

## 4B.2 THE 'AREA INTEGRATED Z/ZDR' TECHNIQUE FOR IMPROVED RAINFALL RATE ESTIMATES WITH OPERATIONAL POLARISATION RADAR

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### 1 INTRODUCTION

Observations of differential reflectivity,  $Z_{dr}$  provide information on the mean raindrop shape and hence raindrop size. When combined with the conventional reflectivity it should be possible to estimate both the size and the concentration of the raindrops and so infer a more accurate rainfall rate than is possible from Z alone. However, it appears that in an operational environment the accuracy with which  $Z_{dr}$  can be estimated at each gate is not sufficient to realise the potential of the method. In this paper we suggest an alternative approach. The values of Z and  $Z_{dr}$  are examined at each gate over a region where the raindrop spectra are supposed to have the same characteristics, and these values are then used to derive an appropriate  $Z = aR^b$  relationship for use over that region.

### 2 Z-R RELATIONSHIPS AND NORMALIZED GAMMA RAINDROP SPECTRA

The natural variability of rain drop spectra is well captured by the normalized gamma function:

$$N(D) = N_w f(\mu) \left( \frac{D}{D_0} \right)^\mu \exp \left( - \frac{(3.67 + \mu)D}{D_0} \right) \quad (1)$$

where

$$f(\mu) = \frac{6}{(3.67)^4} \frac{(3.67 + \mu)^{\mu+4}}{\Gamma(\mu + 4)} \quad (2)$$

with three independent parameters,  $N_w$ , the normalised concentration,  $D_0$ , the median volumetric drop diameter, and  $\mu$  a shape factor for the width of the spectrum. The normalization factor  $f(\mu)$  is chosen so that for a given  $N_w$  the value of the liquid water is independent of  $\mu$ . The numerical factor ensures that when  $\mu = 0$  we have the conventional exponential form  $N(D) = N_w \exp(-3.67(D/D_0))$ .

Assuming a Marshall-Palmer type raindrop spectrum, then as the rain becomes heavier  $D_0$  increases but  $N_w$  and  $\mu$  remain constant. Integration over suitably weighted values of Eqn(1) predicts Z varying as  $N_w D_0^7$  and R as  $N_w D_0^{4.67}$ . Eliminating  $D_0$  gives  $Z = aR^b$  with  $b = 1.5$  and  $a$  varying as  $1/\sqrt{N_w}$  (Bringi and Chandrasekar, 2001). The oft quoted "factor of two" error in the value of R would then arise in natural rain if  $N_w$  varies by up to a factor of ten and consequently 'a' would change by up to a factor of three.

A constant value of  $N_w$  with varying rainfall rate is widely assumed, as in the 'ZPHI' technique of Testud et

al (2000), but it is quite possible that  $N_w$  is a function of  $D_0$ . This will give rise to different values of  $b$ . For example, if  $N_w$  falls as  $1/D_0$  then integration gives that Z varies as  $D_0^6$  and R as  $D_0^{3.67}$  and elimination gives us  $Z = aR^b$  with  $b = 1.63$ . The index of 1.6 is widely used in Europe as a default Z-R relation. Alternatively, if  $N_w$  rises as  $D_0^2$  then we would have Z and R varying as  $D_0^9$  and  $D_0^{6.67}$ , respectively, leading to a value of  $b=1.34$ , close to the default Nexrad Z-R relation. The extreme example would be  $D_0$  remaining constant, in this case, as  $N_w$  rises, Z and R would scale together and we would have  $Z=aR$ , as has been suggested by List (1988).

Fig. 1 shows the full computed solutions for the various  $N_w$  versus  $D_0$  combinations for  $\mu = 5$  using the correct terminal velocity relationship, rather than assuming  $V(D)$  varies as  $D^{0.67}$ , and demonstrates they are very close to the predicted power laws. The value of  $N_w$  for a rainfall rate of  $1 \text{ mm hr}^{-1}$  is fixed in all three cases to be  $8000 \text{ m}^{-3} \text{ mm}^{-1}$  which for  $\mu = 5$  implies a  $D_0$  of  $0.867 \text{ mm}$  and a Z of  $21.72 \text{ dB}$ , so the value of  $a$  in all three equations is 148, but  $b$  varies.

