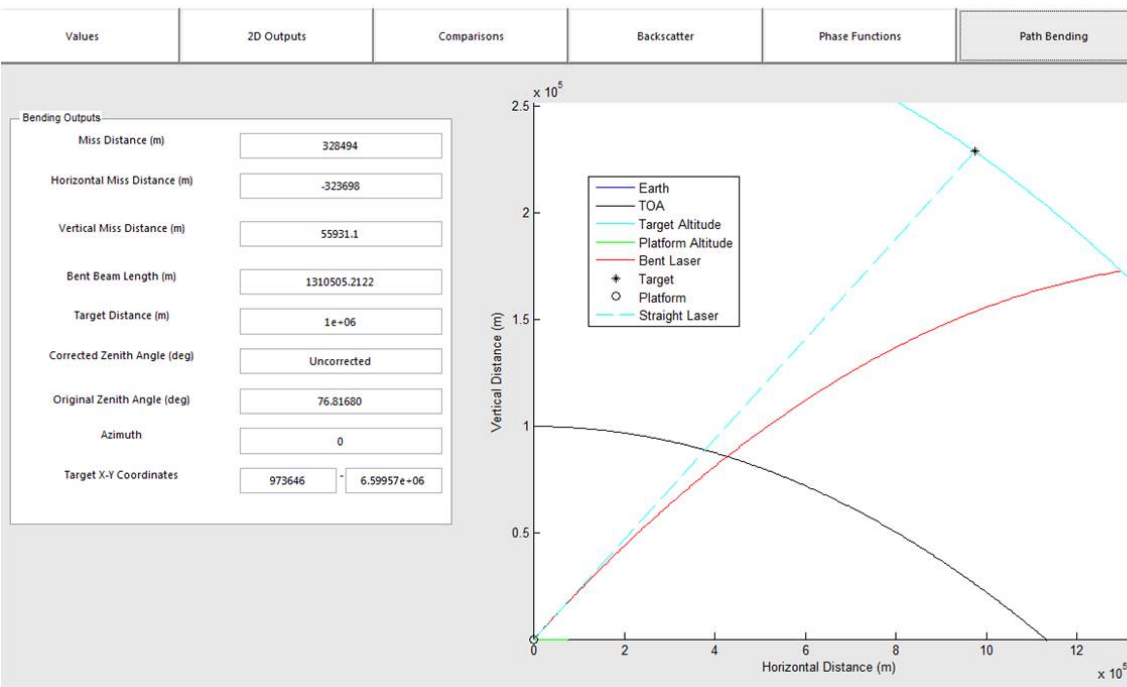
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### Displaced Path

Calculate actual path of laser when aimed at endpoint

### Point to Point

Apply atmospheric compensation correction to improve aim, hit endpoint

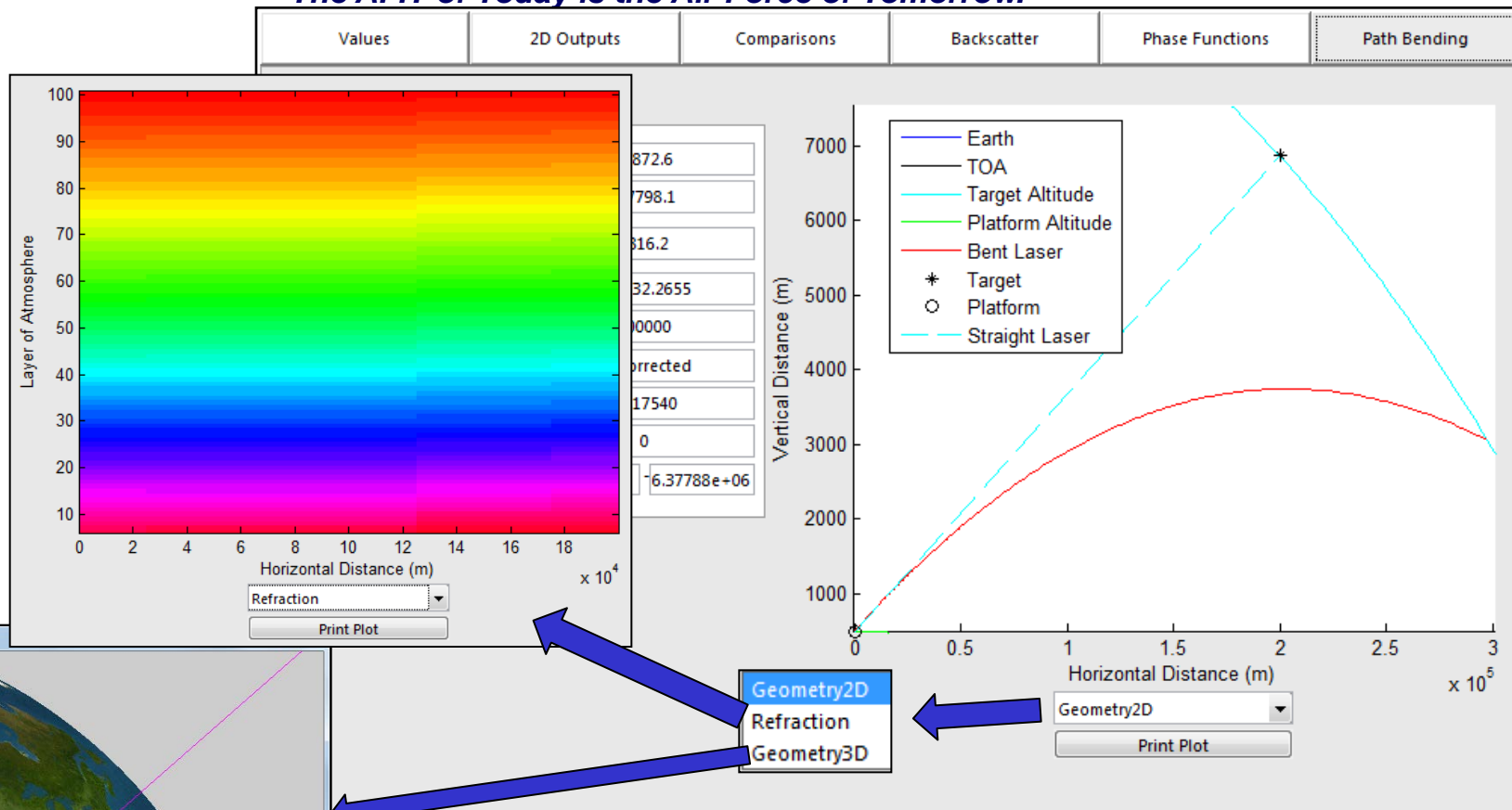




# Atmospheric Profile Production Outputs



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- The Refraction plot is helpful to view horizontal atmospheric variations
  - When used in combination with NOMADS, up to 5 nearest neighboring numerical weather grid points may be considered depending on the path geometry



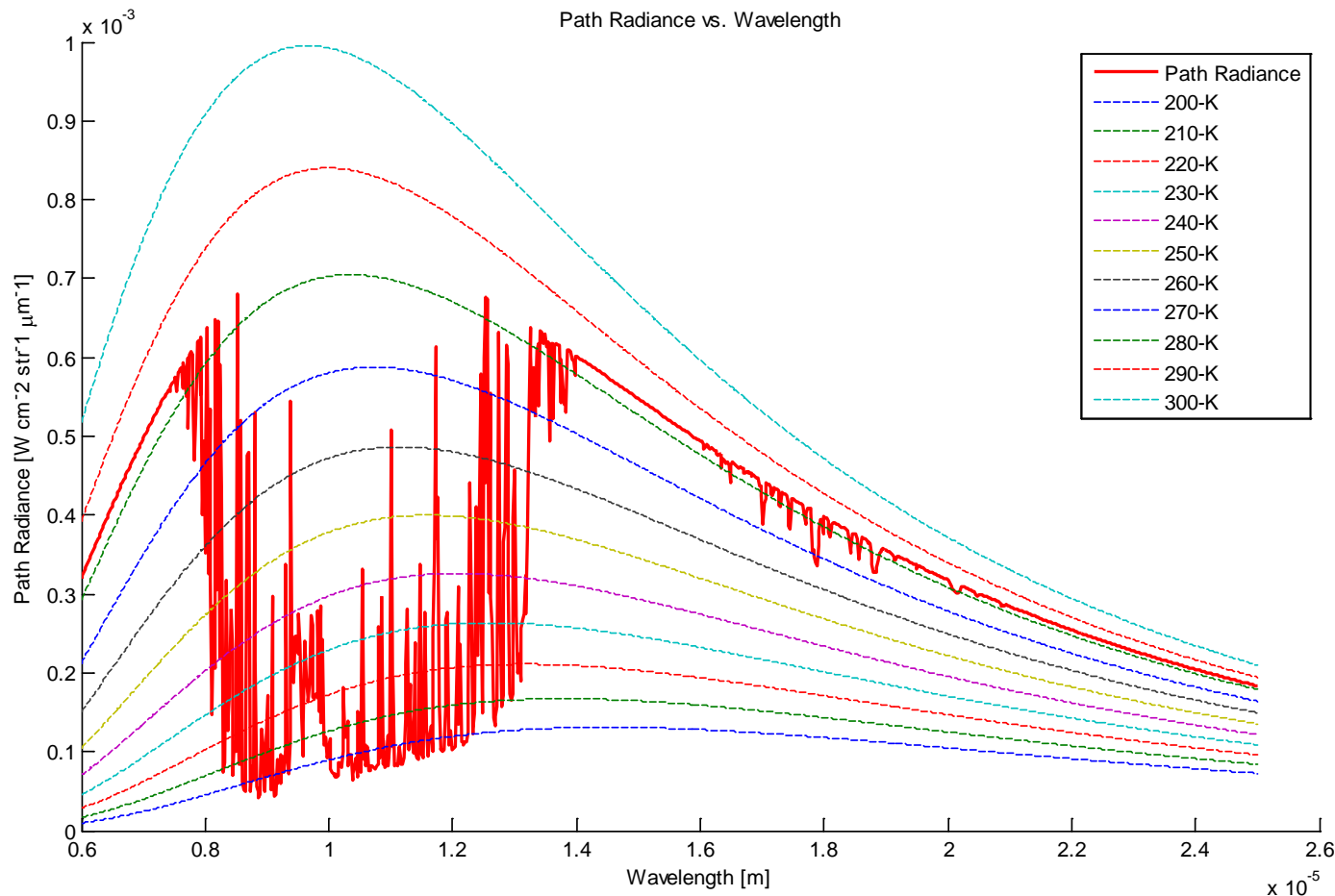


# Path Radiance Tab

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- Printable Plot
  - 1000 molecular points, 10 aerosol points

- Uplooking radiance from sky versus wavelength





## Ingest Numerical Wx Prediction and Remote Sensor Data

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Upgrade radiative transfer code tools  
(e.g. **Path Bending**, **Path Radiance**)

• Initial state: climo-based effects

Integrate gridded numerical **Wx**  
forecast data and remote sensor  
profiles

Evaluate / compare  
atmospheric

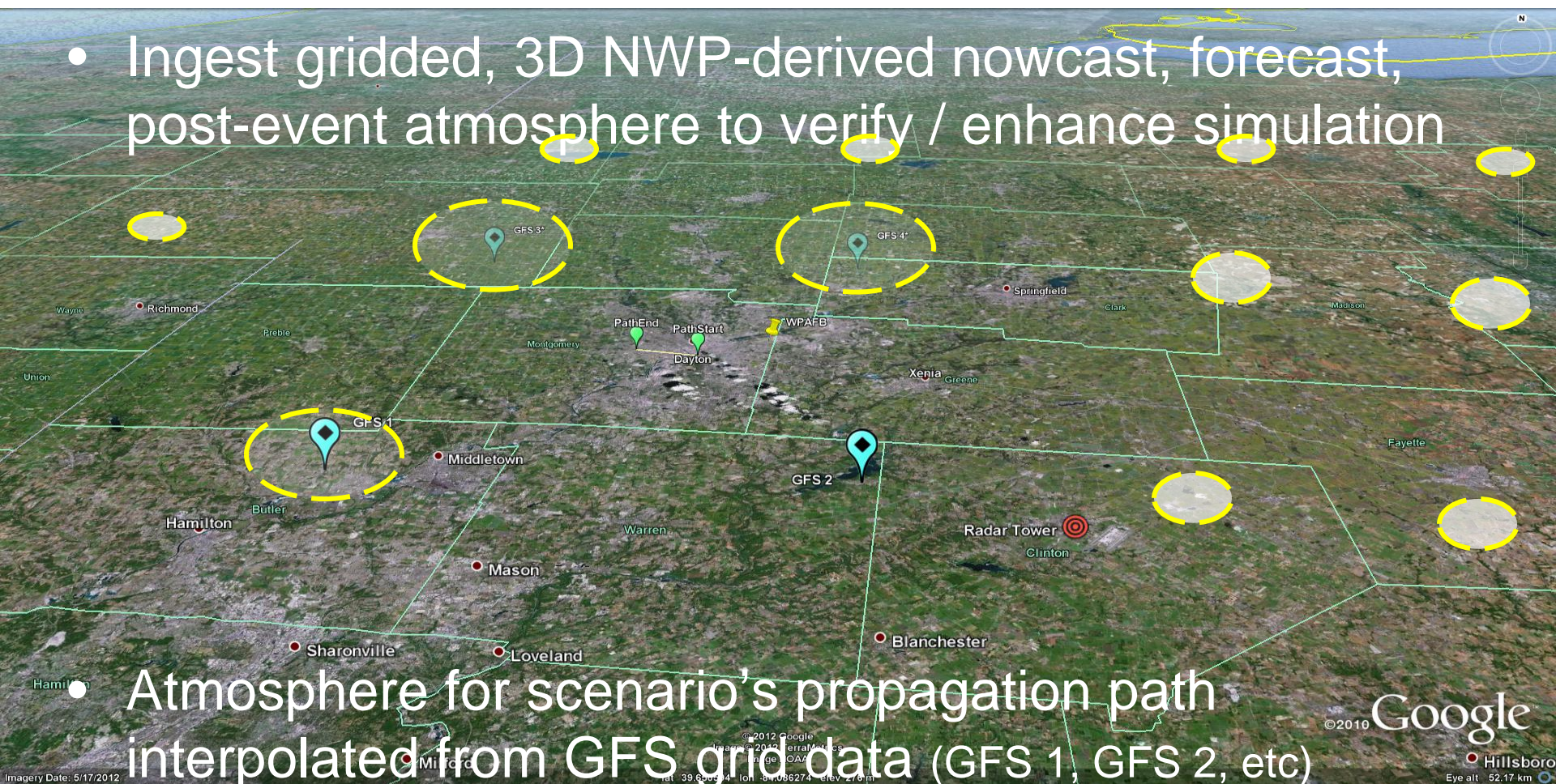
characterization methods

Optimize Path Bending /  
Radiance code

Evaluate impact :  
Remote sensing and  
Directed Energy

Propagation Applications

- Ingest gridded, 3D NWP-derived nowcast, forecast, post-event atmosphere to verify / enhance simulation



- Atmosphere for scenario's propagation path interpolated from GFS grid data (GFS 1, GFS 2, etc)

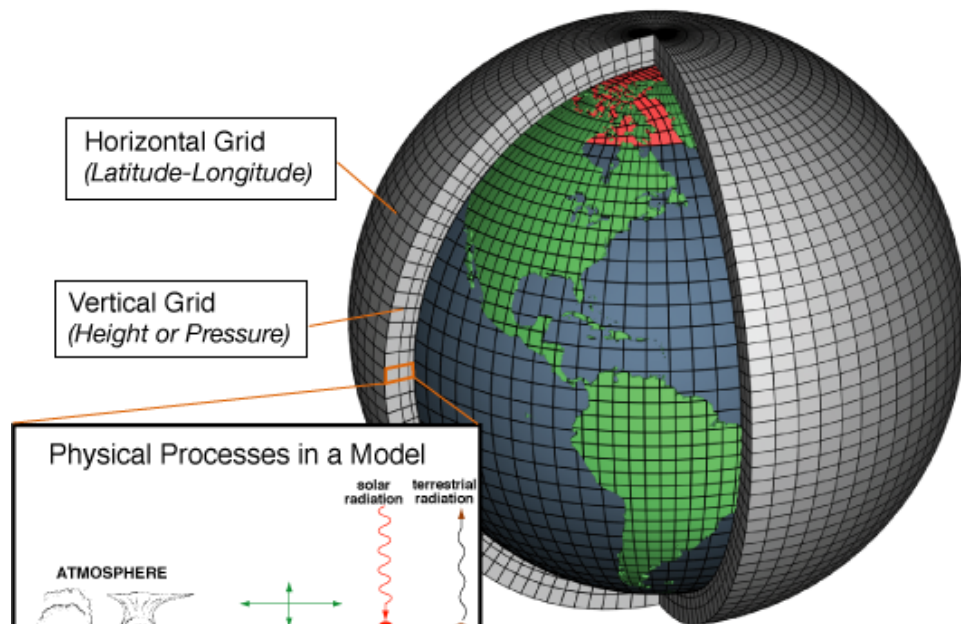


# Numerical Weather Prediction (NWP)

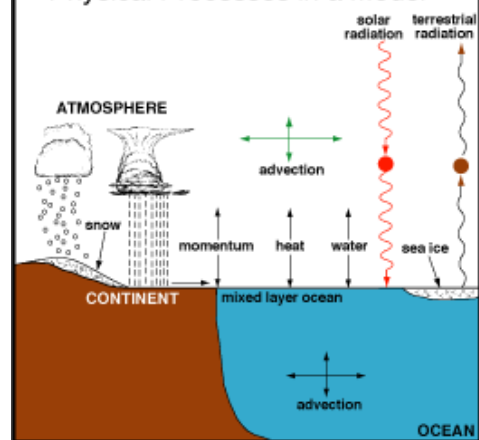
## Models for gap filling

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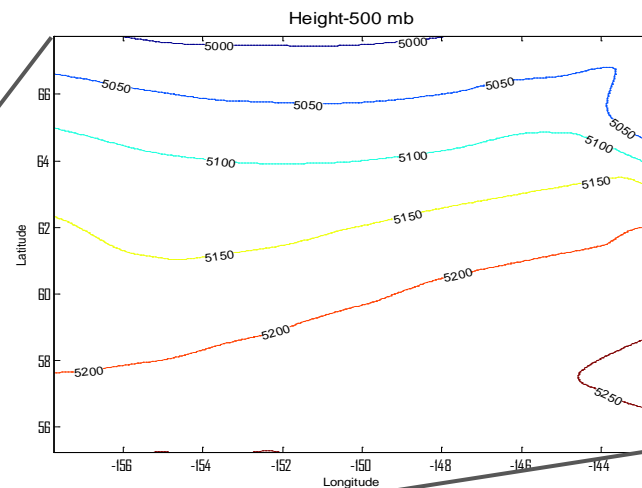
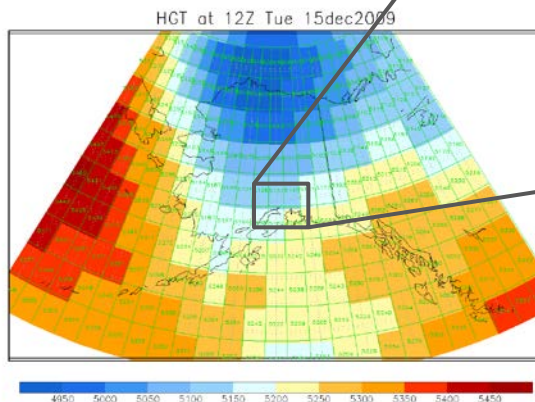
- Global Forecast System (GFS)
- Global 3-D gridded GFS data available with 0.5 deg horizontal resolution, and 3-hour time increments



### Physical Processes in a Model



NOAA Website [Online]  
[http://celebrating200years.noaa.gov/breakthroughs/climate\\_model/](http://celebrating200years.noaa.gov/breakthroughs/climate_model/)

