THE RESISTANCE NETWORK FOR TRANSFER FROM STREET CANYONS

Janet F. Barlow and Stephen E. Beicher University of Reading, UK

INTRODUCTION

Models of the energy balance of the urban landscape need to account for radiative and turbulent transfer to and from all active surfaces. Whilst the radiative transfer is reasonably well understood, little is known about the turbulent transfer. On the scale of a street, turbulent transport can be represented by a network of resistances between the surfaces and the air (e.g. Masson, 2000). The values of these resistances for an urban geometry are not currently known. This paper describes how the naphthalene sublimation technique, developed in Barlow and Belcher (2002), can be used to measure these resistances in a wind tunnel model.

2. RESISTANCE NETWORK

Figure 1 shows the resistance network for a street. $R_{\rm e}$ is the street resistance, $R_{\rm e}({\rm lee})$ and $R_{\rm e}({\rm wind})$ the resistances for the lee and windward walls respectively; $R_{\rm i}$ is the resistance to transport out of the street carryon and $R_{\rm rest}$ the resistance from the building roots.

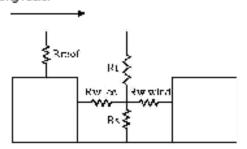


Figure 1: Resistance network for a street carryon. The arrow shows the wind direction.

The resistance, R_i, to transport from the street into the atmosphere above is given by:

$$R_1 = R_S + R_T. \tag{1}$$

The resistance, R_2 , from the wall to the atmosphere is

 $R_2 = (W/H)R_W + R_T$. The resistance, R_3 , from both wall and street is

$$R_3 = R_T + \frac{WR_WR_S}{WR_W + HR_S}.$$
(3)

Equations (1), (2) and (3) can then be inverted to obtain R_5 , R_7 and R_8 in terms of R_1 , R_2 and R_3 .

 R_1 , R_2 and R_3 , were measured using naphthalene sublimation. The active surface was coated with naphthalene and then the windlunnel was run at a constant windspeed. The change in mass of naphthalene over the run was then measured to give the flux out of the carryon, F. By monitoring the temperature, T, of the active surface and applying the ideal gas law, the source concentration of naphthalene vapour, $\rho_{\rm S}$ was calculated. Combining the two gives the resistance

$$R = \frac{\rho_s}{F}$$
(4)

assuming that the background concentration of naphthalene is negligible. By coating () the street only (ii) the wall only and (iii) the street and wall with naphthalene we obtained R₁, R₂ and R₃ respectively.

3. NAPHTHALENE SUBLIMATION METHOD

Figure 2 shows a side-view of the experimental arrangement. A boundary layer was generated using a fence and roughness elements (cf. experiment B in Barlow and Belcher, 2002). An array of 8 street carryons was used with buildings of height h=12.5mm and varying street width (w=50, 12.5, 6.25mm). Naphthalene measurements were made in the eighth carryon downstream. Windspeed was measured at the top of the boundary layer at the midpoint of the eighth carryon using a Pitot-static tube. The temperatures of the street and walls were measured using thermistors.

For each geometry the resistance R_3 was determined for 5 windspeeds between $4ms^4$ and $1\,3ms^4$. It was found that R_1 and R_2 could be derived from the R_3 measurements, i.e. that the measured resistances were independent of the concentration of naphthalene in the carryon. For each aspect ratio, the R_3 experiment was repeated for the both lee and windward walls.

[&]quot;Janet F. Barlow, Dept. of Meteorology, Univ. of Reading, Earley Gate, P.O.Box 243, Reading, RG 66BB, UK. E-mail: j.f.barlow@reading.ac.uk

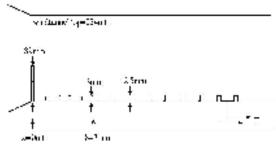


Figure 2 side-view of experimental arrangement. Temperatures of the wall and the street were measured using therm istors.

4. RESULTS

It was observed in all cases that the transfer velocity $w_T = 1/R$ was a linear function of wind speed with negligible offset, hence the dimensionless resistance UR = U/w_T was constant over the range of wind speeds studied for each surface for each geometry. This suggests that the turbulence was the dominant process in transferring scalars from all surfaces. Figure 3 shows dimensionless resistance UR for each surface as a function of street aspect ratio H/W.

It can be seen that UR., for transfer from the leeward wall is almost twice the value from the windward wall. This is consistent with measurements of tracer concentrations within a street carryon (Kastner-Klein and Plate, 1999) which showed increased concentrations of tracer at the lee wall, suggesting weaker transport in its vicinity. The dimensionless resistance for the street UR, lies between the two values. It is interesting to compare our measured values of UR, with values calculated using the empirical formula quoted in Masson (2000). In contrast to our measurements UR, varies with wind speed, and a range of values is shown for each aspect ratio in figure 3. For H/W=0.25 and 1 the range of computed values of UR, is comparable with the measured values for lee and windward walls. There are important differences for H/W=2.

UR_T is small, which suggests that once transfer from the surfaces within the carryon has occurred, ventilation from the carryon is rapid. Evidentially the shear layer at the top of the carryon air space promotes vigorous mixing with the boundary layer as suggested by the observations of Louka, Belcher & Harrison (1999).

It can be seen that there is a small increase in all values of dimensionless resistance between H/W=0.25 and 1, but a notable increase for H/W=2 for the street and leeward wall. As H/W=0.65 marks the onset of the skimming regime, this result suggests a more drastic reduction in the carryon winds for 1<H/>H/W<2, resulting in much reduced transport from

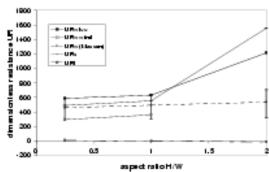


Figure 3: Dimensionless resistance UR as a function of aspect ratio H/W.

each surface within the carryon. This is consistent with the modelling results of Sini et al. (1996), who observed the onset of two counter rotating vortices within the carryon for aspect ratios of H/W≥1.6. Further experiments will be carried out to clarity this point.

5. CONCLUSIONS

Naphthalene sublimation has been used to calculate resistances to turbulent transfer from surfaces within a street carryon. Results suggest that scalar transfer is largest from the windward wall and is smaller for the street surface and leeward walls. This is consistent with the decrease in wind speed around the main, intermittent carryon vortex. Transfer out of the top of the carryon is much more efficient by comparison.

This paper forms part of the UWERN Urban Meteorology Programme (http://www.met.rdg.ac.uk/Research/urb_met/). Funding from NERC under grant GST/02/2231 is gratefully acknowledged.

Barlow, J.F. and Belcher S.E. 2002: A windfunnel model for quantifying fluxes in the urban boundary layer, accepted for publication in *Boundary-Layer Meteorol*.

Kastner-Klein, P. and Plate, E.J., 1999: Wind-tunnel study of concentration fields in street carryons, Atmos. Environ., 33, 3973-3979

Louka, P., Belcher, S.E. & Harrison, R.G. 2000: Coupling between air flows in streets and the well-developed boundary layer aloft, Atmos. Environ. 34, 2613-2621

Masson, V., 2000: A physically-based scheme for the urban energy budget in atmospheric models, Boundary-Layer Meteorol., 94, 357-397.

Sini, J.F., Anquetin, S., and Mestayer, P.G., 1995: Pollutant dispersion and thermal effects in urban street carryons, Atmos. Environ., 30(15), 2659-2677.