In the next section we show how analysis of observed values of Z and differential reflectivity  $Z_{dr}$  provides information on raindrop size and concentration and reveals how  $N_w$  and  $D_0$  are linked and can be used to predict the best values of  $a$  and  $b$  to be used in a Z-R relation.

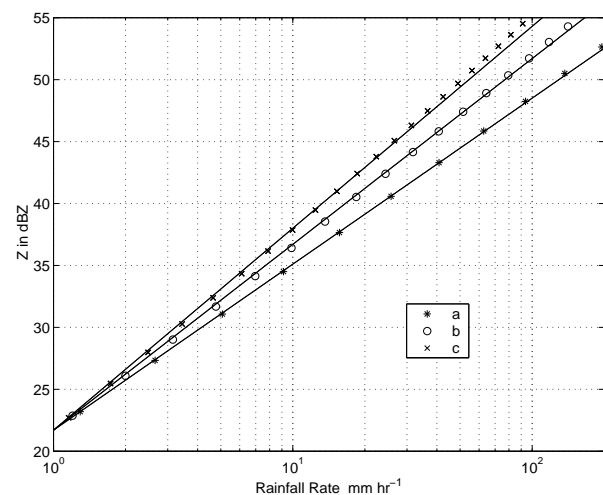


Figure 1: The value of Z and R computed for  $\mu = 5$  and  $N_w = 8000 \text{ m}^{-3} \text{ mm}^{-1}$  for  $D_0 = 0.867 \text{ mm}$  and  $R = 1 \text{ mm hr}^{-1}$ . a)  $N_w \propto D_0^2$  b)  $N_w$  const, c)  $N_w \propto D_0^{-1}$ . The straight lines all have  $a = 148$ , but  $b$  is 1.34, 1.5 and 1.63, respectively.

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### 3 THE LINK BETWEEN DIFFERENTIAL REFLECTIVITY, DROP CONCENTRATION AND DROP SIZE

The differential reflectivity,  $Z_{dr}$ , essentially measures the mean raindrop shape and hence once the drop shapes are known can be related to the equivolumetric diameter,  $D_0$ , in the normalized gamma function. Because  $Z_{dr}$  is a ratio it is independent of  $N_w$ , so for a given  $Z_{dr}$  (constant  $D_0$ ) both  $Z$  and  $R$  will scale with  $N_w$ . For each value of  $Z_{dr}$  we can calculate the value of  $Z$  for a rainfall rate of  $1 \text{ mm hr}^{-1}$ :  $Z(1 \text{ mm hr}^{-1}) = f(Z_{dr})$ . If we were to observe  $Z_{obs}$  is a factor 'x' above this value of  $Z$ , then we can say that the rain rate is  $x \text{ mm hr}^{-1}$ . In Fig 2 are plotted the values of  $Z$  and  $Z_{dr}$  expected for a rainfall rate of  $1 \text{ mm hr}^{-1}$  for various values of  $\mu$  using the drop shapes of Goddard et al (1995) based on comparing observed  $Z_{dr}$  values above a ground based disdrometer. Essentially the same curves are produced if the later laboratory shapes of Andsager et al (1999) are used. For comparison with Fig 1 the solid line in Fig 2 describes the values of  $Z$  and  $Z_{dr}$  for  $N_w = 8000 \text{ m}^{-3} \text{ mm}^{-1}$ . We see that  $R=1 \text{ mm hr}^{-1}$  has a  $Z$  of 21.7dBZ and a  $Z_{dr}$  of just 0.14dB. For this value of  $N_w$  a  $Z_{dr}$  of 0.5dB would be associated with a rainfall rate of just under  $10 \text{ mm hr}^{-1}$ .