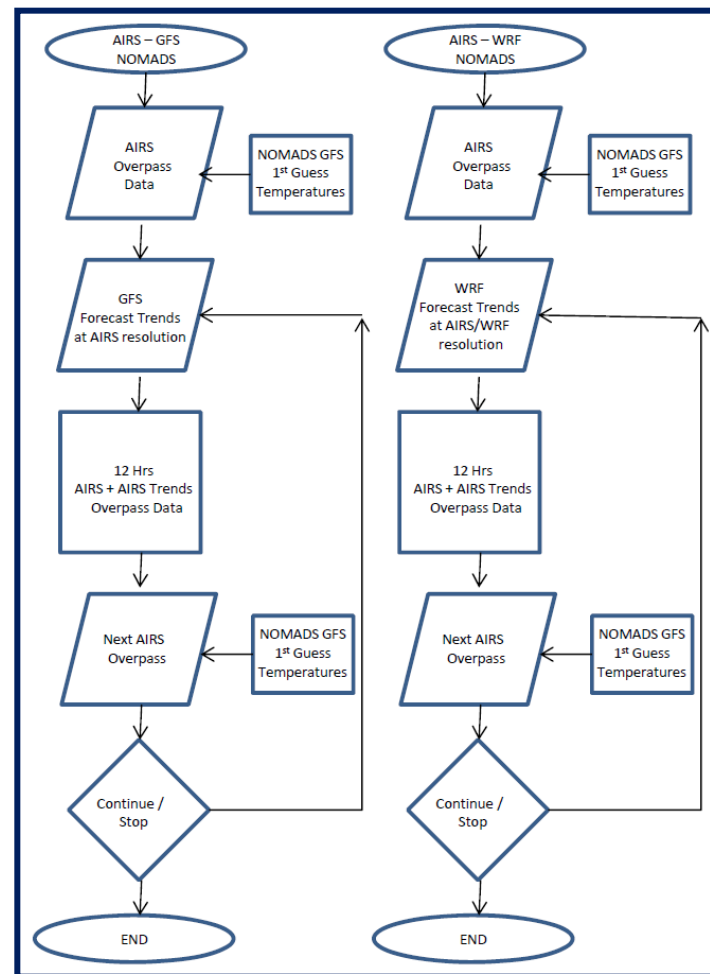
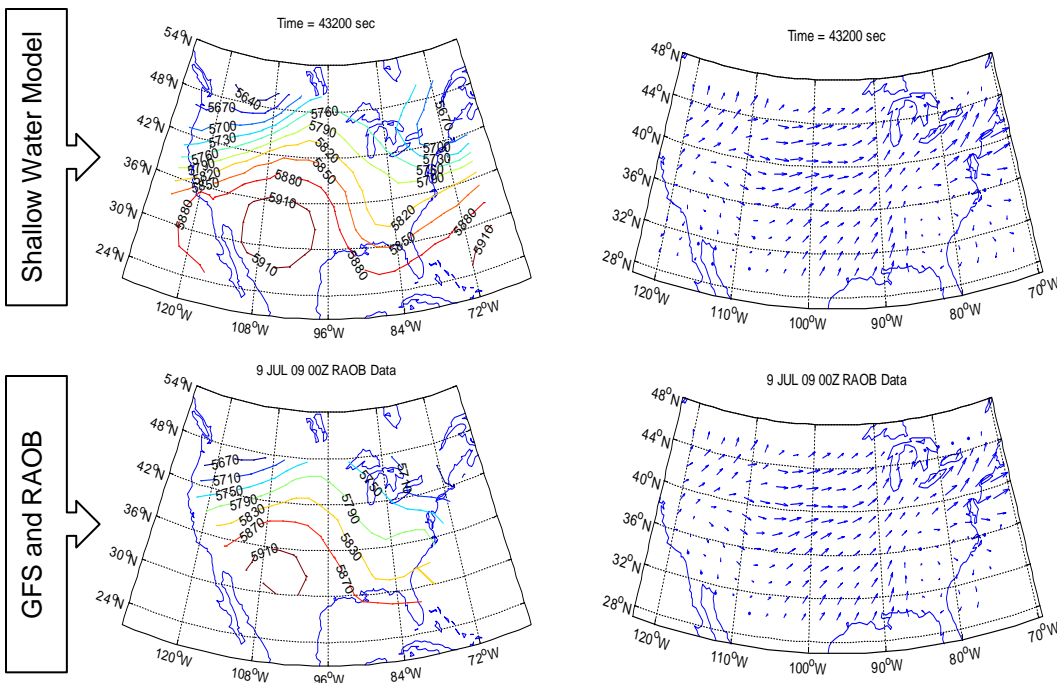


# Gap Filling with NWP

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- Simple weather model initialized with gridded GFS data and rawinsonde observations
- Model runs at 1-min time-step for next 12 hours



# Methodology

## NWP Impact: Extinction / RH Comparisons

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NOMADS - 29 August 2013 - 550nm  
1800 cycle + 27hrs

LEEDR Extinction Profiles  
(using NWP)

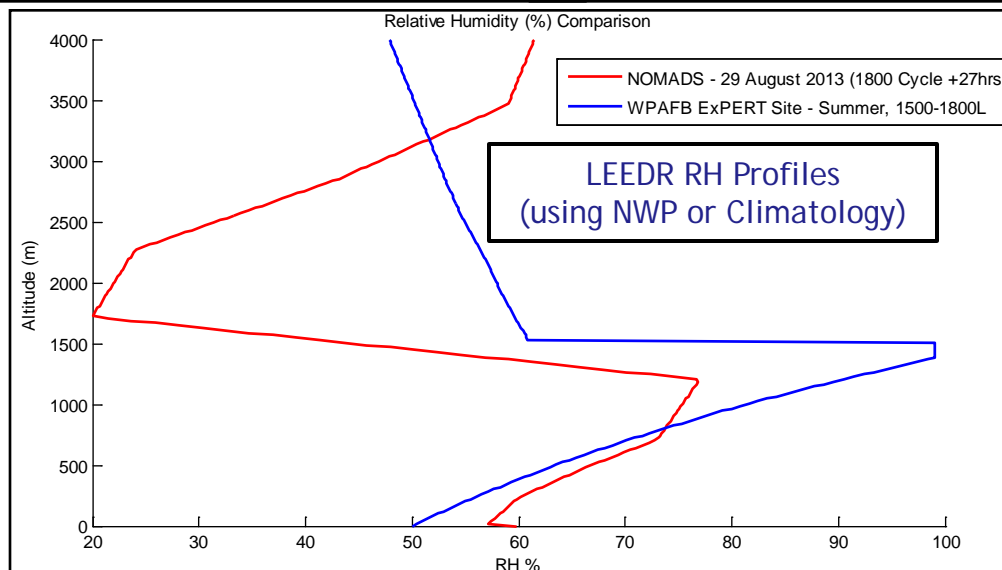
— Molecular Absorption (1/km)  
- - Molecular Scattering (1/km)  
— Aerosol Absorption (1/km)  
- - Aerosol Scattering (1/km)  
— Total Absorption (1/km)  
- - Total Scattering (1/km)  
— Total Extinction (1/km)

WPAFB ExPERT Site - Summer, 550nm  
1500-1800L

LEEDR Extinction Profiles  
(using Climatology)

Dependent Variables

Dependent Variables



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*Aim High...Fly - Fight - Win*

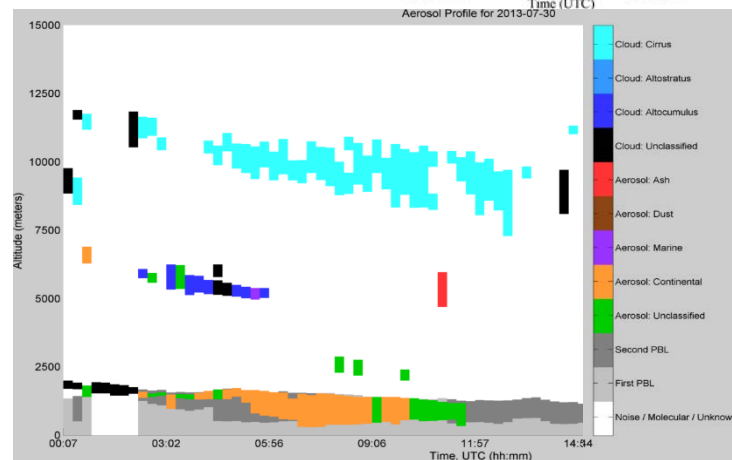
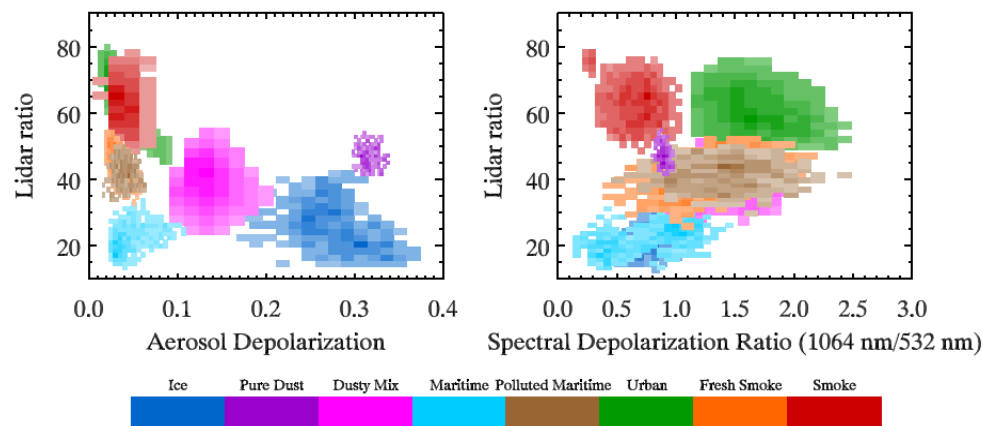
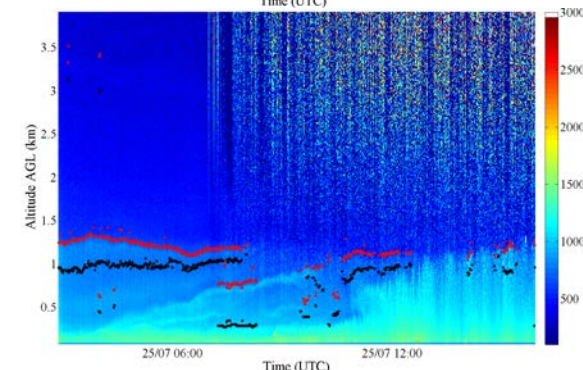
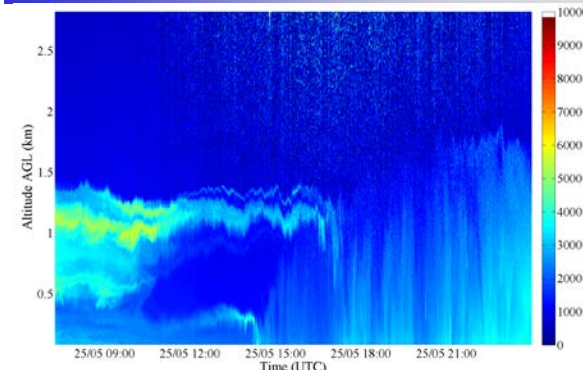
# Ground-Based LIDAR

## AFIT's R-MAN 510

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- Diode Pumped Tripled Nd:YAG
- Parallel / Cross channels (355 nm)
- Nitrogen Raman Channel (387 nm)
  - 355 nm light backscatters at 387 nm, to find total extinction
  - Record LIDAR ratio for aerosol classification
- ~21 km cloud ceiling
  - ~2 km aerosol ceiling during day
  - ~12 km aerosol ceiling during night

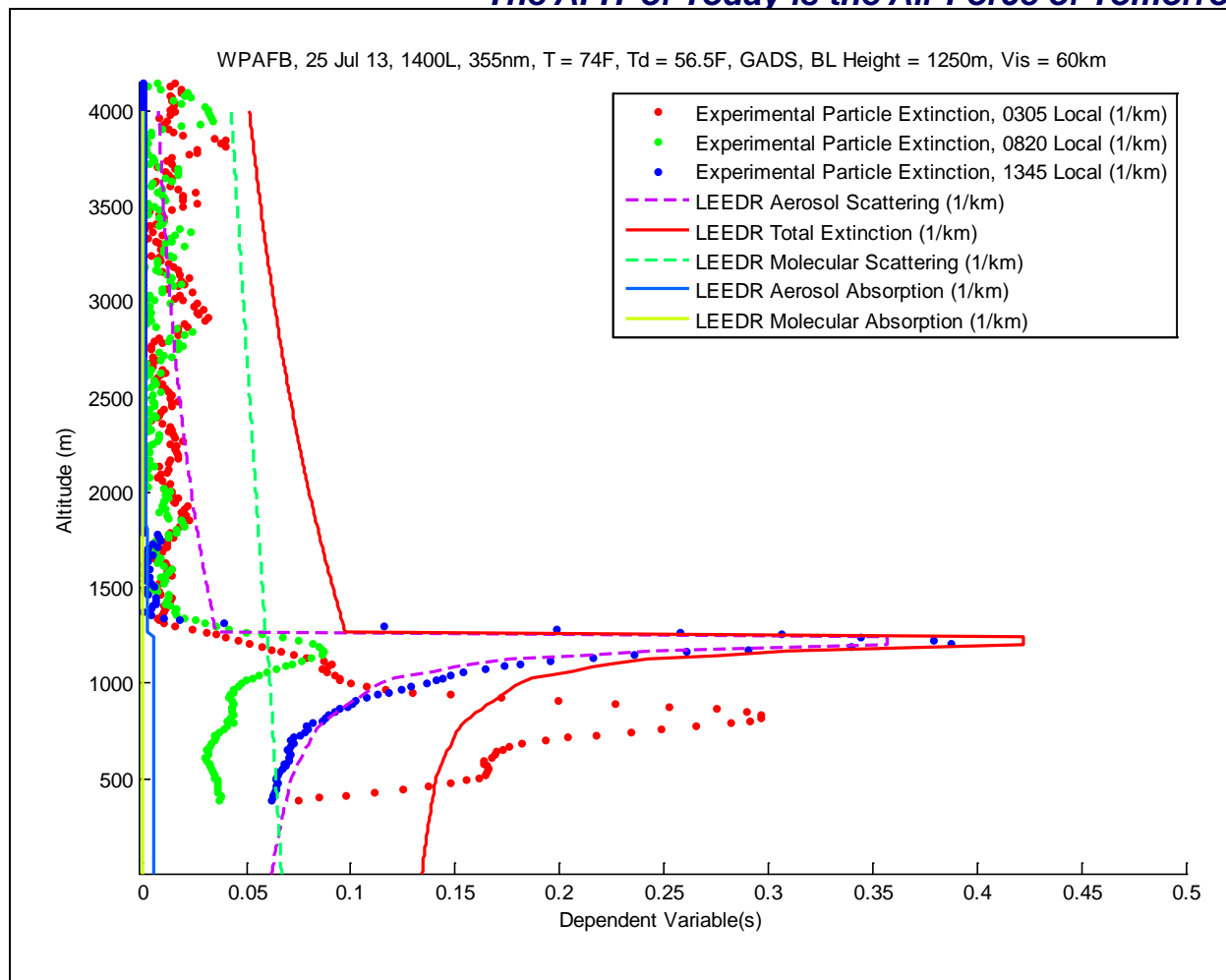


S. T. Fiorino, C. Rice, K. Keefer and M. Via, "LIDAR Validation Experiments of LEEDR Aerosol Boundary Layer Characterizations," in *Directed Energy Professional Society - Annual Directed Energy Symposium*, Huntsville, AL, 2014.



# Example Extinction Plot – WPAFB Validation

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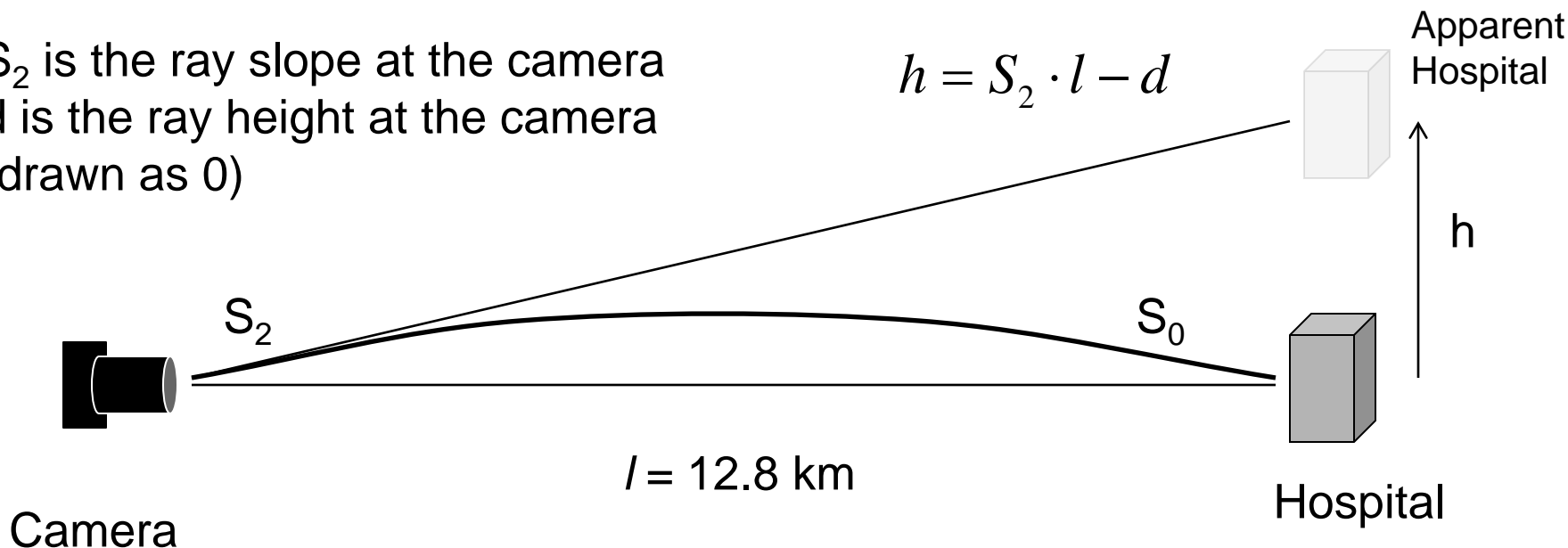
Example LEEDR plot using a BL height of 1250 m at WPAFB ExPERT site, GADS summer aerosols, visibility of 60 km, and surface conditions for WPAFB for 25 Jul 13 at 1400L (T = 23°C, T<sub>d</sub> = 13 °C) vs. measurements from the roof of Bldg 640 conducted with a lidar operating at 355 nm

# Assessment of Refractive Index Gradient Variability from Time Lapse Imagery

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$S_2$  is the ray slope at the camera  
 $d$  is the ray height at the camera  
 (drawn as 0)

$$h = S_2 \cdot l - d$$



$$h = \left( \int_0^l \kappa(x') dx' + S_0 \right) \cdot l - \int_0^l \int_0^{x'} \kappa(x'') dx'' dx' + S_0 l = \int_0^l x \cdot \kappa(x') dx'$$

The image shift is proportional to the linearly weighted change to the curvature along the path, with zero weight at the source.

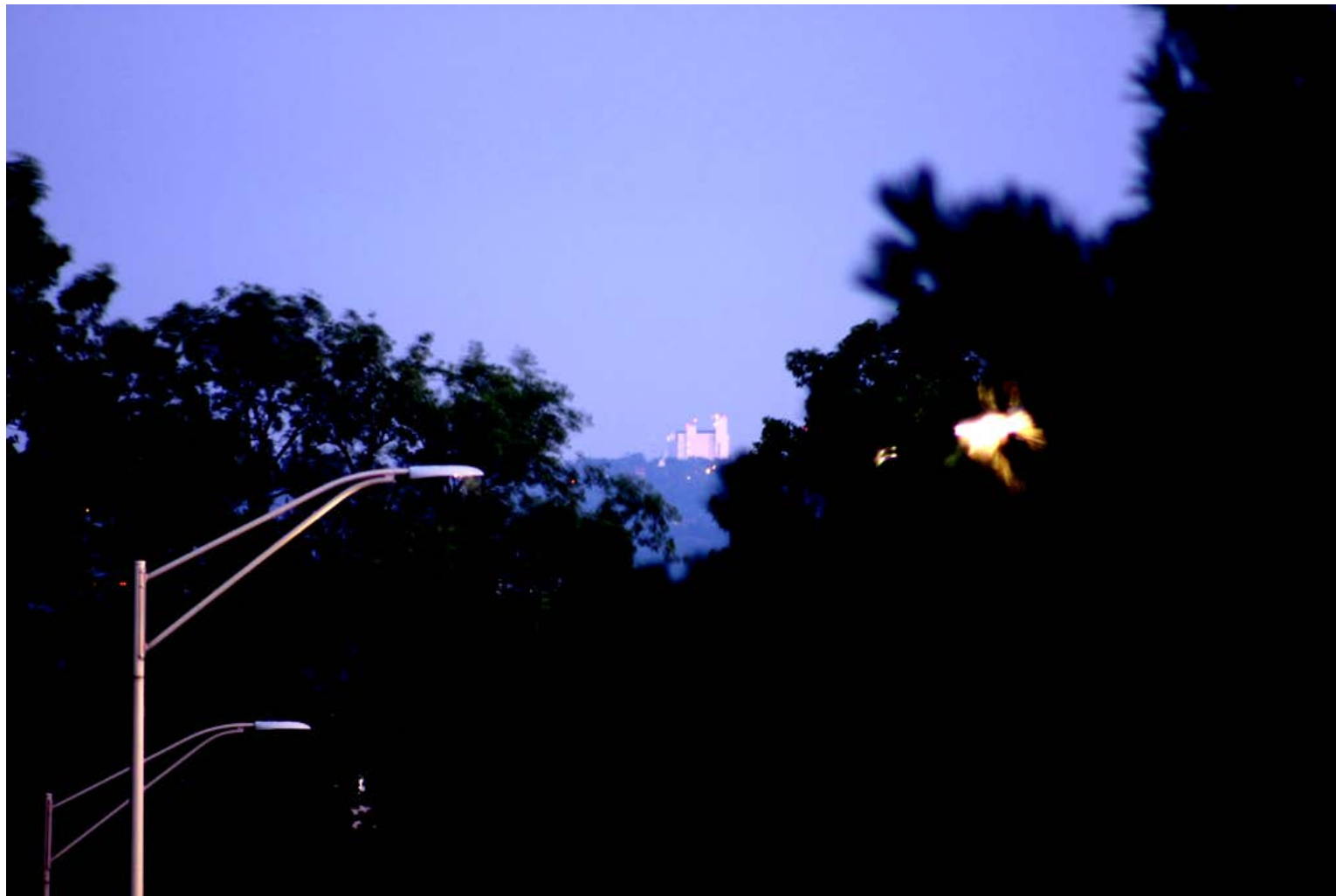


# Sfc. Database & PITBUL

## View from 644



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Hospital at center is 12.8 km distant.

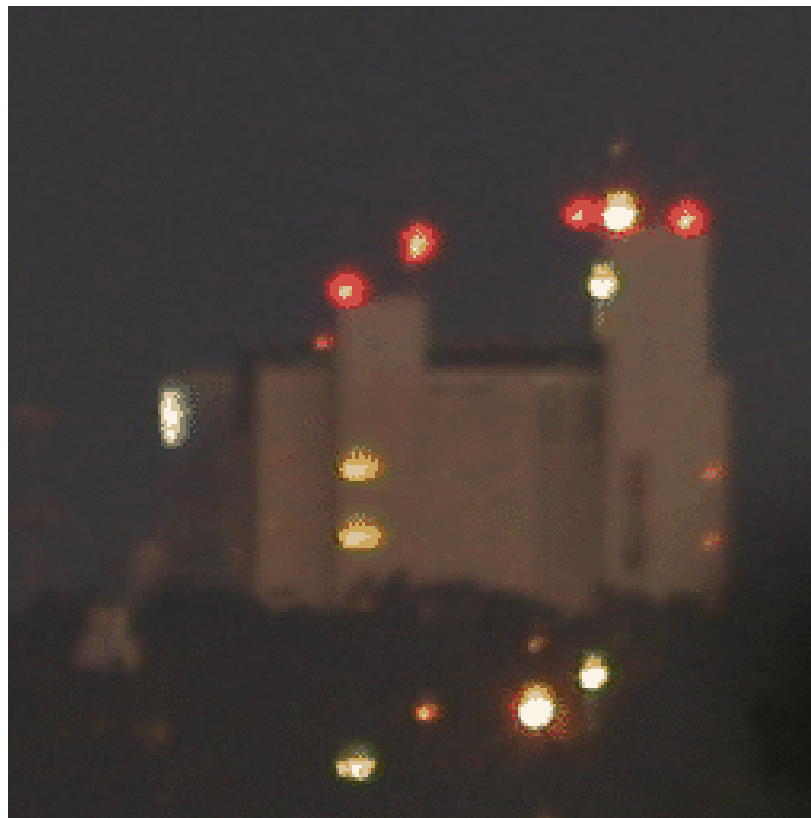


# Assessment of Refractive Index Gradient Variability from Time Lapse Imagery



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## 25 July 2014



256 x 256 pixels. 10 minutes between images.  
Clearest day we took pictures.

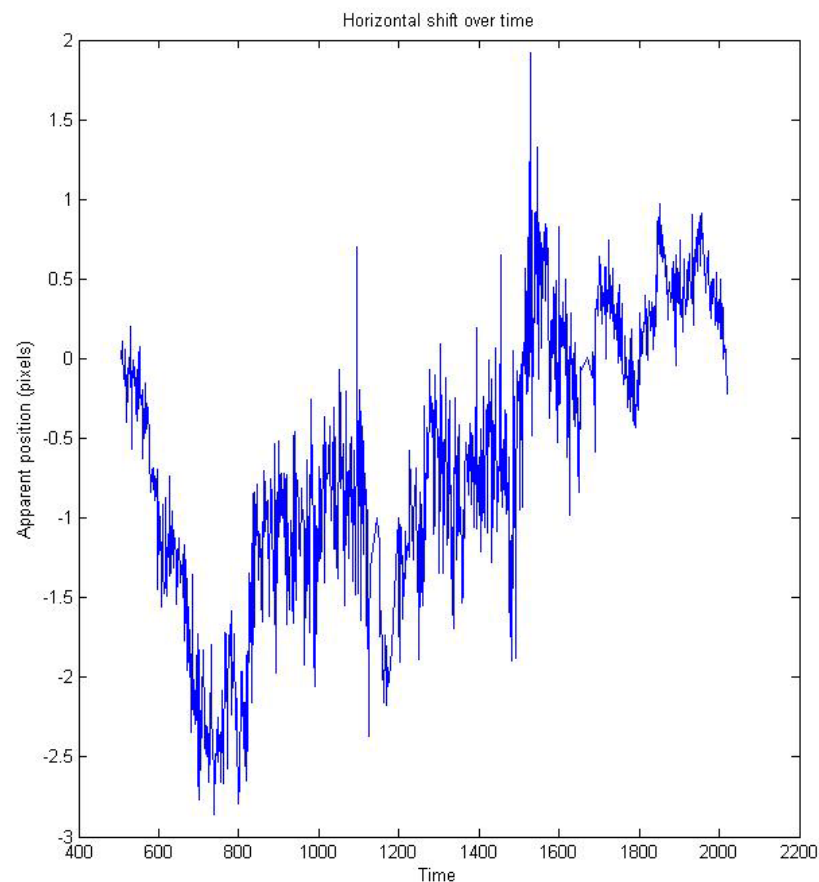
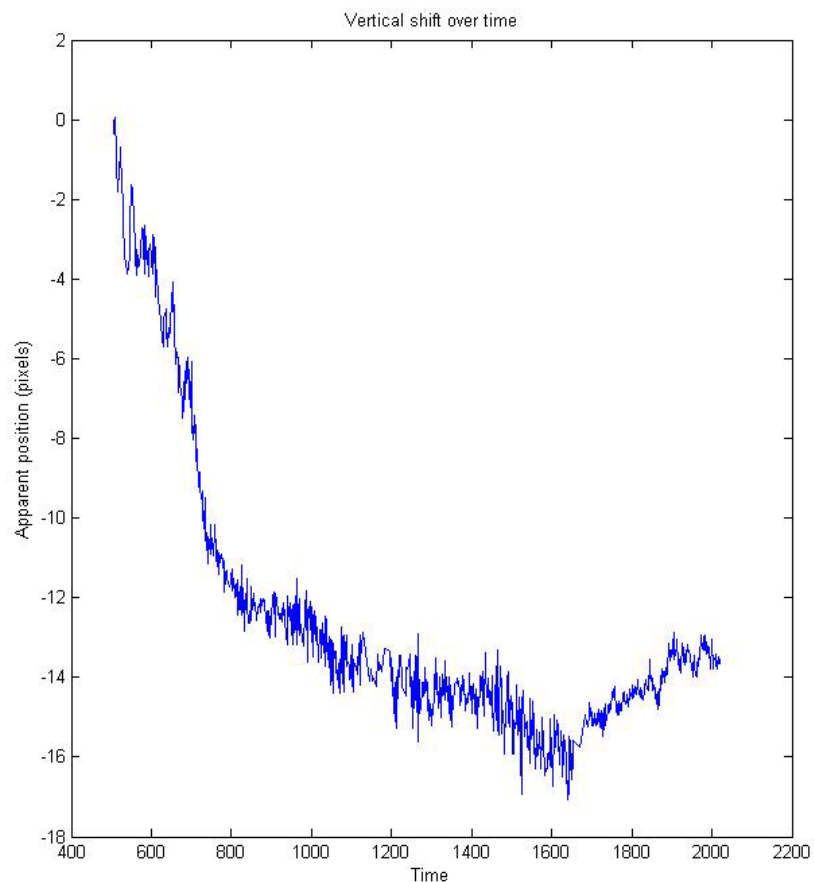


# Assessment of Refractive Index Gradient Variability from Time Lapse Imagery



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07/25/2014

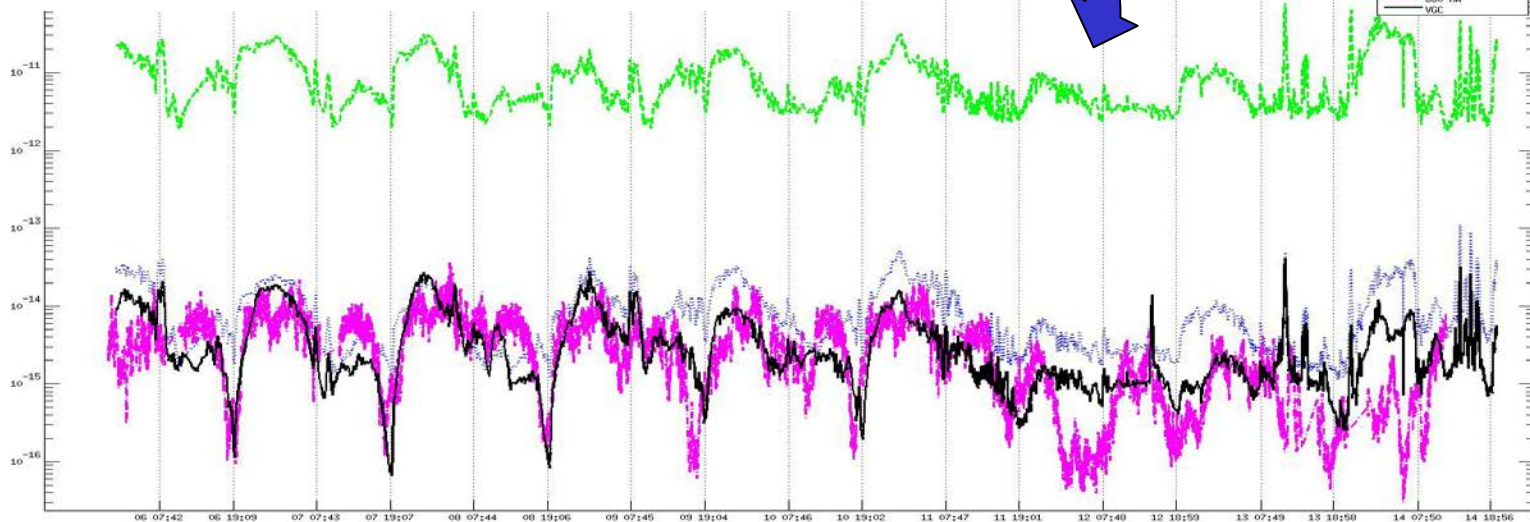
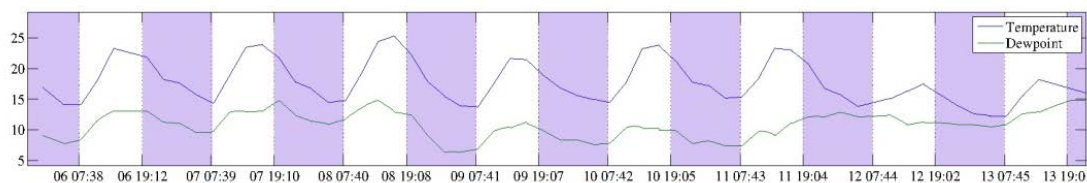
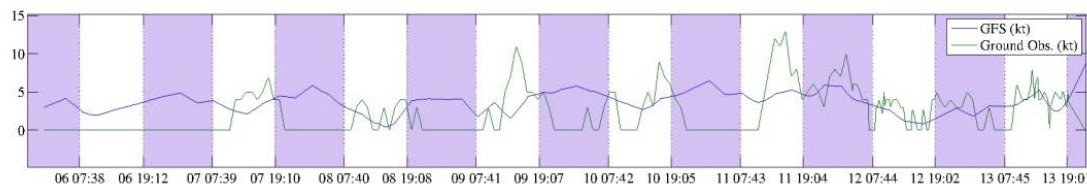
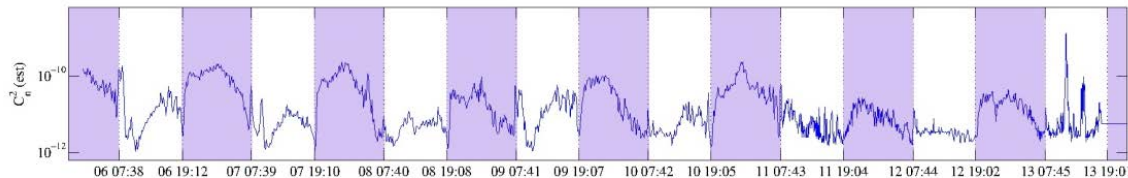




# Unique $C_n^2$ Measurement Using Wx Radar

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- Uncorrected Wx radar  $C_n^2$  values are adjusted for wind-driven eddies, ground reflections, and wavelength (humidity) using NWP gridded data rather than obs. or balloon data



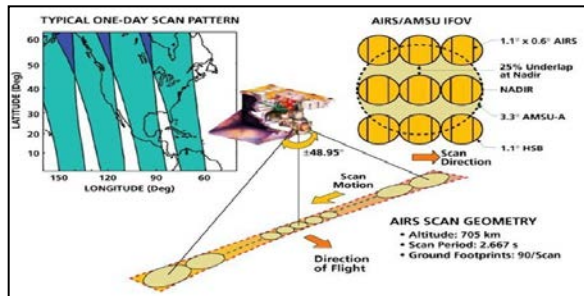
Optics Express paper,  
"Wavelength  
Correction for  $C_n^2$ "  
in draft



# Methodology

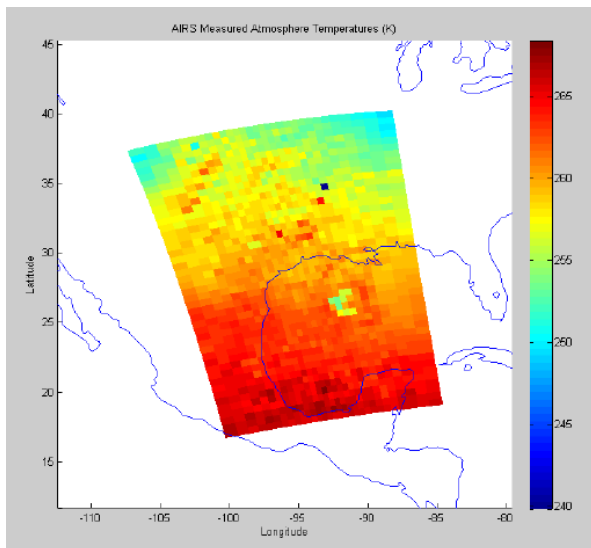
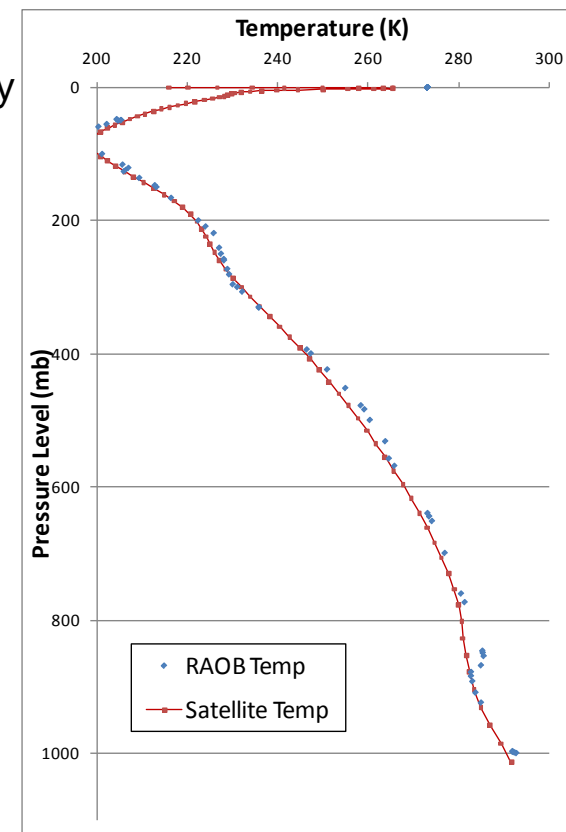
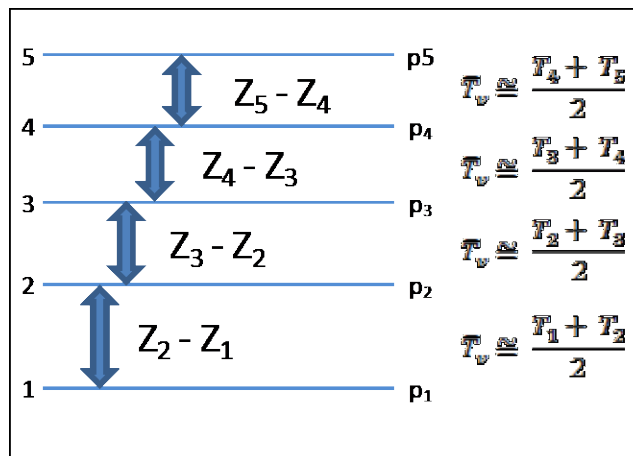
## Satellite-Derived $C_n^2$