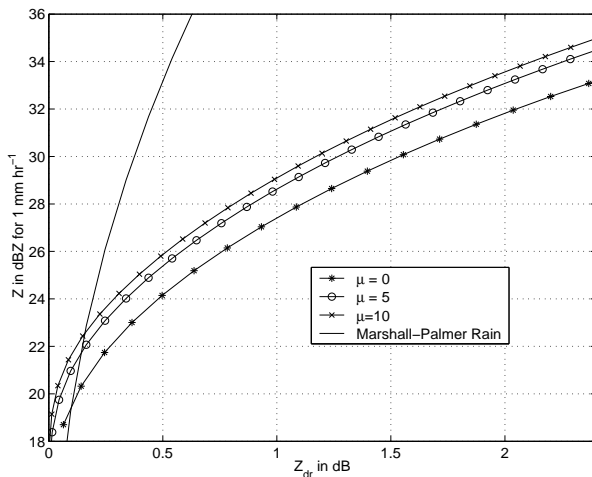


Figure 2: The value of  $Z$  for a rainfall rate of  $1 \text{ mm/hr}$  as a function of the observed  $Z_{dr}$  for different values of  $\mu$ . The solid line are the values of  $Z$  and  $Z_{dr}$  for const  $N_w = 8000 \text{ m}^{-3} \text{ mm}^{-1}$ .

The slopes of the lines in Figure 2 provide us with an estimate of the required accuracy of the  $Z_{dr}$  estimate. The steep slope for low rainfall rates means that for a rainfall rate of  $3 \text{ mm hr}^{-1}$  to be estimated to within 25% then  $Z_{dr}$  must be known to better than 0.1dB. For  $10 \text{ mm hr}^{-1}$  this can be relaxed to 0.2dB. Many flood producing situations in Europe result from prolonged rainfall of less  $10 \text{ mm hr}^{-1}$ ; unfortunately achieving an accuracy of  $Z_{dr}$  at each gate of 0.1dB is impossible for an operational radar (see Illingworth, 2003 for a detailed discussion). The statistical noise in the  $Z_{dr}$  estimator means that even if the correlation between the H and V returns is 0.98, then 60 independent samples are needed to achieve 0.2dB accuracy. Unrealistically long dwell times would be needed

for 0.1dB. In addition, for operational radars with imperfect antennas, effects such as reflectivity gradients in the presence of mismatched sidelobes, mismatched beam patterns in H and V leading to a lowering of the correlation, and triple scattering echoes will all contribute noise into the individual  $Z_{dr}$  estimates.

In the next section we outline a different approach which relies on the characteristics of  $Z$  and  $Z_{dr}$  to provide information on drop sizes and concentrations.

### 4 THE AREA INTEGRATED Z/ZDR TECHNIQUE

Observations of  $Z$  and  $Z_{dr}$  taken in convective rain over a 4km square region of a low level PPI with the narrow beam (0.28deg) Chilbolton S-band radar are displayed in Fig.3. Values of  $Z$  are ranging from 30dBZ to 55dBZ. Even with this high quality research radar the data points show considerable scatter; the spread in  $Z$  for a given  $Z_{dr}$  is over 10dB indicating that inferred values of  $N_w$  over this small region are scattered over an order of magnitude. Similarly, for a given  $Z$  there is a big spread of observed  $Z_{dr}$ , indicating that for a particular value of  $Z$  the rainfall rates are changing by over a factor of two. The dash-dot line is a polynomial fit of  $Z$  against  $Z_{dr}$  but of course since the rainfall rates are distributed around this in a logarithmic fashion, if the scatter reflects reality, then the mean rainrates will be above this line. We suggest that if the scatter is due to random noise arising from instrumental imperfections, using individual data points will lead to a biased retrieval in the rainfall rate.

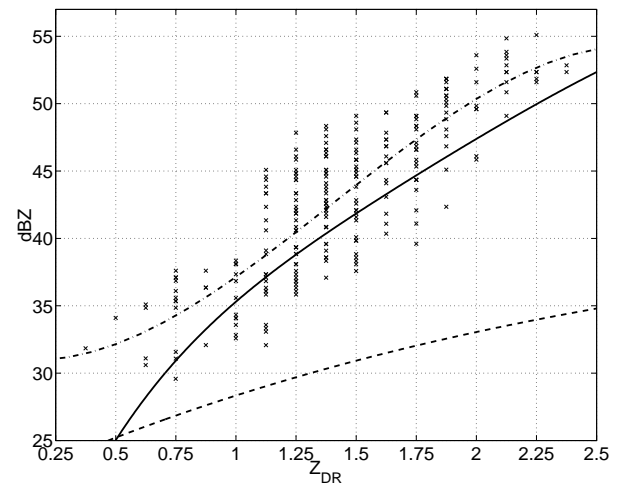


Figure 3: Observed values of  $Z$  and  $Z_{dr}$  for a 4km square region of convective rain. Solid line - Marshall-Palmer; Dashed line:  $R=1 \text{ mm hr}^{-1}$ ; Dash-dot line - polynomial fit.