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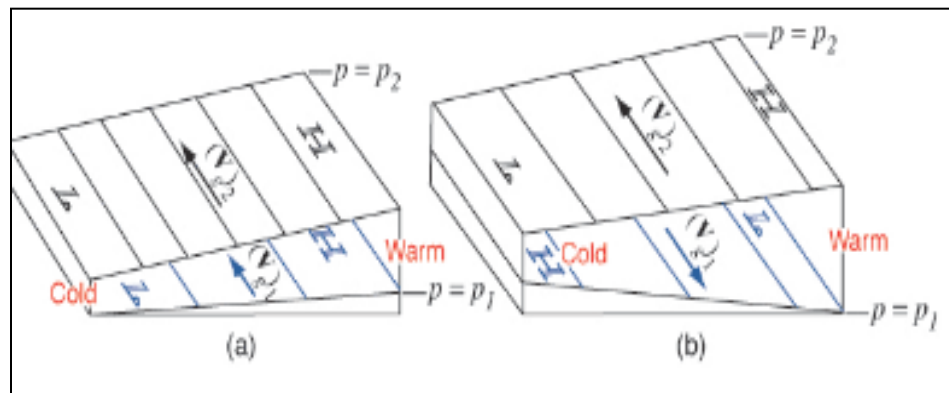
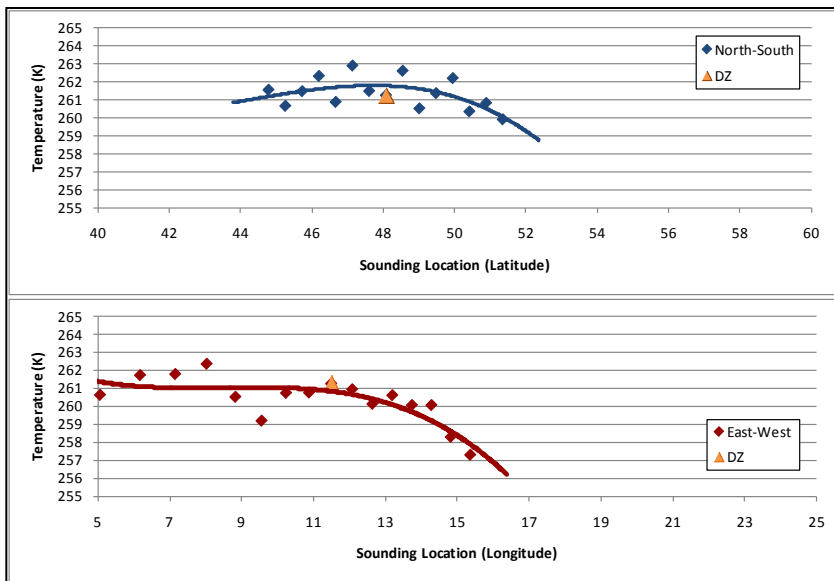
- Atmospheric IR sounder (AIRS) and Advanced Microwave Sounding Unit (AMSU) on polar orbiting Aqua Satellite
- Global coverage provides vertical temperature profile (surface to 80km) at each sounding location
- Height assigned to pressure levels by adding each layer's thicknesses

$$Z_2 - Z_1 = \frac{R_d \bar{T}_v}{g_0} \ln \left[ \frac{p_1}{p_2} \right]$$



# Thermal Wind Relationship

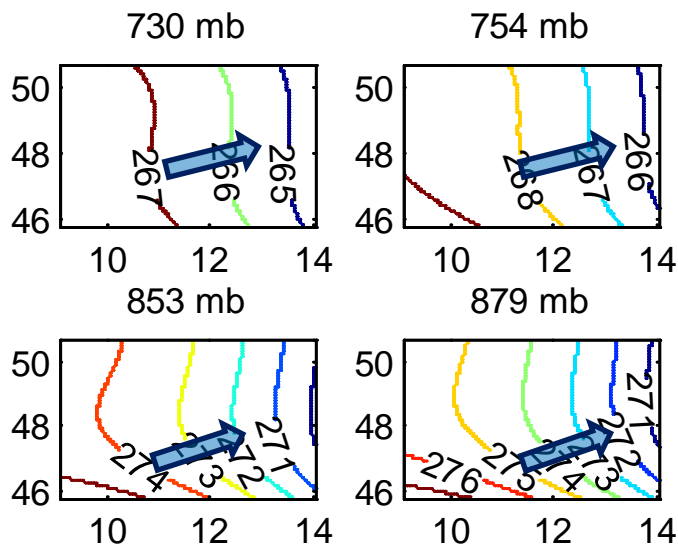
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$$\frac{\partial u_g}{\partial z} = -\frac{g}{f T} \left[ \left( \frac{\partial T}{\partial y} \right)_z + \frac{\partial T}{\partial z} \left( \frac{\partial z}{\partial y} \right)_p \right]$$

$$\frac{\partial v_g}{\partial z} = \frac{g}{f T} \left[ \left( \frac{\partial T}{\partial x} \right)_z + \frac{\partial T}{\partial z} \left( \frac{\partial z}{\partial x} \right)_p \right]$$

g – acceleration due to gravity  
f – Coriolis parameter  
T – temperature  
p – atmospheric pressure  
z – geometric height

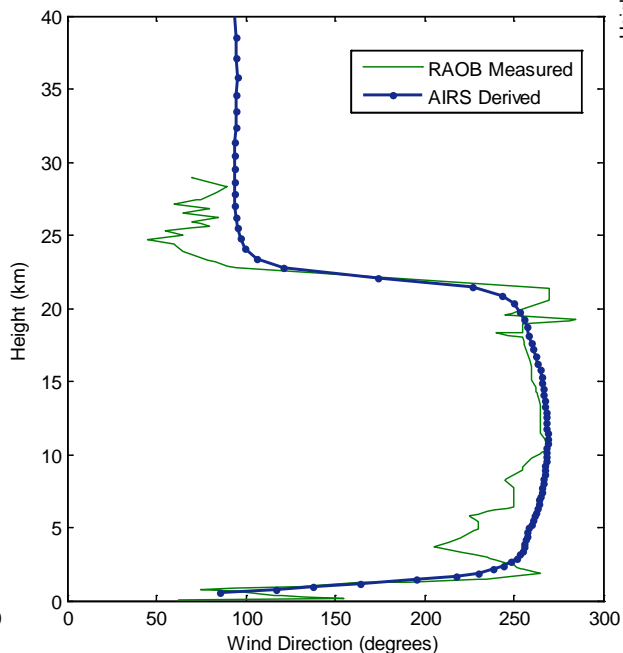
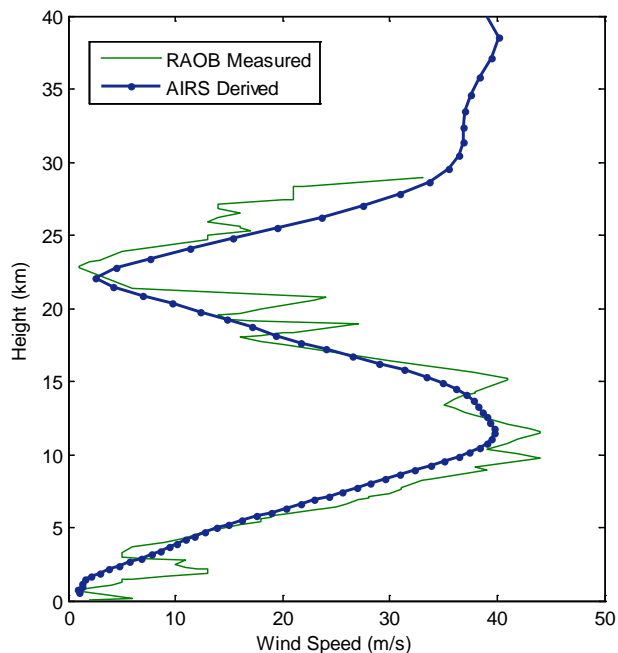


- J. M. Wallace and P. V. Hobbs, "Atmospheric Science: An Introductory Survey," (Elsevier Academic Press, Burlington, MA, 2006), 2nd ed.
- H. B. Bluestein, "Synoptic-Dynamic Meteorology in Midlatitudes, volume 1," (Oxford University Press, New York, 1992).

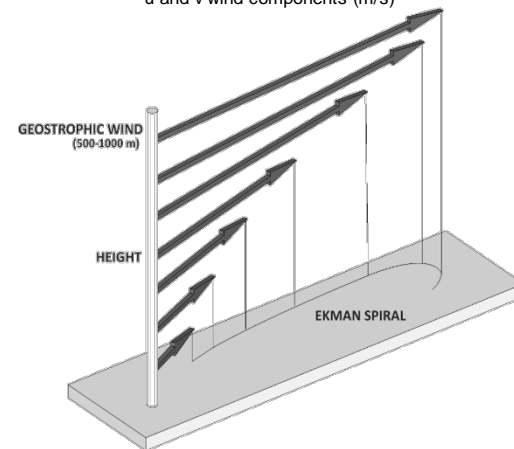
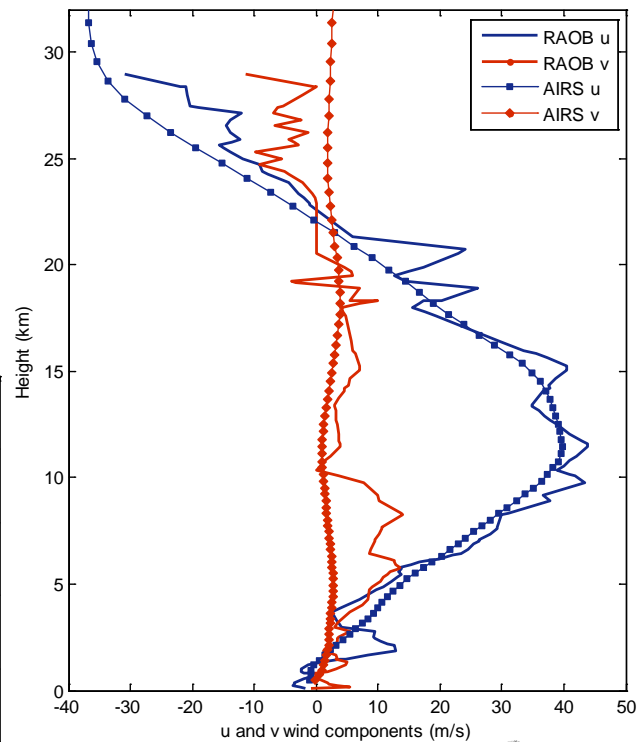
# AIRS Derived Wind Profiles

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Wind profile from 1250 UTC AIRS temperature data compared with Anchorage 1200 UTC rawinsonde



11 Apr 2014 1250 UTC, Anchorage, AK



# Calculation of $C_n^2$

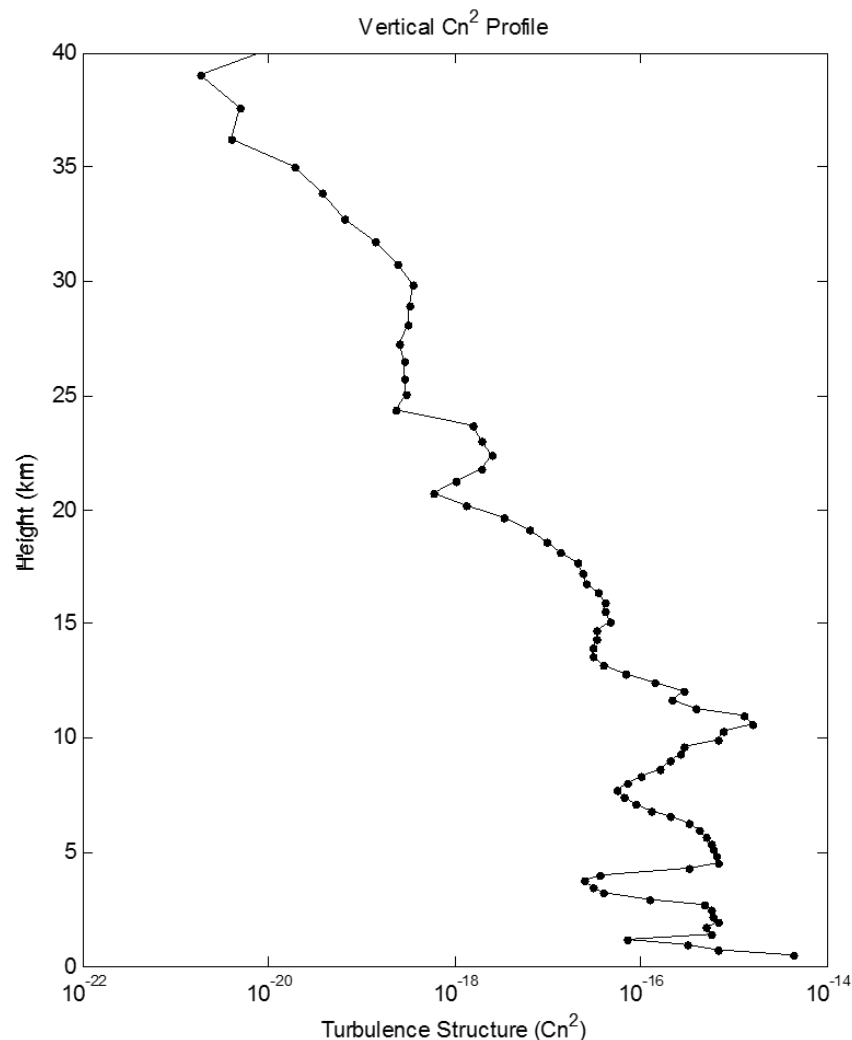
*The AFIT of Today is the Air Force of Tomorrow.*

$$C_n^2 = \left( 79 \times 10^{-6} \frac{P}{T^2} \right) C_T^2$$

$$C_T^2 = a^2 \left( \frac{K_H}{K_M} \right) L_o^{\frac{4}{3}} \left( \frac{\partial \theta}{\partial Z} \right)^2$$

$$\frac{\partial \theta}{\partial Z} = \left( \frac{\partial T}{\partial Z} + \gamma_d \right)$$

$$C_n^2 = 2.8 \frac{K_H}{K_M} \left( 79 \times 10^{-6} \frac{P}{T^2} \right)^2 L_o^{4/3} \left( \frac{\partial T}{\partial Z} + \gamma_d \right)^2$$





# Incorporation of Vertical Wind Gradient



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- Richardson Number and Eddy Diffusivity calculation

$$Ri = \left( g \frac{\partial \ln \theta}{\partial z} \right) / \left( \frac{\partial V}{\partial z} \right)^2$$

$L_o$  = mixing length  
Effectively an outer scale;  
Estimated at ~100 to 200 m

$$\frac{K_H}{K_M} = \begin{cases} \frac{1}{7Ri}, & \text{for } Ri \geq 1, \\ \frac{1}{6.873Ri + \frac{1}{1+6.873Ri}}, & \text{for } 0.01 < Ri \leq 1. \end{cases}$$

$$C_n^2 = 2.8 \frac{K_H}{K_M} \left( \frac{(79 \times 10^{-6} P)}{T^2} \right)^2 L_o^{4/3} \left( \frac{\partial T}{\partial Z} + \gamma_d \right)^2$$

R. J. Alliss and B. D. Felton, "Validation of Optical Turbulence Simulations from a Numerical Weather Prediction Model in Support of Adaptive Optics Design", Proceedings of the Advanced Maui Optical and Space Surveillance Technologies Conference, Wailea, Maui, Hawaii, September 1-4, 2009, Ed.: S. Ryan, The Maui Economic Development Board., p.E54.

J. O. Kondo, O. Kanechika, and N. Yasuda, "Heat and momentum transfers under strong stability in the atmospheric surface layer," Journal Atmos. Sci., 35, 1012-1021; 1978.

V. Tatarskii, "The effects of the turbulent atmosphere on wave propagation," translation, Published for NOAA by the Department of Commerce and the National Science Foundation, Washington D.C. (1971). Israel Program for Scientific Translations.

# Effect of Smooth Temperature Profile on Gradient Richardson Number

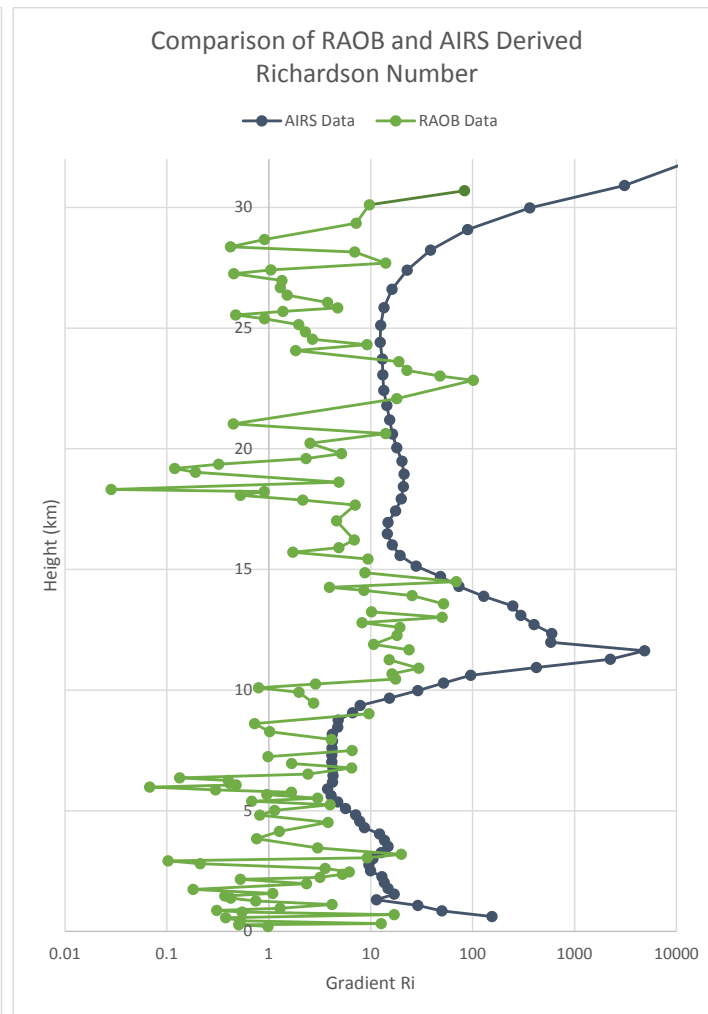
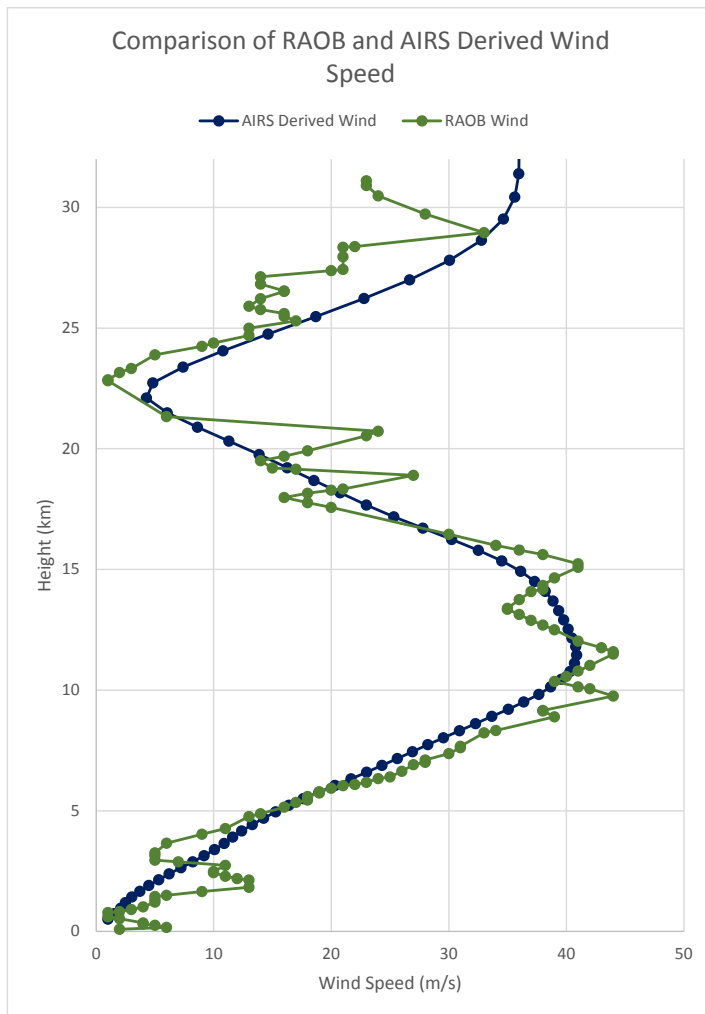
*The AFIT of Today is the Air Force of Tomorrow.*

$$Ri = \left( g \frac{\partial \ln \theta}{\partial z} \right) / \left( \frac{\partial V}{\partial z} \right)^2$$

$$\theta = T \left( \frac{1000}{P} \right)^{\frac{R}{c_p}}$$

g – accel. due to gravity  
 $\Theta$  – potential temperature  
 z – geometric height  
 V – horizontal wind speed  
 T – temperature  
 P – pressure  
 R – gas constant of air  
 $c_p$  – specific heat of air

$$R/c_p = 0.286$$







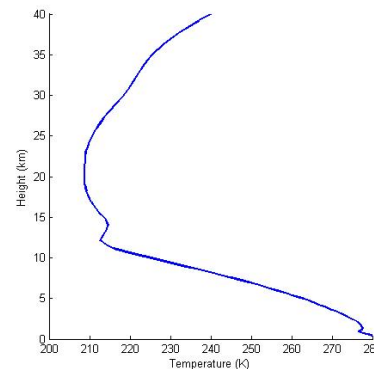
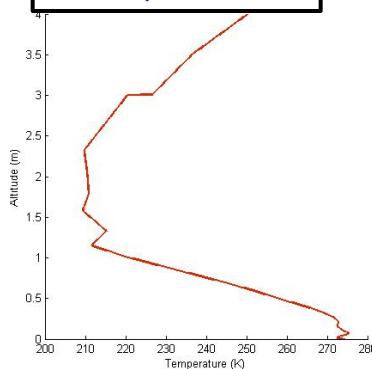
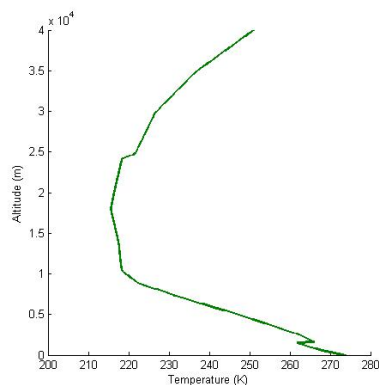
# Results