A polynomial fit of  $Z$  as a function of  $Z_{dr}$  is plotted as the dash-dot line in Fig 3 and is about 2-3dB above the Marshall-Palmer line, indicating that the values of  $N_w$  are approximately constant but rather higher than  $8000 \text{ m}^{-3} \text{ mm}^{-1}$ , and that  $a$  should be lower than the 148 in Fig 1. The difficulty with this approach is that a polynomial fit of  $Z_{dr}$  against  $Z$  would give a very different relationship.

The alternative approach is shown in Fig 4, where the individual observations of  $Z$  and  $Z_{dr}$  in Fig 3 have been converted into  $Z$  and  $\log R$  and plotted, together with the  $b=1.5$  Marshall-Palmer line from Fig 1. Because the data are so scattered, a regression of  $Z$  on  $Z_{dr}$  will produce a different result from the regression of  $Z_{dr}$  on  $Z$ . In this case the most appropriate fit is the so-called 'standard deviation' or 'SD' line. If we compute the average value of the data points,  $\overline{\log R}$  and  $\overline{\log Z}$  and their standard deviations  $\sigma_{\log R}$  and  $\sigma_{\log Z}$ , then the SD line passes through the point  $\overline{\log R}$  and  $\overline{\log Z}$  with the gradient  $\sigma_{\log Z} / \sigma_{\log R}$ . In this convective case the SD line suggests we have  $a=433.5$  and  $b=1.33$ .

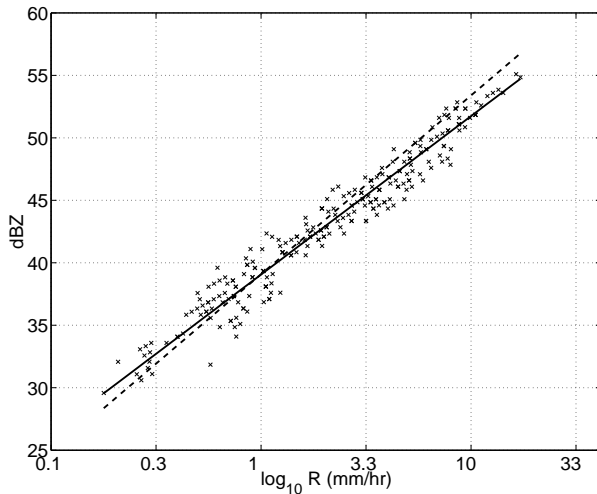


Figure 4: The data in Fig 3 plotted in  $\log Z$ - $\log R$  space. Solid line: S-D line equivalent to  $Z = 433R^{1.33}$ . Dashed line: Marshall-Palmer with  $b=1.5$ .

The observations in stratiform are rather different and are displayed for a 4km square in Fig 5. In this case the range of the data is less with  $Z$  values between 28dBZ and 40dBZ and the highest values of  $Z_{dr}$  only 1.8dB. Although there is again a large scatter of the individual data points, there is a definite suggestion that when compared to the const  $N_w$  Marshall-Palmer line,  $N_w$  is falling as the drops get larger and  $D_0$  increases.

The stratiform data is replotted in  $\log Z$ - $\log R$  space in Fig 6. Because of the smaller dynamic range the relative scatter of the data points is much greater than in Fig 4, and so polynomial fits or regression lines will give inconsistent values. The S-D line gives  $Z = 321R^{1.62}$ .