## Satellite Atmosphere Soundings: Winds / Temp Comparisons

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Dayton OH 12 Jan 2014, 18Z

### Temperature

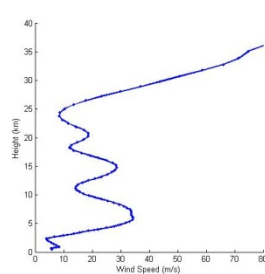
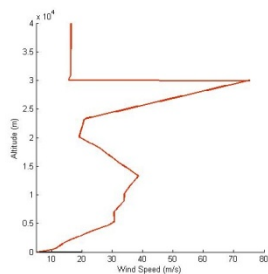
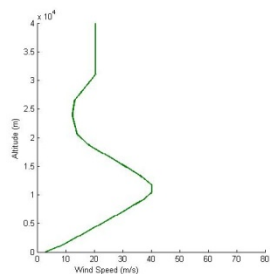


Climo-derived

NWP-derived

AIRS-derived

### Wind Speed

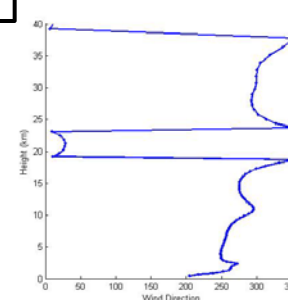
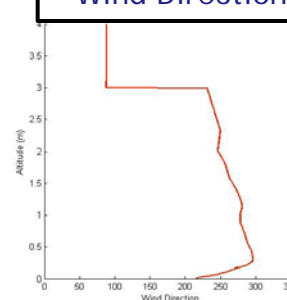
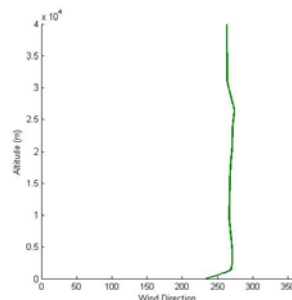


Climo-derived

NWP-derived

AIRS-derived

### Wind Direction



Climo-derived

NWP-derived

AIRS-derived

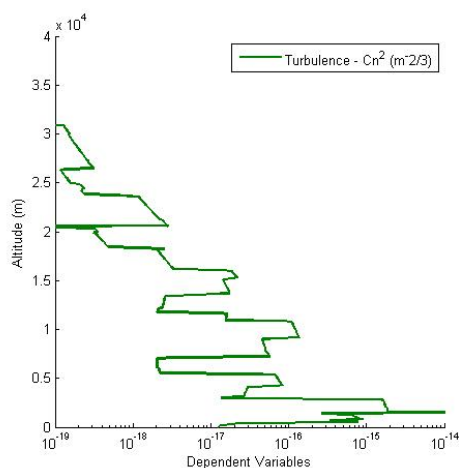
### Applying

$K_H/K_M$  - modified Tatarski

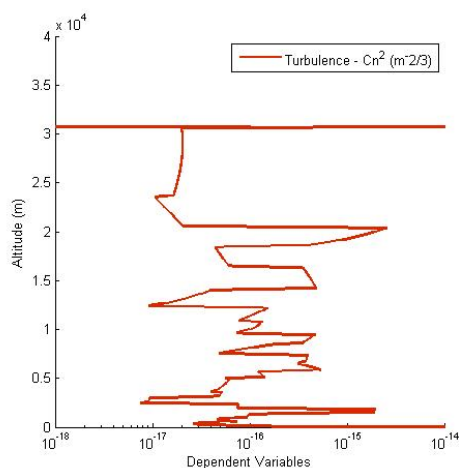
$$C_n^2 = 2.8 \frac{K_H}{K_M} \left( \frac{(79 \times 10^{-6} P)}{T^2} \right)^2 L_o^{4/3} \left( \frac{\partial T}{\partial Z} + \gamma_d \right)^2$$

$$C_v^2(z) = (0.714) C_n^2(z) \left( \partial \frac{\langle \mathbf{v}(z) \rangle}{\partial z} \right)^2 (\nabla \langle n \rangle)^{-2}$$

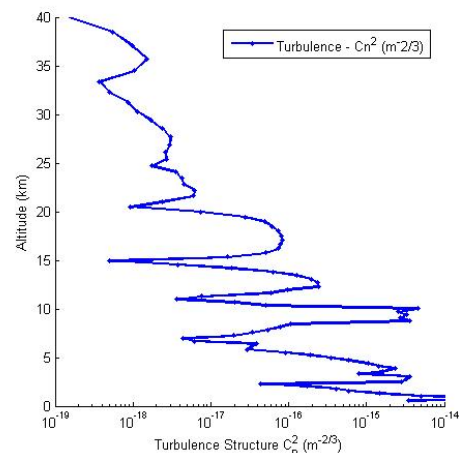
Comparable  $C_n^2$  Profiles for Dayton OH 12 Jan 2014, 18Z



Climo-derived



NWP-derived



AIRS-derived

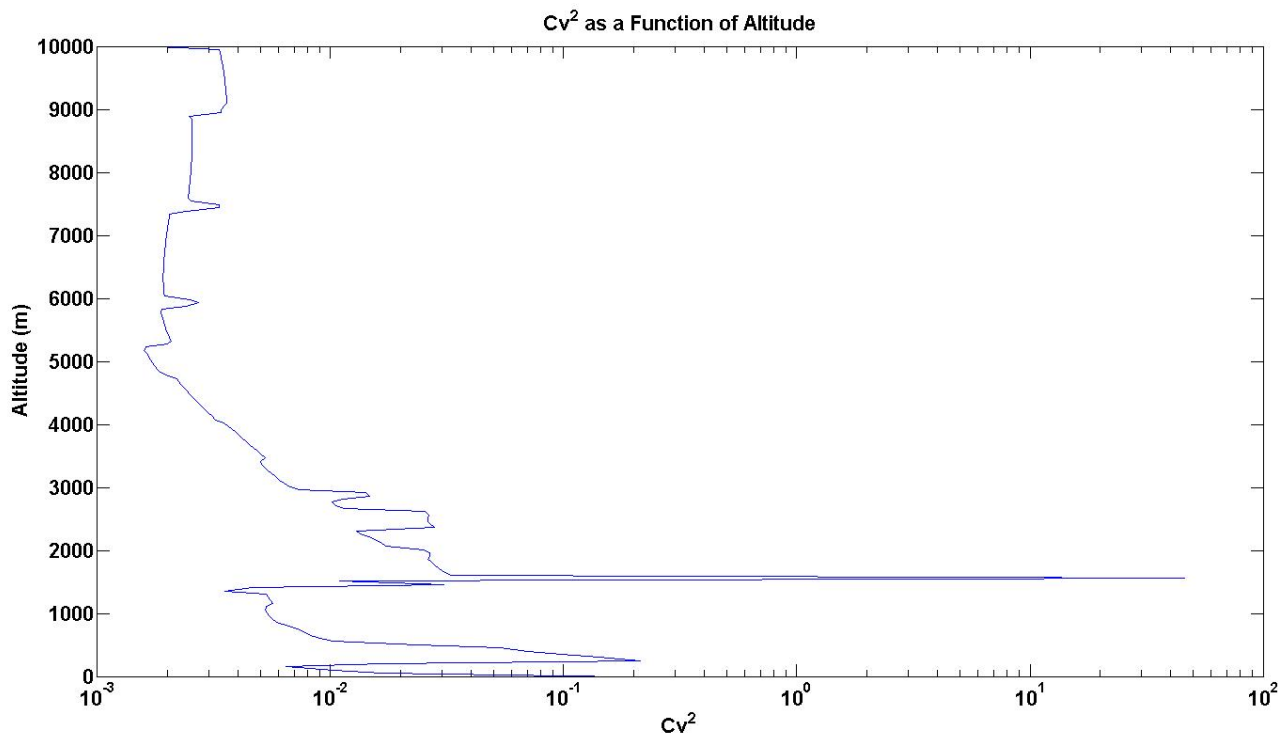
**Satellite-derived optical turbulence with enhanced global 4D resolution can offer flexible radiative transfer solutions**

# $C_v^2$ from Temperature Profiles

*The AFIT of Today is the Air Force of Tomorrow.*

- Fung 2003 (SAIC AR-45 Report, corrected Eq 32), a velocity structure constant ( $C_v^2$ ) profile is related to refractive index profile

$$C_v^2(z) = (0.714) C_n^2(z) \left( \partial \frac{\langle \mathbf{v}(z) \rangle}{\partial z} \right)^2 (\nabla \langle n \rangle)^{-2}$$



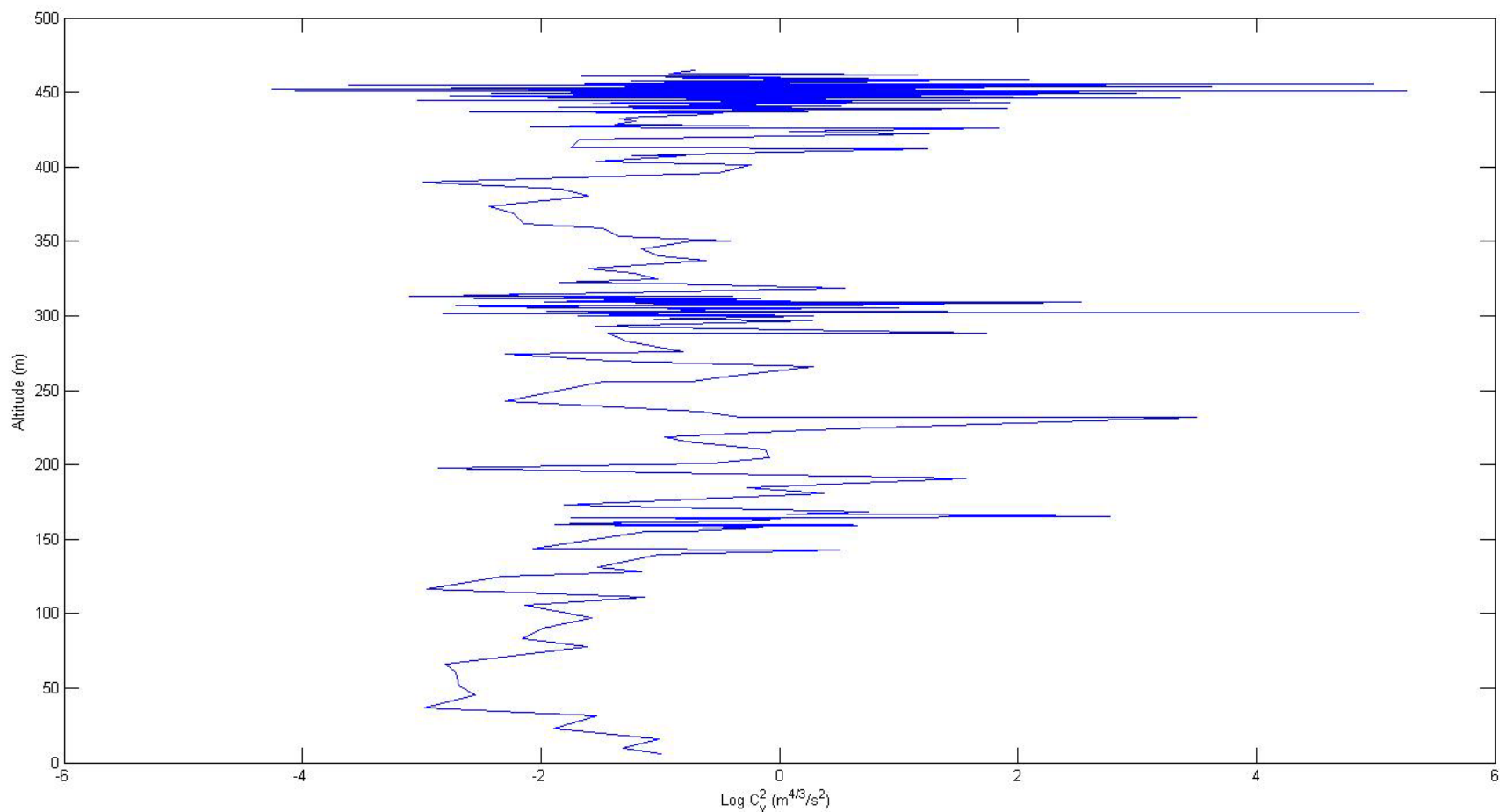


# $C_v^2$ from Temperature Profiles



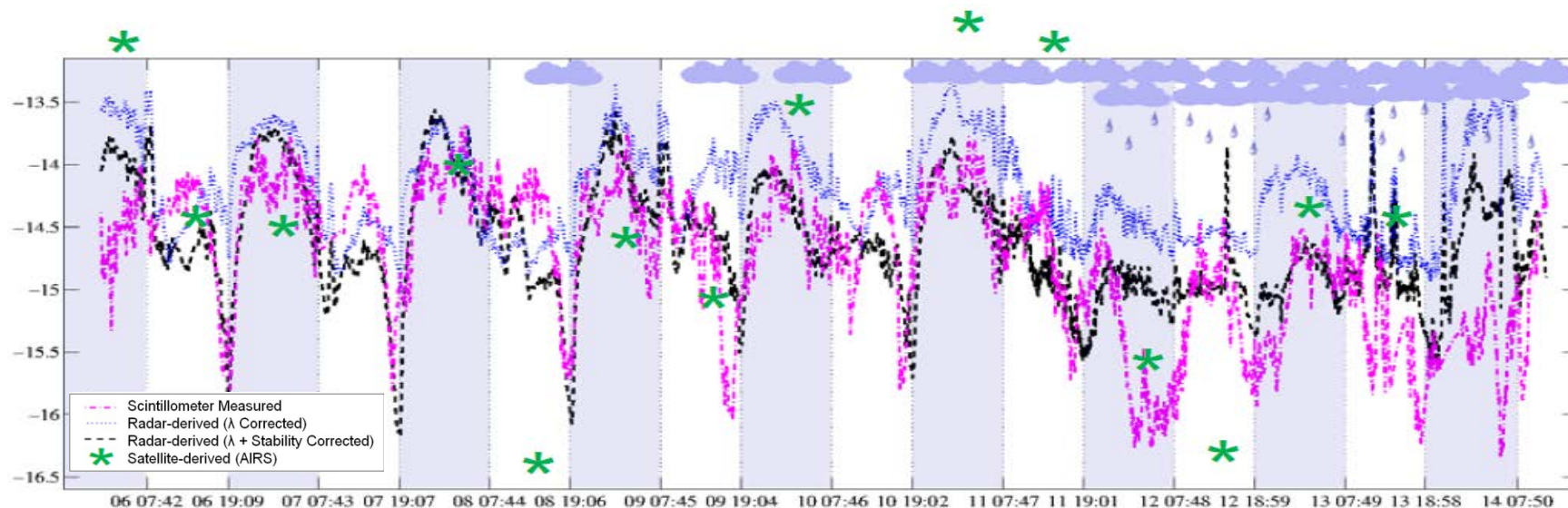
*The AFIT of Today is the Air Force of Tomorrow.*

- Micro-meteorological data for profile below was collected by Tim Chavez at HELSTF NM on 23 Jul 13



# Optical Turbulence Characterization by Refractive Index Structure Function

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- Radar-derived and satellite-derived index of refraction structure function values ( $\text{Log}_{10} C_n^2$ ) compared with scintillometer measured  $\text{Log}_{10} C_n^2$  along a 7-km path in Dayton, OH



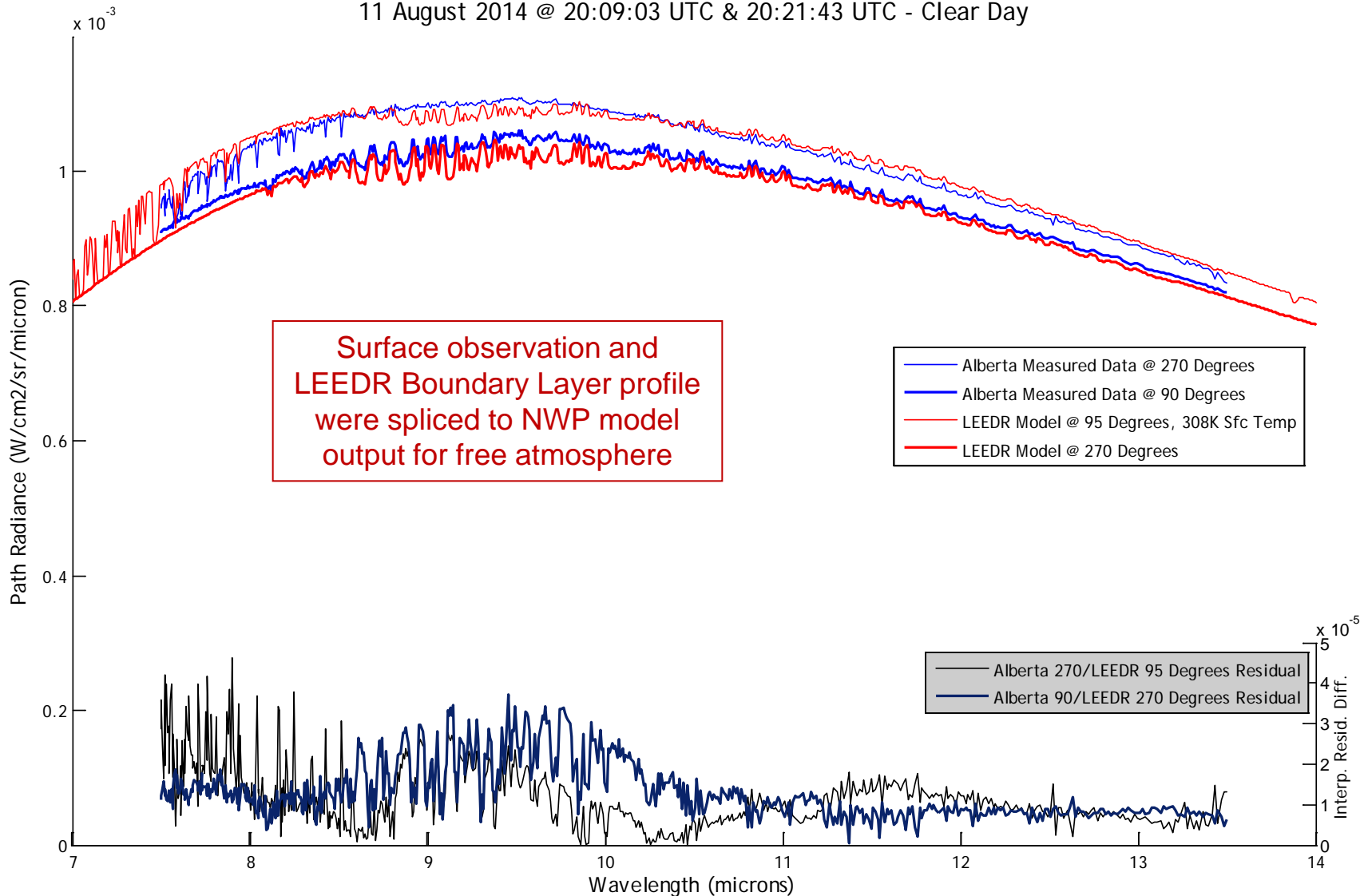


# LEEDR Comparison with Field Data Collected in Southern Alberta



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Alberta vs LEEDR Path Radiance 90 & 270 Degrees- Single Scattering  
11 August 2014 @ 20:09:03 UTC & 20:21:43 UTC - Clear Day