## 5 CONCLUSIONS

We suggest that the different  $Z = aR^b$  relations can be explained in terms of the variability of  $N_w$  and  $D_0$  in the normalized gamma function used to represent the range of naturally occurring drop size spectra. As rainfall becomes heavier  $D_0$  generally increases and if  $N_w$  remains constant then  $b = 1.5$ . If  $N_w$  falls with increasing  $D_0$  then  $b$  rises above 1.5, but if  $N_w$  falls then  $b$  is lower than 1.5. In theory, observations of  $Z_{dr}$  combined with  $Z$  should enable values of  $N_w$  and  $D_0$  to be derived at each gate, but

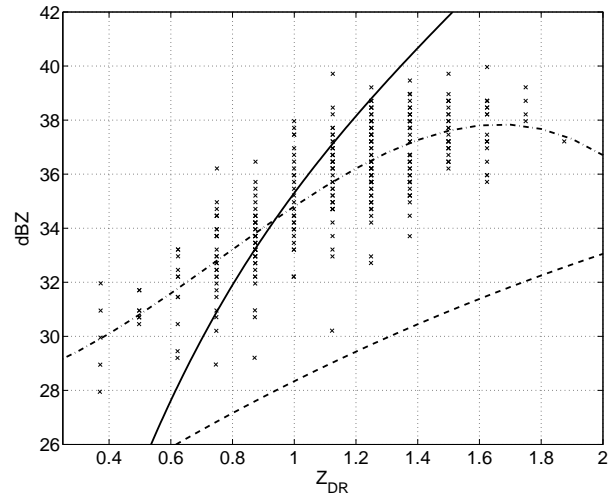


Figure 5: Observed values of  $Z$  and  $Z_{dr}$  as for Fig 3 but for stratiform rain.

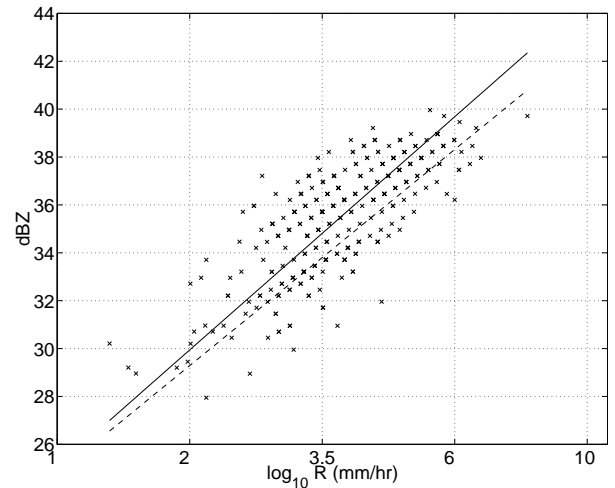


Figure 6: AS for Fig 4 but for 4km square region of stratiform rain. Solid line is S-D line equivalent to  $Z = 321R^{1.62}$ .

in practice the values at individual gates are too noisy for this to be possible.

We suggest a new approach, whereby the values of  $\log Z$  and  $\log R$  derived from observed  $Z$  and  $Z_{dr}$  over a small region are examined, and an 'SD' fit through the data provide a better estimate of  $a$  and  $b$  in the  $Z$ - $R$  relation. This method assumes that the instrumental effects introduce random noise into both of the observables,  $Z$  and  $Z_{dr}$ , so that an averaged value will approach reality. However, because the inferred rain rates are logarithmically distributed in  $Z/Z_{dr}$  space, averaging of the noisy values at individual gates could produce a biased value of rainfall.

Initial tests on a 4km square region of convective rain and a similar sized region of stratiform rain, yield the relationships,  $Z = 433R^{1.33}$  and  $Z = 321R^{1.62}$ . This seems to confirm the many empirical findings recently published, that the convective rain has a higher concentration of raindrops than stratiform, and it also suggests that higher val-

ues of  $b$ , such as the 1.6 used as a default in Europe' really are more appropriate for stratiform conditions. Stratiform rainfall originates from melting snow, and it may be that in heavier precipitation the increased aggregation of snowflakes is responsible for the fall in  $N_w$ .

It seems that this method could be applied operationally and, when consideration is given to the broader beamwidth of such radars, appropriate values of  $a$  and  $b$  derived over each square region of side 10 or 20km. We plan to investigate this further.

ACKNOWLEDGEMENTS. We thank RAL for the Chilbolton radar data. RJT acknowledges the support of a NERC studentship and the Met Office.

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