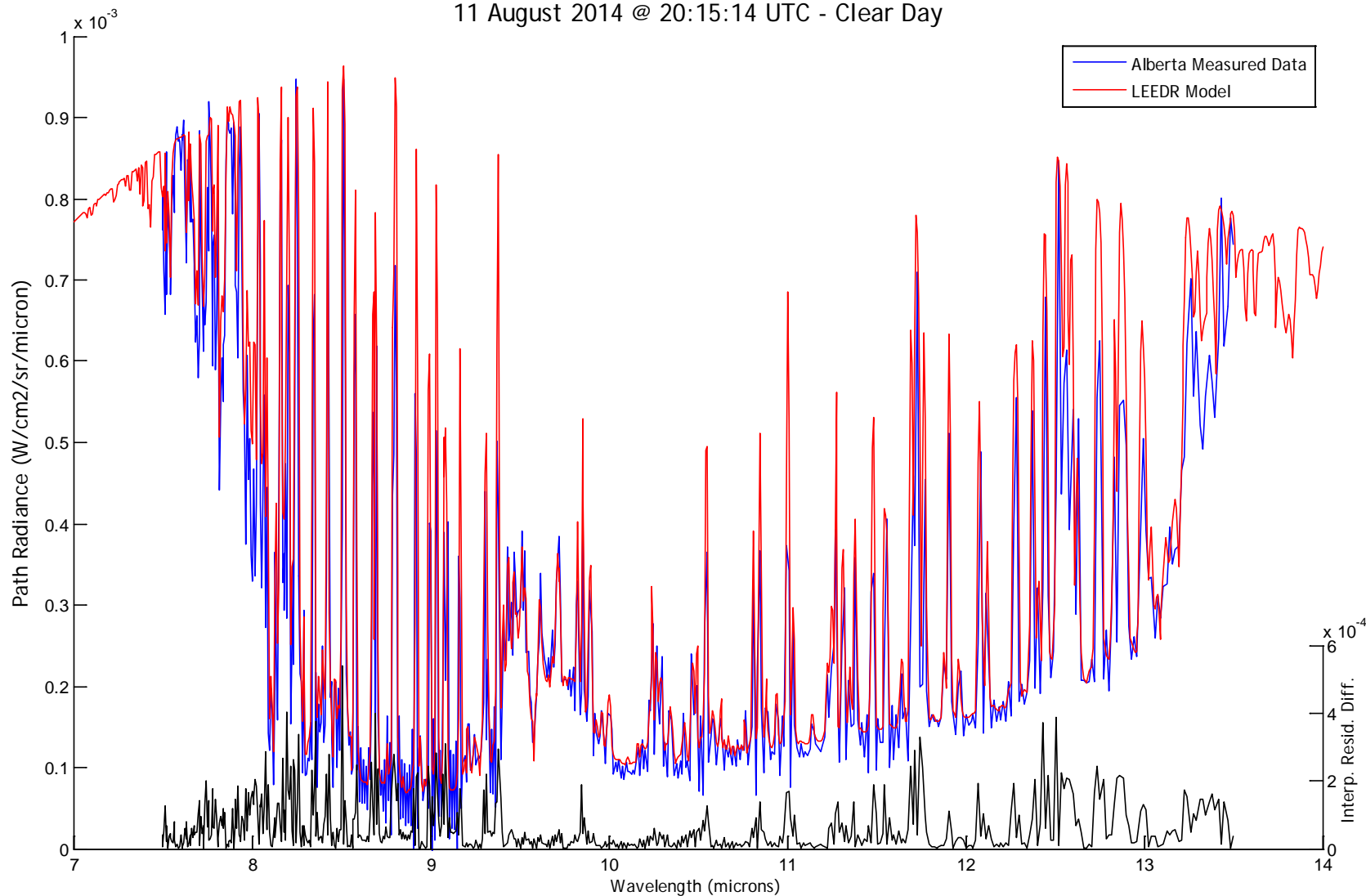


# LEEDR Comparison with Field Data Collected in Southern Alberta



*The AFIT of Today is the Air Force of Tomorrow.*

Alberta vs LEEDR Path Radiance 180 Degrees- Single Scattering  
11 August 2014 @ 20:15:14 UTC - Clear Day





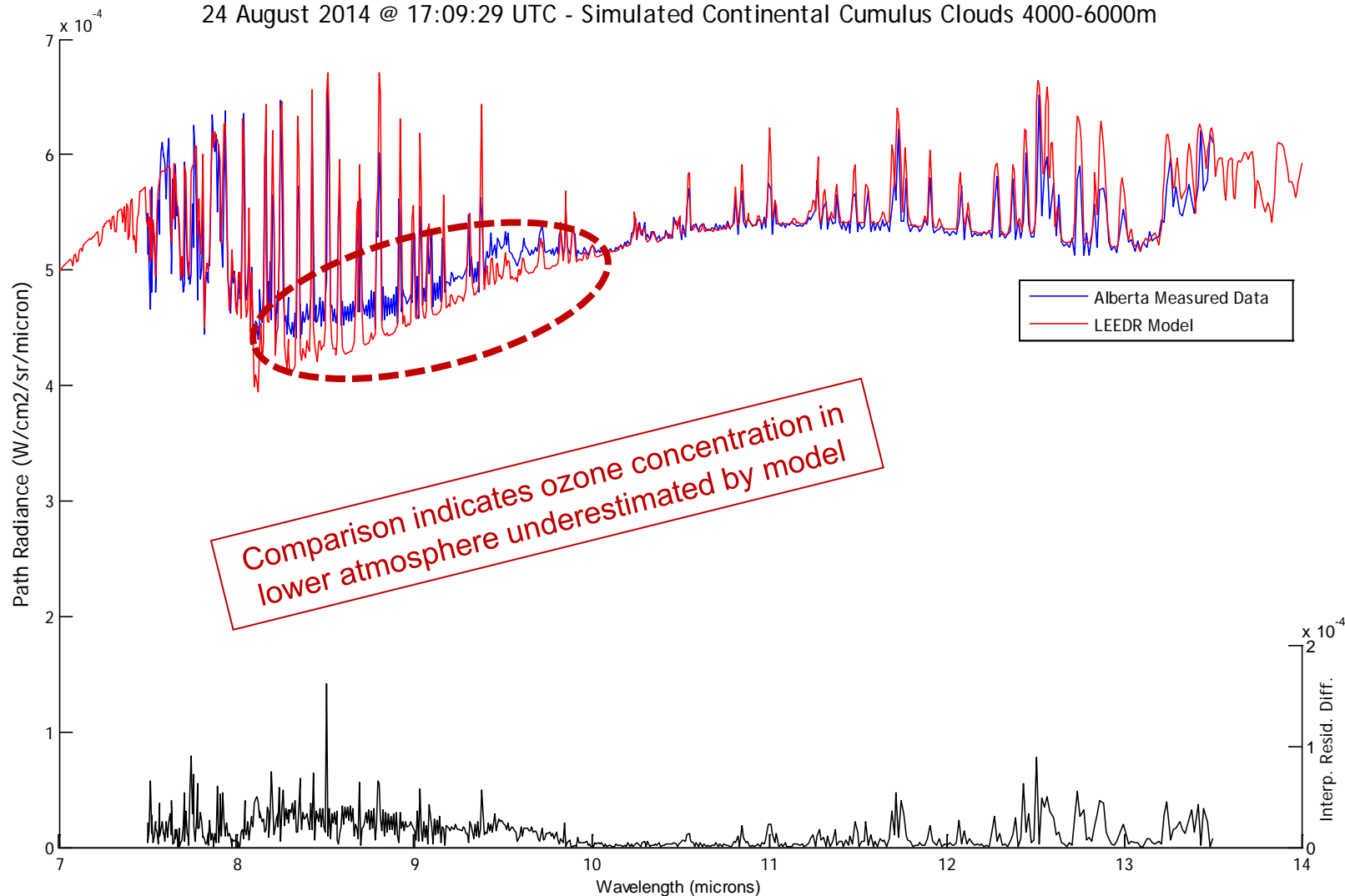
# LEEDR Comparison with Field Data Collected in Southern Alberta



*The AFIT of Today is the Air Force of Tomorrow.*

Alberta vs LEEDR Path Radiance 180 Degrees- Single Scattering

24 August 2014 @ 17:09:29 UTC - Simulated Continental Cumulus Clouds 4000-6000m





# Conclusions



*The AFIT of Today is the Air Force of Tomorrow.*

- Novel methods to obtain temperature, winds, turbulence, cloud base and top heights, and aerosol extinction values through a combination of NEXRAD and satellite-based remote sensor data enhance fundamental radiative transfer calculations (e.g. path radiance and refraction, optical turbulence)
- 4D gridded structure functions of temperature,  $C_T^2$ , refractive index,  $C_n^2$ , and wind velocity,  $C_v^2$  will immediately benefit directed energy simulation tools (e.g. AFIT's High Energy Laser Tactical Decision Aid) and applications (e.g. laser communication system design)
- Higher resolution path radiance solutions can benefit industry and government EO/IR sensor capabilities



# Future Work



*The AFIT of Today is the Air Force of Tomorrow.*

- Model Verification and Validation (V&V)
  - Next intended use to be validated: remote sensing
  - Results accuracy: compare with field test campaigns
- Expand NWP data integration to higher resolution weather models (WRF, AFWA models, and Fleet Numerical models)
  - Utilize this improved resolution gridded data in DE propagation models (e.g. AFIT's High Energy Laser End to End Operational Simulation and Tactical Decision Aid)
- Incorporate multiple-scattering calculations in DE propagation models and validate model's accuracy at shorter wavelengths





# AMERICAN METEOROLOGICAL SOCIETY

95th Annual Meeting 4 - 8 January 2015



Air Force Institute of Technology  
Center for Directed Energy  
Wright-Patterson AFB, Ohio



## Using Satellite, NWP, and Atmospheric Refraction Assessments to Enhance Radiative Transfer Characterizations for Remote Sensing and Directed Energy Applications

S. T. Fiorino<sup>1</sup>, D. C. Meier<sup>1</sup>, L. R. Burchett<sup>1,4</sup>, M. F. Via<sup>1,2</sup>, C. A. Rice<sup>1,3</sup>, B. J. Elmore<sup>1,3</sup>, and K. J. Keefer<sup>1,2</sup>  
Department of Engineering Physics

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[christopher.rice@afit.edu](mailto:christopher.rice@afit.edu)  
[kevin.keefer.ctr@afit.edu](mailto:kevin.keefer.ctr@afit.edu)

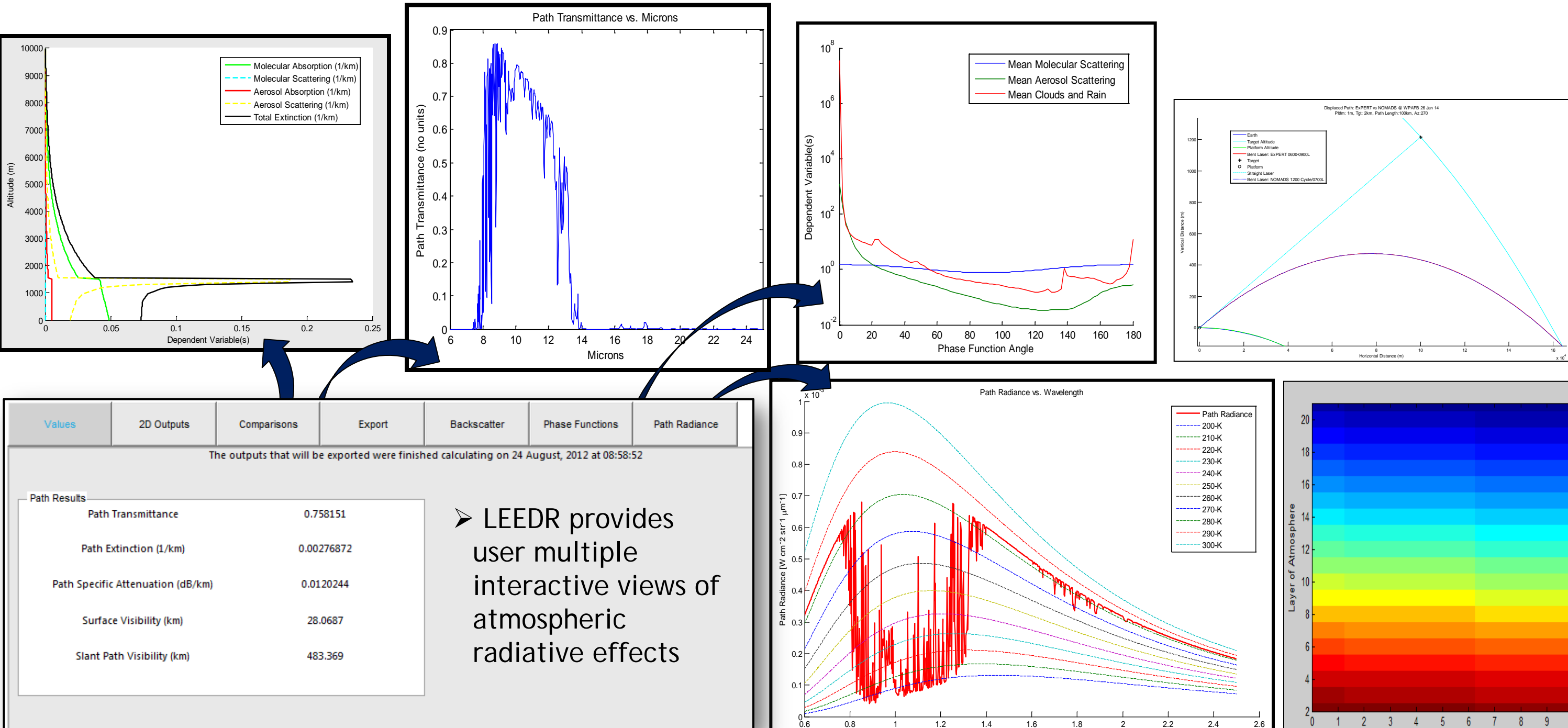
This study merges gridded numerical weather prediction (NWP) data from the NOMADS (NOAA National Operational Model Archive & Distribution System), satellite data from the Atmospheric Infrared Sounder (AIRS), Advanced Microwave Sounding Unit (AMSU), and Moderate-Resolution Imaging Spectroradiometer (MODIS) sensor suites, and makes comparisons to doppler radar data from NOAA's NEXRAD network and data from a Leosphere R-MAN 510 ultraviolet LIDAR (Light Detection and Ranging) unit to enhance radiative transfer modeling, inclusive of atmospheric refraction effects, and demonstrates the implications for remote sensing and laser propagation applications. The Laser Environmental Effects Definition and Reference (LEEDR) model's radiative transfer code was modified to ingest current and/or archived world-wide gridded numerical weather and satellite data, as well as probabilistic climatological information, thus enabling multi-dimensional realistic atmospheric profiles for traditional extinction analysis as well as more comprehensive light refraction and path radiance calculations. Implications for remote sensing applications are drawn directly from LEEDR and those for laser propagation by way of world-wide effectiveness analyses using the High Energy Laser End to End Operational Simulation (HELEEOS) and High Energy Laser Tactical Decision Aid (HELTDA). Collectively, these models enable the creation and application of numerically- or remote sensor-derived 4D profiles of temperature, pressure, water vapor content, optical turbulence, and atmospheric particulates and hydrometeors as they relate to line-by-line or band-averaged layer extinction coefficient magnitude at any wavelength from 350 nm to 8.6 m. Climatologically-based aerosol concentrations and associated optical properties are assumed for all scenarios.

### Simulation Tool:



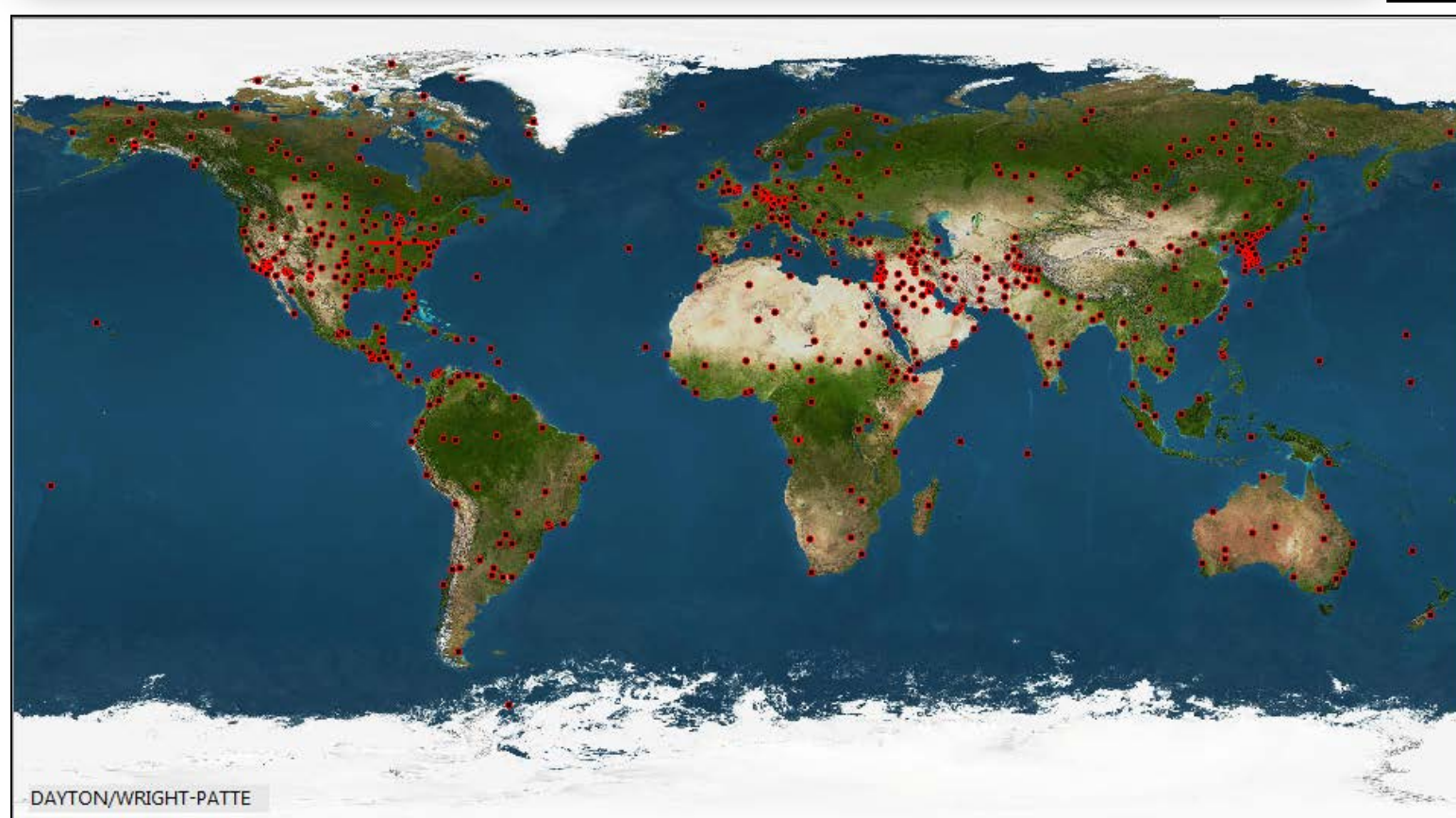
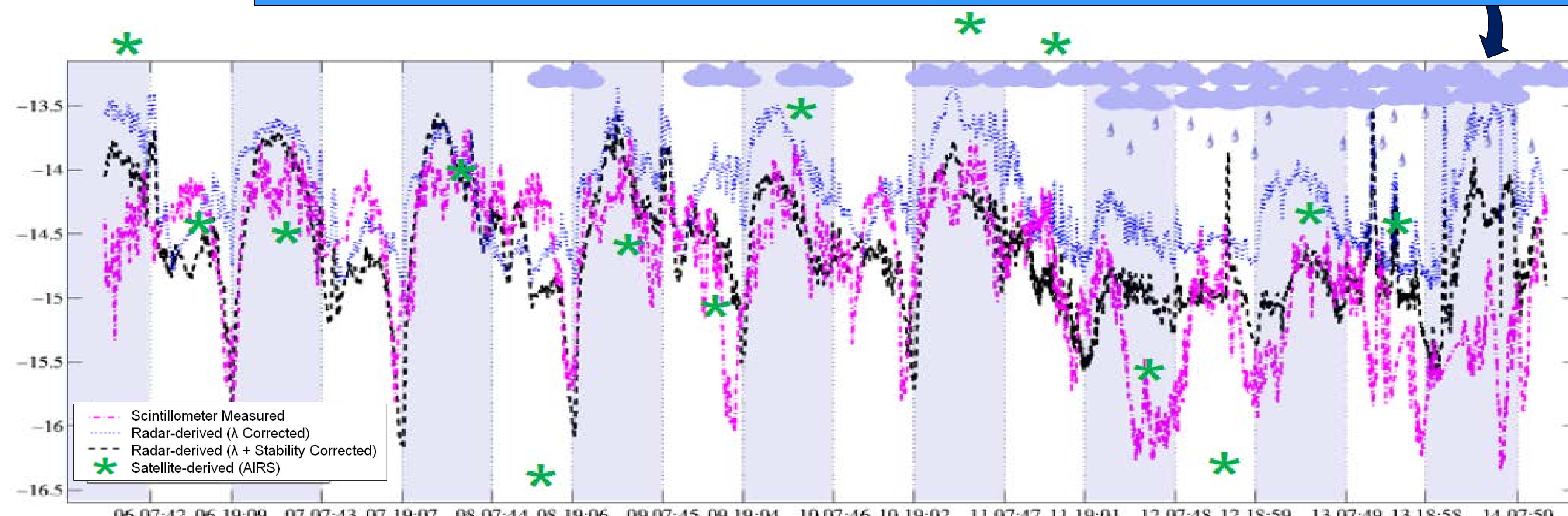
#### LEEDR radiative transfer code augmented by:

- Probabilistic Extreme and Percentile Environmental Reference Tables (ExPERT) data for 573 land sites; Surface Marine Gridded Climatology
- 4D real-time and/or archived NWP now-cast / forecast and weather satellite data

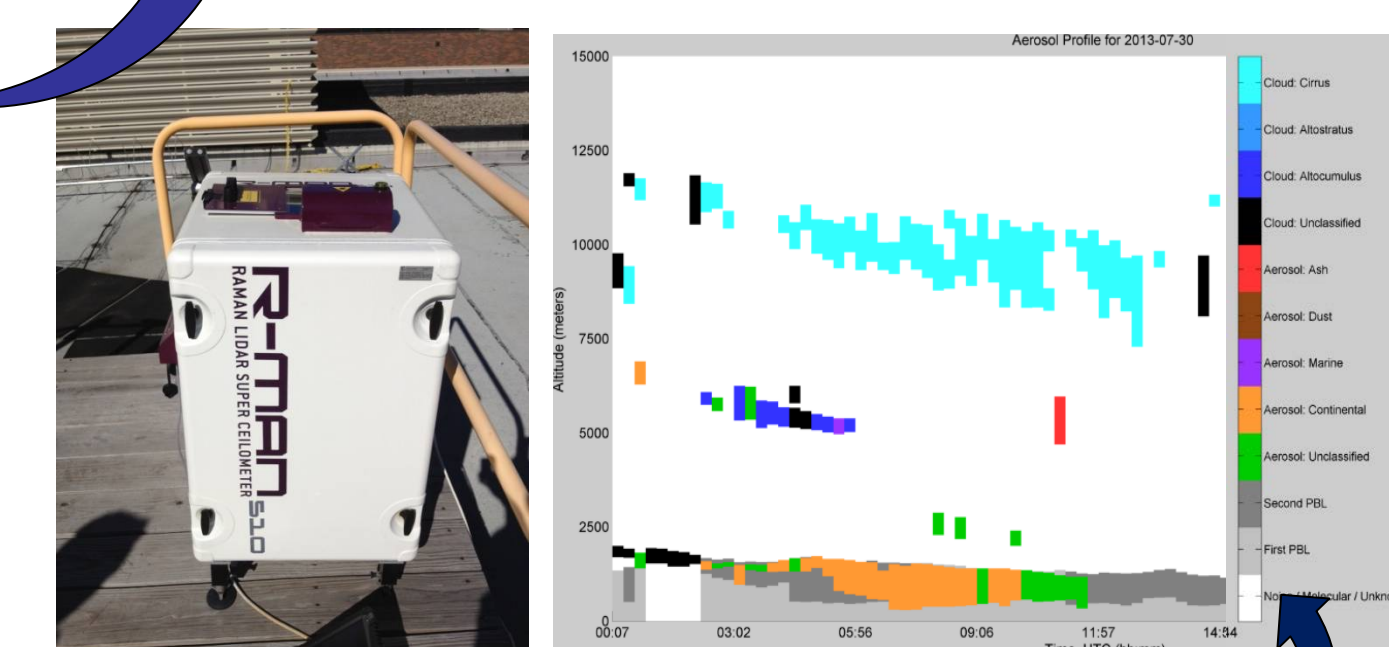
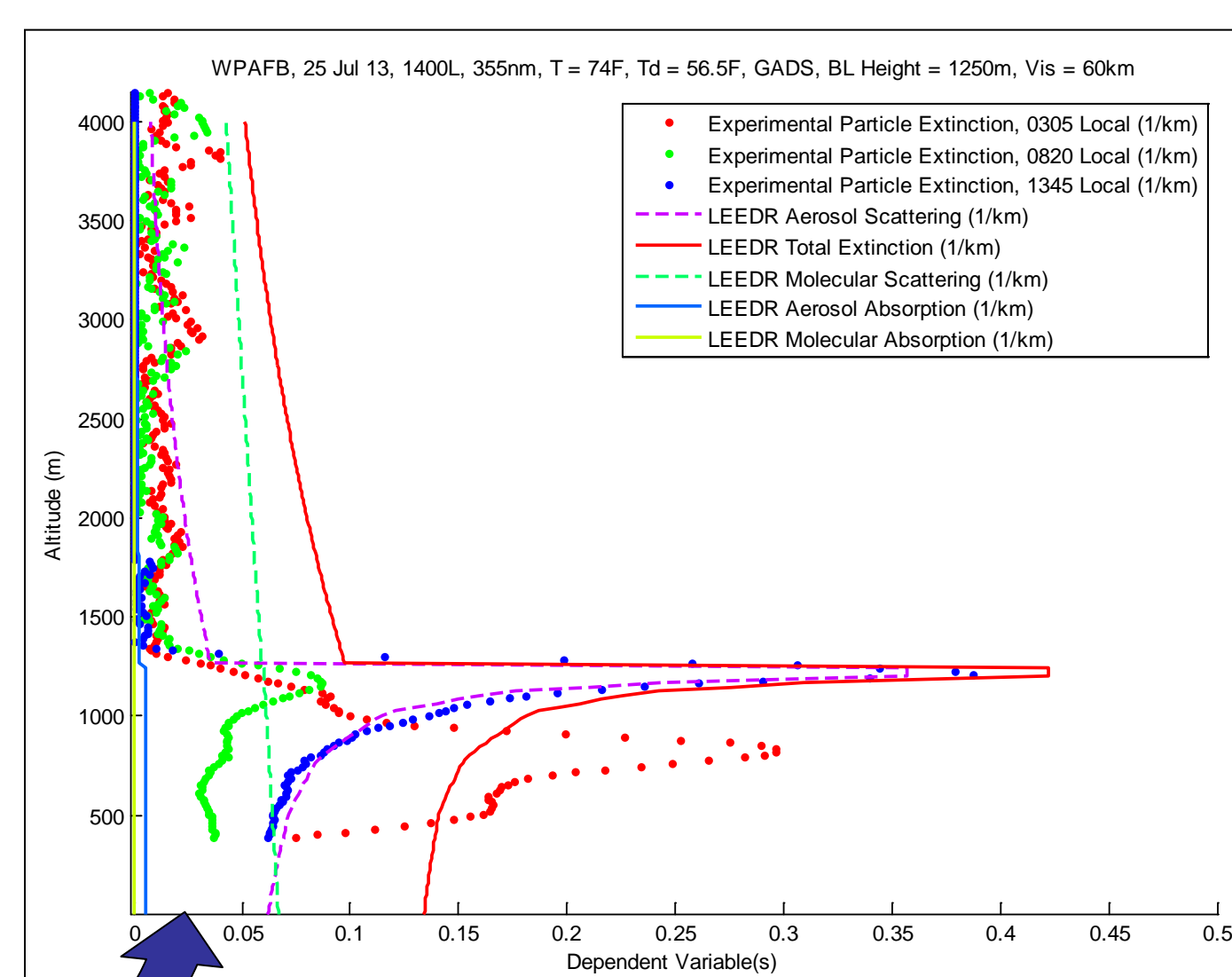
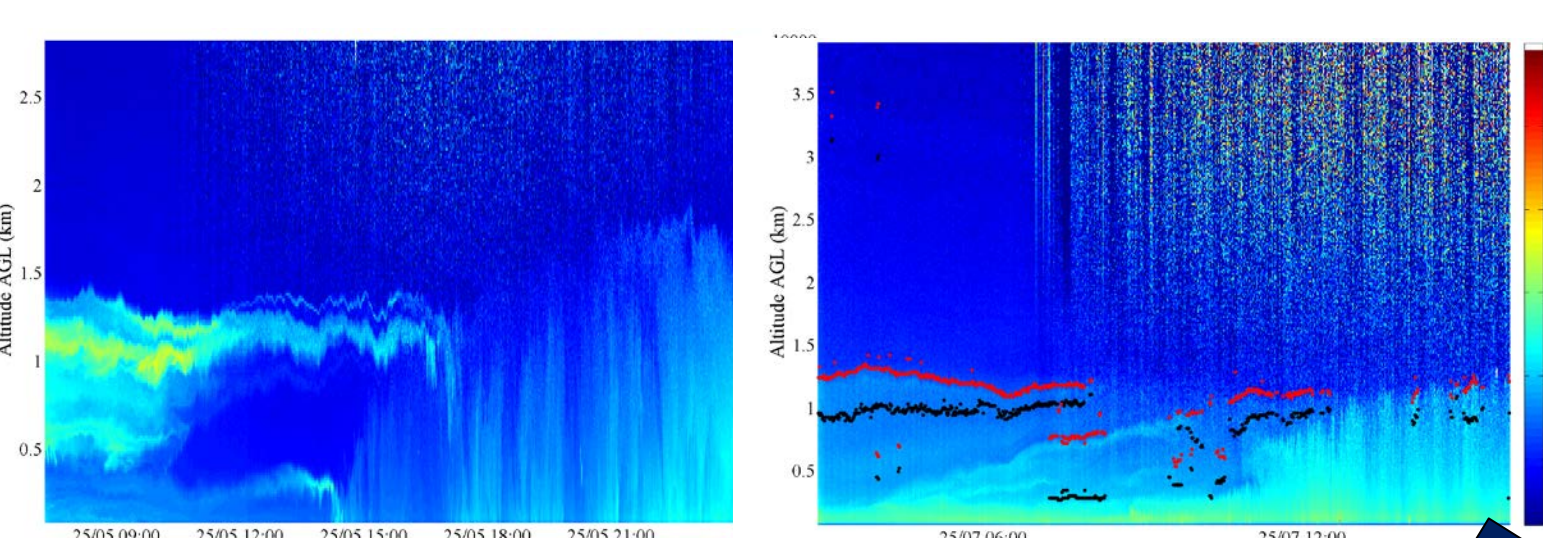


### Results:

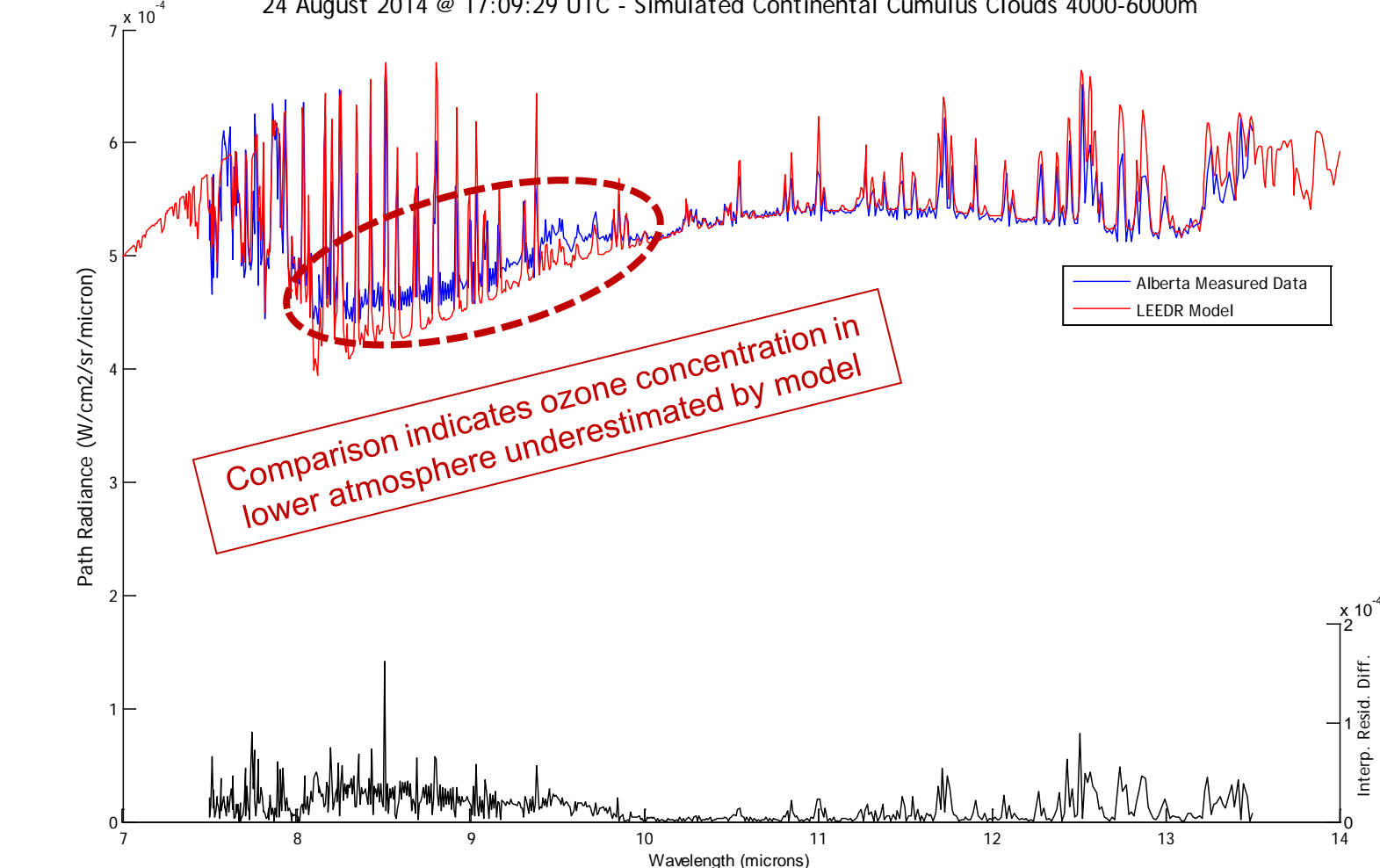
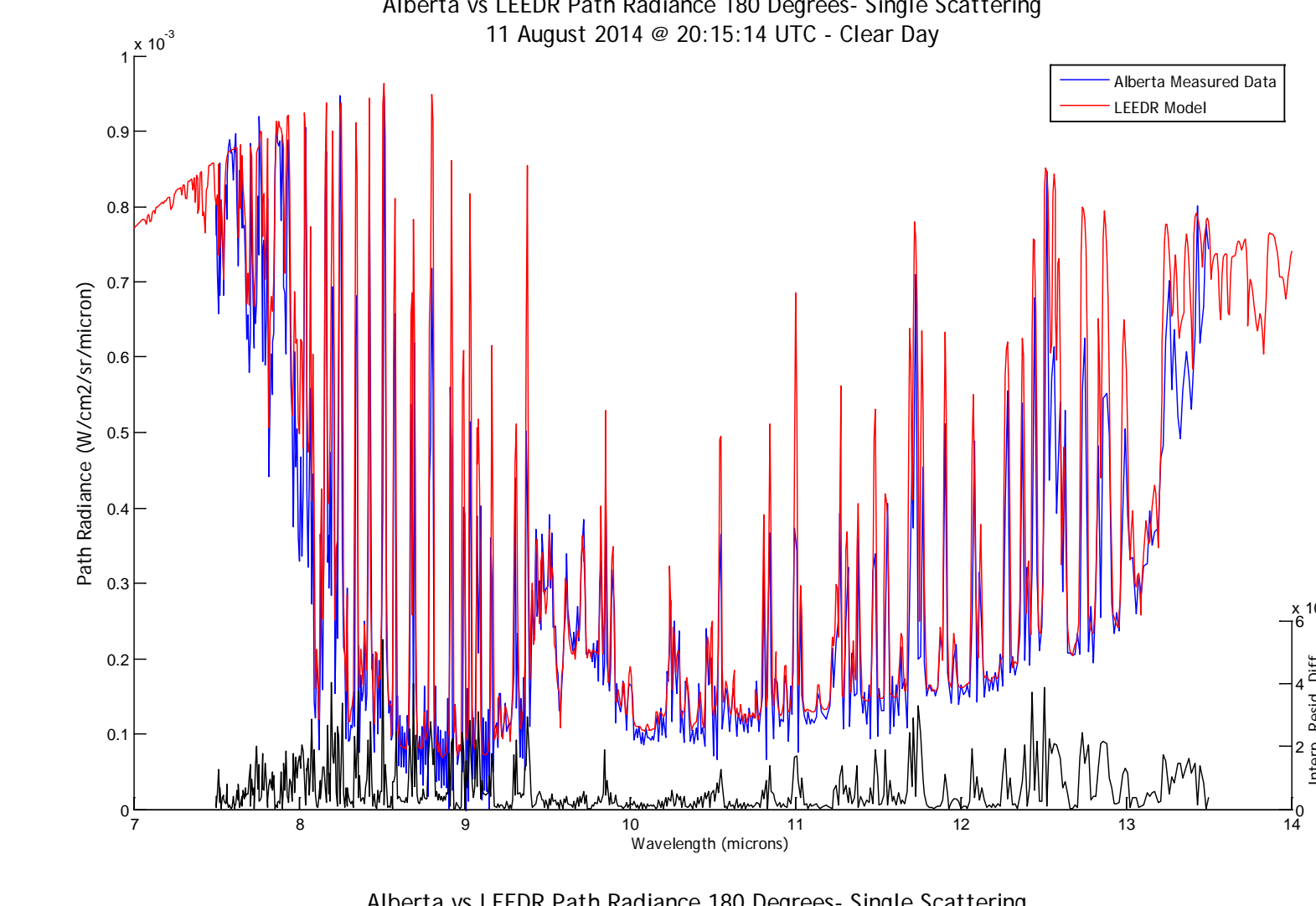
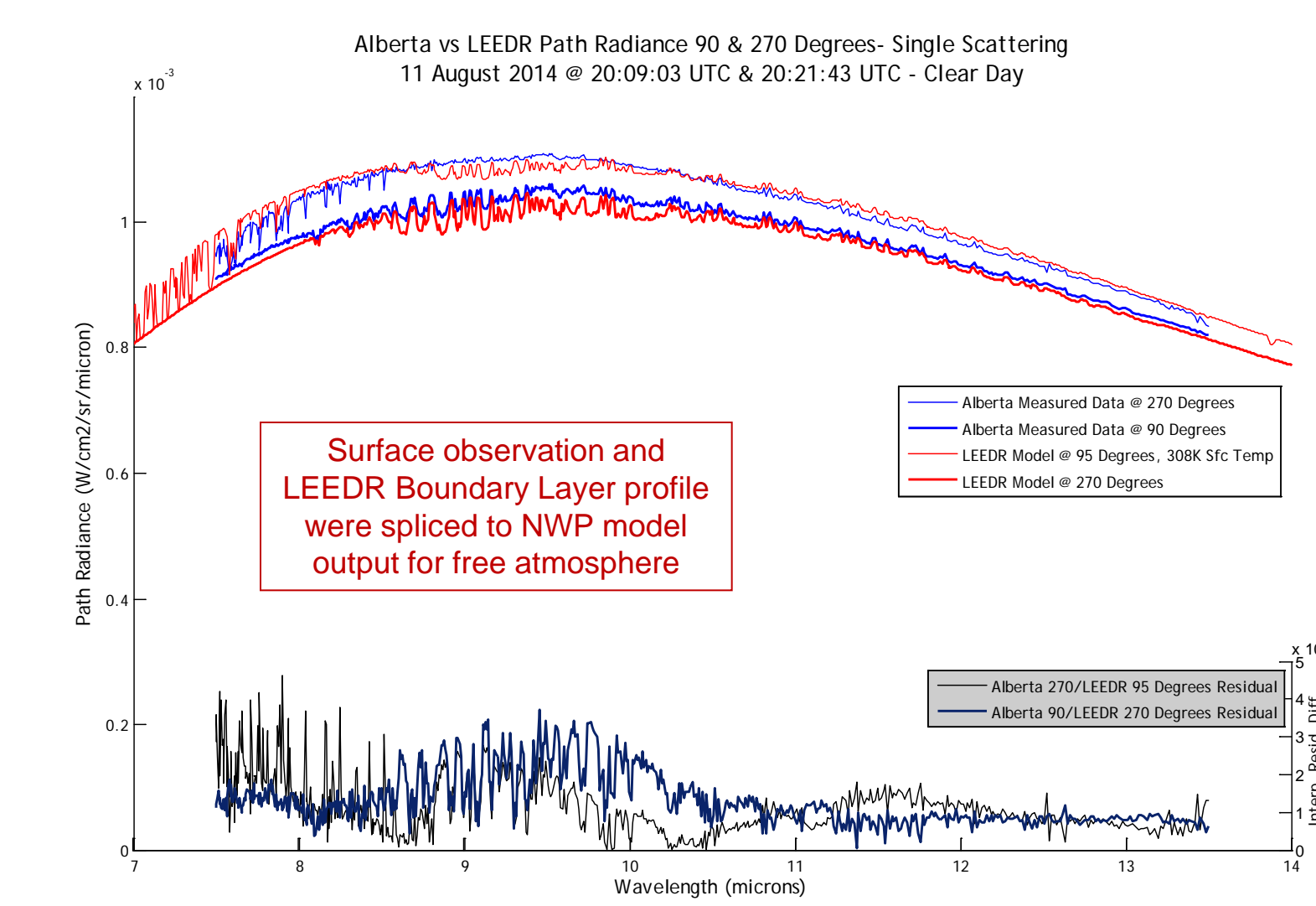
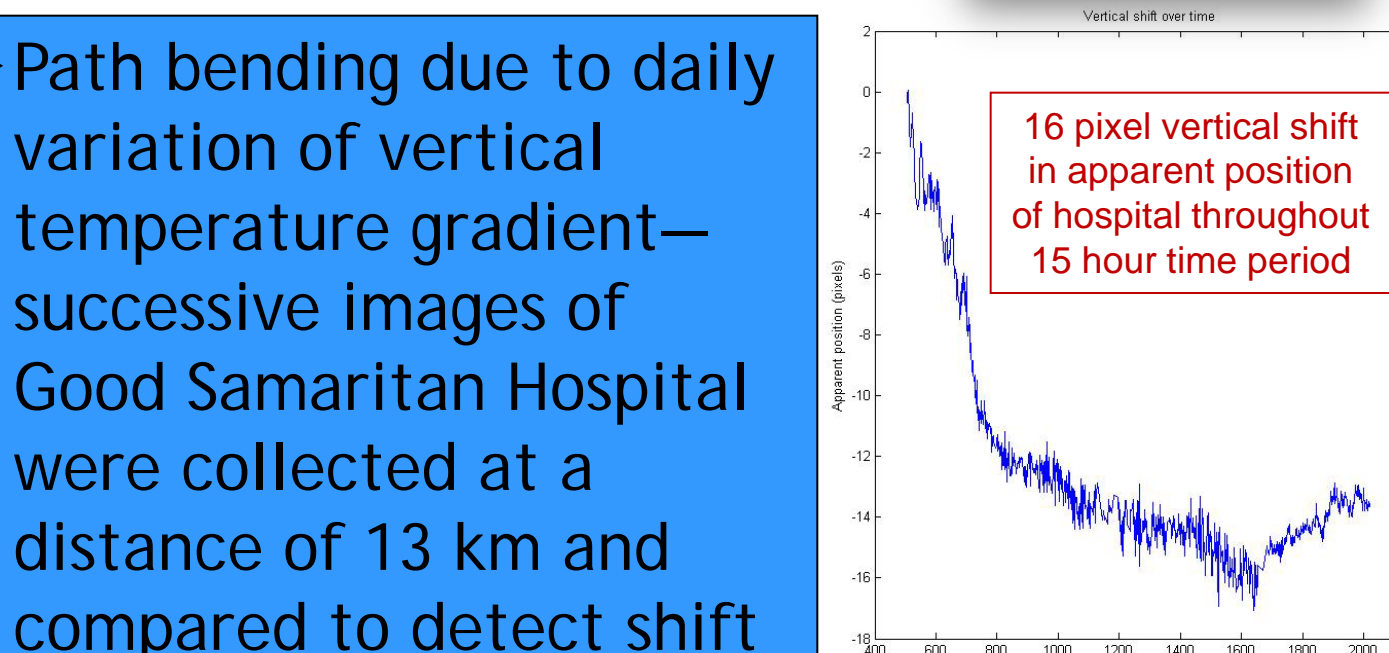
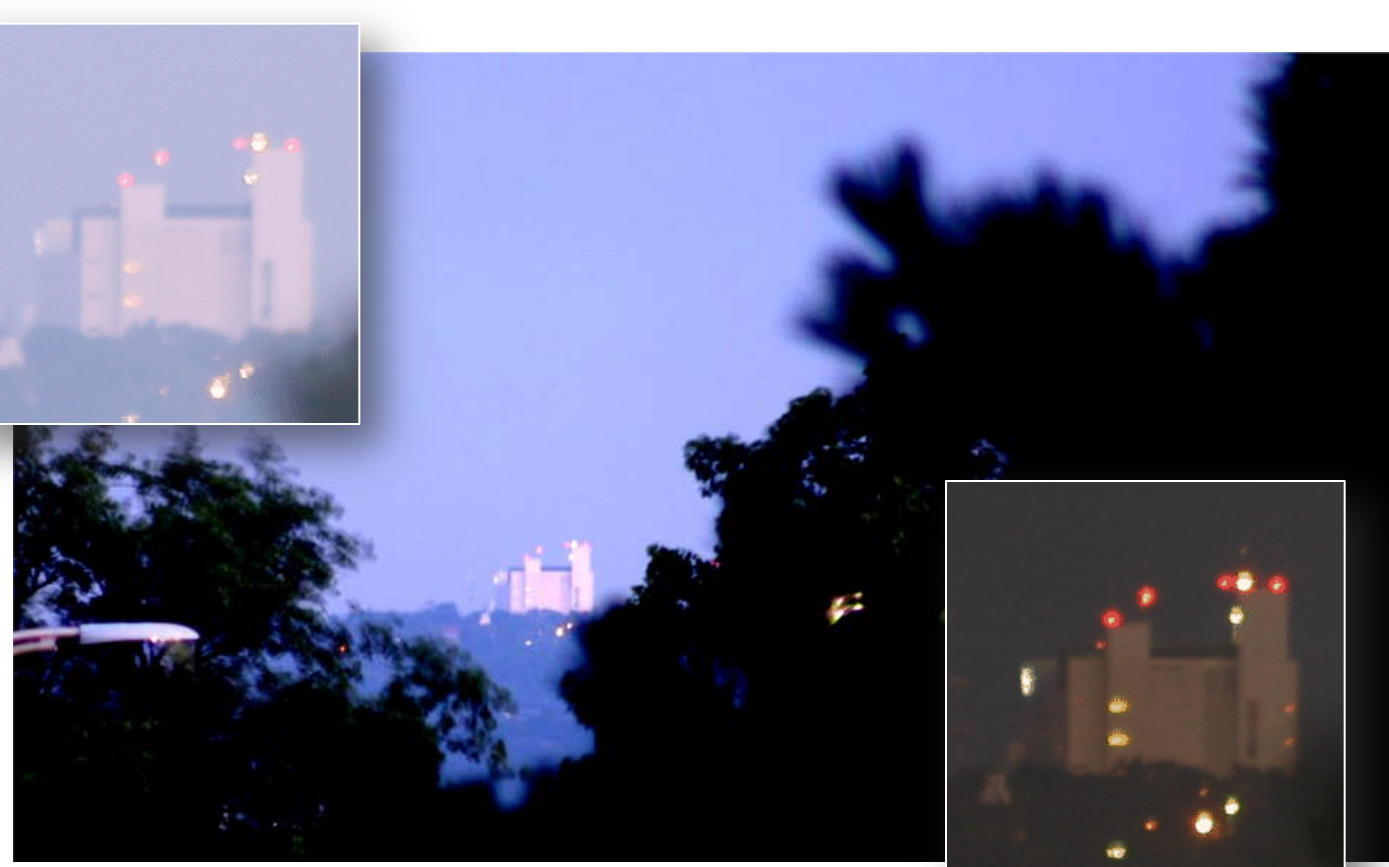
Radar-derived and satellite-derived index of refraction structure function values ( $\log_{10} C_n^2$ ) compared with scintillometer measured  $\log_{10} C_n^2$  along a 7-km path in Dayton, OH



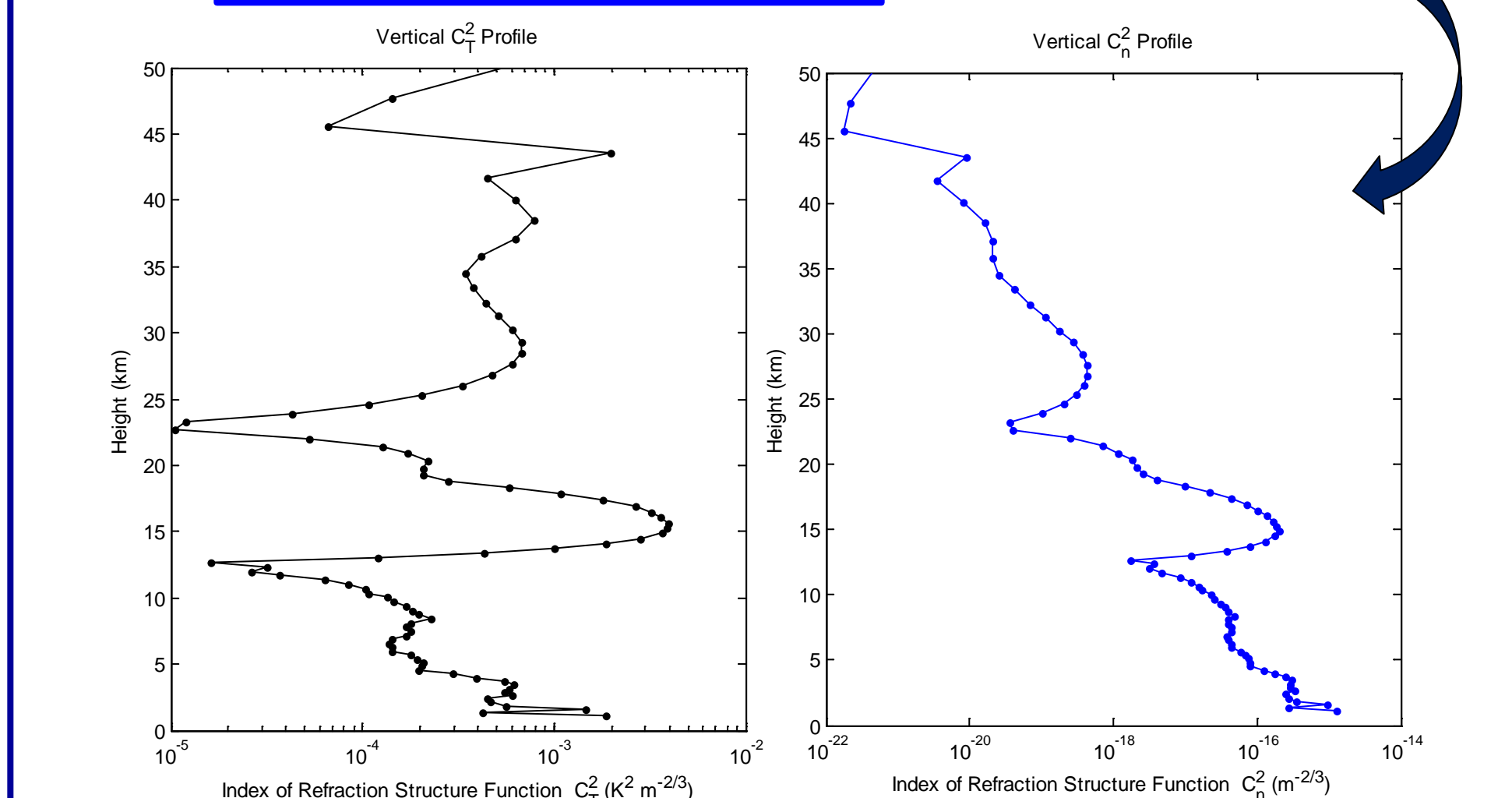
Raman LIDAR validates LEEDR's unique profile of elevated aerosol effects which arise when aerosol radiative characteristics are correctly coupled to appropriate boundary layer lapse rates of temperature and dewpoint



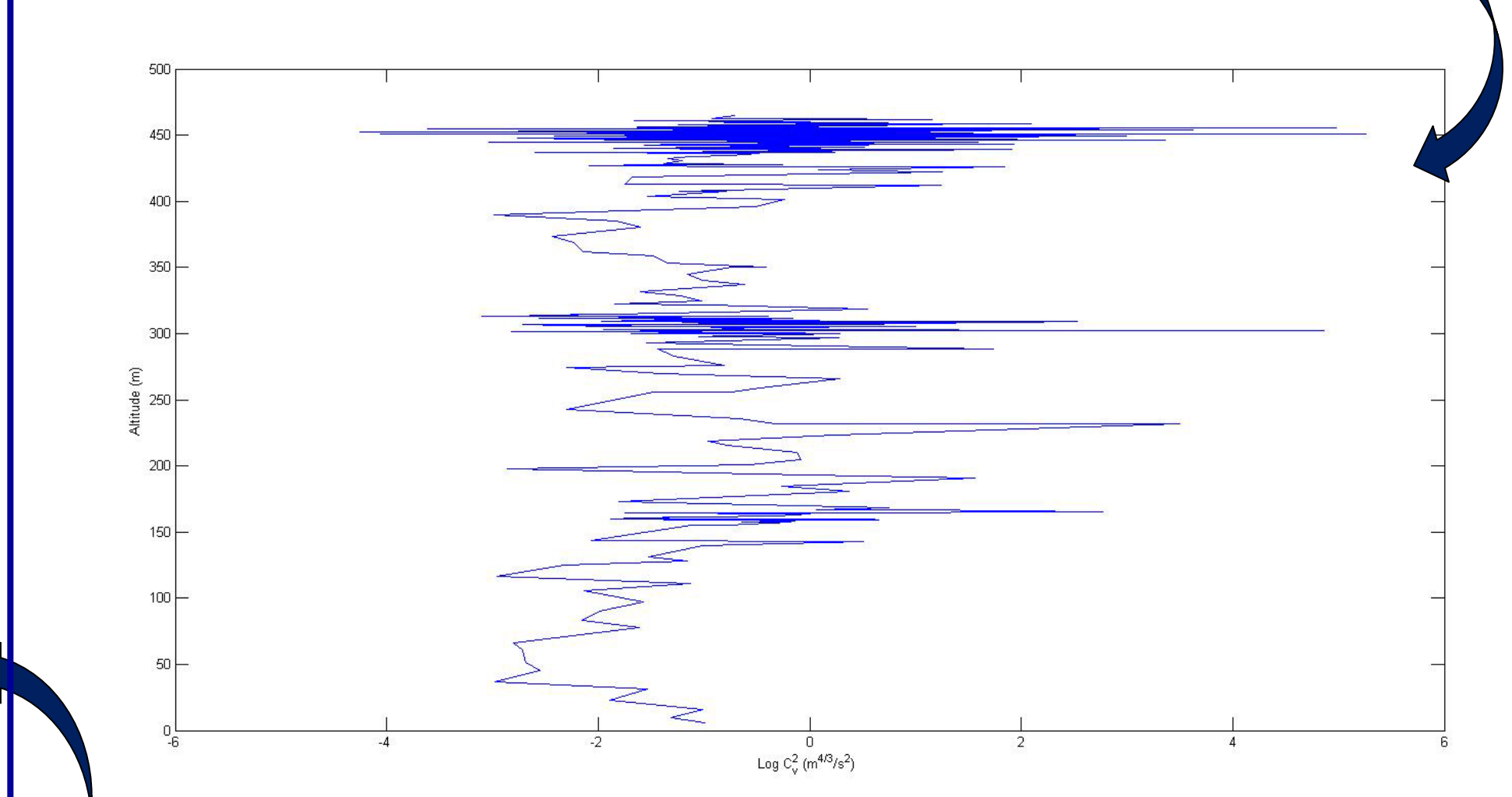
LIDAR ratio allows detection of Planetary Boundary Layer top height, cloud layer detection, and aerosol classification—up to 2 km (day) & 12 km (night)



Applying  $C_n^2 = 2.8 \frac{K_0}{K_0} \left( \frac{79 \times 10^{-6} P}{T^2} \right)^{1/3} L_0^{4/3} \left( \frac{\partial T}{\partial z} + \gamma_a \right)^2$   
 $C_n^2(z) = (0.714) C_n^2(z) \left( \frac{\partial \ln(\rho)}{\partial z} \right)^2 \left( \frac{\partial T}{\partial z} + \gamma_a \right)^2$



$C_n^2$  profile derived from micro-meteorological data for profile collected by Tim Chavez at HELSTF NM on 23 Jul 13



LEEDR Path Radiance compared with field measurements - vertical and horizontal paths with clear and cloud covered sky (Radiance measurements made August 2014 at Southern Alberta site)



### Conclusions:

- Novel methods to obtain temperature, winds, turbulence, cloud base and top heights, and aerosol extinction values through a combination of NEXRAD and satellite-based remote sensor data enhance fundamental radiative transfer calculations (e.g. path radiance and refraction, optical turbulence)
- 4D gridded structure functions of temperature,  $C_T^2$ , refractive index,  $C_n^2$ , and wind velocity,  $C_V^2$  will immediately benefit directed energy simulation tools (e.g. AFIT's High Energy Laser Tactical Decision Aid) and applications (e.g. laser communication system design)
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